Date: May 5, 2021



Jose Pugeda 12050 Baltimore Avenue Beltsville, MD 20705-1247 (301) 370-2211		NB+C Enginee 6095 Marshale Suite 300 Elkridge, MD 2	e Drive
Subject:	Mount Analysis Report		
Carrier Designation:	T-Mobile <i>ANCHOR</i> T-Mobile Site Number:		7WAC050A
	T-Mobile Site Name:		White Oak Tower
Engineering Firm Designation:	NB+C ES Project Number:		100595
Site Data:	301 Maple Ave West Vienna, Latitude: <i>38.89820100°</i> , Long 81.5 ft Penthouse Rooftop Pipe Mounts at 79.0 ft		5100°

Dear Mr. Pugeda,

**NB+C** Engineering Services is pleased to submit this "Mount Analysis Report" to determine the structural integrity of the above-mentioned tower mounts.

The purpose of the analysis is to determine acceptability of the tower mount stress level. Based on our analysis we have determined the tower mount stress level for only the mount structure to be:

# Existing + Proposed Equipment

# 99.7% - Sufficient Capacity

The analysis has been performed in accordance with the ANSI/TIA-222-G standard, 2015 Virginia Uniform Statewide Building Code and local code requirements based upon a wind speed of 115 mph (ultimate 3-second gust).

All equipment proposed in this report shall be installed in accordance with the information provided for the determined available structural capacity to be effective.

We at *NB+C Engineering Services* appreciate the opportunity of providing our continuing professional services to *T-Mobile*. If you have any questions or need further assistance on this or any other projects, please give us a call.

Structural analysis prepared by: Muritala Adegoke, PhD

Respectfully submitted by:

Krupakaran Kolandaivelu, PE Director of Engineering VA License No. 49792



# TABLE OF CONTENTS

# **1] INTRODUCTION**

#### **2] ANALYSIS CRITERIA**

Table 1 - Final Antenna and Cable Information

## **3] ANALYSIS PROCEDURE**

Table 2 - Documents Provided 3.1] Analysis Method

3.2] Assumptions

### 4] ANALYSIS RESULTS

Table 4 - Section Capacity [Summary]Table 5 - Connection Capacity [Summary]

# **5] CONCLUSIONS & RECOMMENDATIONS**

# 6] APPENDIX A

Mount Analysis Additional Calculations

# 1] INTRODUCTION

The proposed mounts are 2.0" nom sch 40 Pipe x 6ft long and 2.5" nom sch 40 x 12ft long Pipe Mounts located in Vienna, VA.

# 2] ANALYSIS CRITERIA

Building Code: TIA-222 Revision: Risk Category:	2015 Virginia Uniform Statewide Building Code ANSI/TIA-222-G
Wind Speed:	115 mph
Exposure Category:	В
Topographic Factor:	1
Ice Thickness:	0.75 in
Wind Speed with Ice:	30 mph
Seismic Sds:	0.129

## Table 1 - Final Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Carrier	Feed Line Size (in)	Note
		4	Ericsson	AIR6449 B41 (33.10"x20.60"x8.30", 112lbs)	T-Mobile	(4) 6x12	
		4	Ericsson	RADIO 4415 B25 (16.5"x13.5"x5.90". 46lbs)	I-MODILE	Hybrid	-
74.0 79.0	74.0 79.0	6	-	2.5SCH40	-	-	-
		2	Site Pro 1	WWM03	-	-	-
		2	Site Pro 1	SP250-6	-	-	-

### Table 2 - Existing Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)		Antenna Manufacturer	Antenna Model	Carrier	Feed Line Size (in)	Note
		2	Andrew	TMBXX-6516-A2M			
		4	Ericsson	Twin Style 1A	•		2
		6	Ericsson	Twin Style 1B		(4) 6x12	
74.0 79.0	74.0 79.0	4	Ericsson	AIR32 DB B66A/B2A	T-Mobile	Hybrid <sup>1</sup>	
		4	Ericsson	APXVAARR24_43-U-NA20	-		1
		4	Ericsson	Radio 4449 B71+B85	-		
		6	-	Mount Pipes	-	-	-

Notes: 1) 2)

) Existing Equipment to remain

Existing Equipment to be removed; was not considered in this analysis.

# 3] ANALYSIS PROCEDURE

# Table 3 - Documents Provided

Document	Remarks	Reference	Source
RFDS	T-Mobile	2/2/2021	On File
Site Audit Photos	NB+C	2/10/2021	On File
Previous Construction Drawings	Advantage Engineers	9/09/2010	On File
Previous structural Analysis	CMX	1/27/2010	On File
Construction Drawings	NB+C	4/19/2021	On File

#### 3.1] Analysis Method

RISA-3D (Version 18.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower mount and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

#### 3.2] Assumptions

This report is based on the theoretical capacity of the existing mount structure and is not an assessment of the overall suitability of the existing mount structure or its components for any particular use other than specified in this report:

- 1) This report makes no warranties, expressed and/or implied, and disclaims any liability arising from material, fabrication and erection of the existing Structure or proposed equipment, and any other existing or proposed components or appurtenances.
- 2) Tower mounts were built in accordance with the manufacturer's specifications.
- 3) The tower mounts have been maintained in accordance with the manufacturer's specifications and current TIA Standards.
- 4) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Table 1.
- 5) Material grades were not provided and were assumed to be in accordance with Table 2-4 "Applicable ASTM Specifications for Various Structural Shapes" per the AISC 15<sup>th</sup> Edition of the Steel Construction Manual. The following material grades were assumed:
  - a) Pipe Grade: ASTM A53-B-35
  - b) Angle Grade: ASTM A36
  - c) HSS Rect. Grade: ASTM A500 Gr. B
  - d) Plate Grade: ASTM A36
- 6) All welds and connections are assumed to develop at least the member capacity unless determine otherwise and explicitly stated in this report.
- 7) Location of the existing and proposed equipment on the existing mount structure is based on information provided to **NB+C ES**.

This analysis may be affected if any assumptions are not valid or have been made in error. Network Building + Consulting Engineering Services, LLC should be notified to determine the effect on the structural integrity of the tower mount structure.

# 4] ANALYSIS RESULTS

able 4 - Section Capac	ble 4 - Section Capacity (Summary)							
Component Type	Size	Bending Capacity %	Shear Capacity %	Pass / Fail				
MP2	Pipe 2.5 STD	54.7	3.8	Pass				
WWM03	HSS4X4X3	3.7	0.9	Pass				
MP1	Pipe 2.0 STD	6.6	1.4	Pass				

# Table 4 - Section Capacity (Summary)

# Table 5 - Connection Capacity (Summary)

Component Type	Size	Capacity %	Pass / Fail
Hilti HY-70 with 4" embedment	1/2" ø Threaded Rods	87.6	Pass
Hilti HY-20 with 6" embedment	5/8" ø Threaded Rods	99.7	Pass
Hilti HY-200 with 5-5/8" embedment	5/8" ø Threaded Rods	35.6	Pass

Notes:

1) See "Appendix A - Mount Analysis Additional Calculations" for additional calculations supporting the % capacity consumed.

Mount Structure Rating (max from all components) =	99.7%	
--	-------	--

# 5] CONCLUSIONS & RECOMMENDATIONS

Based on the performed analysis of the mount structure for applied gravity and lateral loads, the mount structures were determined to have <u>adequate</u> structural capacity per the requirements of the *ANSI/TIA-222-G* standard and the *2015 Uniform Statewide Building Code* to support the proposed T-Mobile antennas and associated equipment. To ensure the requirements of the *ANSI/TIA-222-G* standard and the *2015 Uniform Statewide Building Code* are met with the existing and proposed loading in place, **NB+C ES** has the following recommendation[s]:

- 1. All mount bolts be checked for tightness prior to the installation of the proposed loading and that all rusted hardware be replaced with galvanized hardware.
- The proposed AIR6449 B41 antennas, in Alpha and Beta sectors, will be supported on the existing mount pipes attached to the penthouse wall. The proposed AIR6449 B41 antenna, in Gamma sector, will be supported on the proposed 2.5SCH 40 x 6' LG mount pipe attached to the penthouse wall with Site Pro 1 Standoff arms, P/N: WWM03(typ. of 2) with 5/8" Ø threaded rods & Hilti HIT-HY 200 epoxy, min. 5-5/8" embedment. The proposed AIR6449 B41 antenna, in Delta sector, will be supported on the proposed 2.5SCH 40 x 6' LG mount pipe attached to the penthouse wall with Site Pro 1 flush mounts, P/N: SP250-6(typ. of 2) with (2) 5/8" Ø threaded rods & Hilti HIT-HY 200 epoxy, min. 5-5/8" embedment.
- 3. The existing RFS equipment and proposed radios, in all sectors, will be supported on the **proposed** 2.5SCH40 x 12ft long pipe mounts, attached to the penthouse wall with the existing wall mounts to be reused(typ. of 3).

This engineering analysis is based upon the theoretical capacity of the mount structure. It is not a condition assessment of the mount. If substantial modifications are to be made or the assumptions made in this analysis are not accurate, **NB+C ES** should be notified immediately to perform a revised analysis.

The conclusions reached by **NB+C ES** in this report are only applicable for the previously mentioned existing structural mount members supporting the T-Mobile telecommunications antennas. Furthermore, no structural qualification is made or implied by this report for the existing structural members not supporting the proposed equipment.

# APPENDIX A

# MOUNT ANALYSIS ADDITIONAL CALCULATIONS

100595 T-Mobile T-Mobile White Oak Tower 7WAC050A May 5, 2021



### **Pipe Mount Analysis**

Applicable Codes			
Interational Building Code	2015 Virginia Uniform S	tatewide Building Code	
ASCE Standard	ASCE 7-10		
TIA Standard	ANSI/TI/	4-222-G	
Site Parameters			
Tower Height	81.5	ft	
Mount Centerline Height	79	ft	
Ground Elevation	412.9	ft	
State	VA	-	
County	Fairfax	-	
Basic Wind Speed per ASCE 7-10	115.0	mph	
Maintenance Wind Speed	30	mph	
Ice Wind Speed	30	mph	
Design Ice Thickness	0.75	in	
Design Acceleration, S <sub>ds</sub>	0.129	-	
Exposure Category	В	(B,C, or D)	
Topographic Factor	1	K <sub>zt</sub>	
Tower Type	Rooftop	-	
Risk Category	I	-	
Mount Type	Pipe Mount	-	

#### Rooftop Information

Height above roof	16.33	ft
Parapet Height	0	ft
Horizontal Distance	130.19	ft
Width of Windward Face of Building	61.25	ft
Height of Windward Face of Building	65.16	ft
H <sub>1</sub>	0.0	ft
H <sub>2</sub>	61.3	ft

Wind Parameters per TIA-222-G						
		Parameters				
G <sub>H</sub>	1.00	Gust Factor				
Ka	0.90	Shielding Factor				
Kz	0.92	Velocity Pressure				
Kd	0.95	Wind Direction Probability				
Ks	N/A	Rooftop Wind Speed-up factor				
K <sub>e</sub>	N/A	Ground Elevation factor				
I wind	N/A	Importance Factor (Wind w/o Ice)				
q <sub>z</sub>	29.71	Nominal Wind Pressure (psf)				
q z*Ka	26.74	Design Wind Force (psf)				
q <sub>mz</sub>	2.02	Maintenance Wind Pressure (psf)				
C/D	110.54	(in/in)				
Ice V	/ind Speed F	Parameters				
K <sub>iz</sub>	1.09	Velocity Pressure				
/ Ice	1.00	Importance Factor (Ice)				
t <sub>iz</sub>	1.64	Escalated Ice Thickness (in)				
q <sub>iz</sub>	2.02	Ice Wind Pressure (psf)				
q <sub>iz</sub> *K <sub>a</sub>	1.82	Design Ice Wind Force (psf)				
C/D <sub>iz</sub>	28.84	(in/in)				
S	eismic Para	meters				
/ <sub>seismic</sub>	1.00	Importance Factor				
ρ	1.00	Reducton Factor				
R	2.00	Response Modification Factor				
C <sub>s</sub>	0.06	Seismic Response Coefficient				
A <sub>s</sub>	3.00	Amplification Factor				
E <sub>v</sub>	0.0774*D	Vertical Seismic Effect				
E <sub>h</sub>	0.1935*W	Horizontal Seismic Effect				

#### Appurtenances Table

Manufacturer	Model	Equipment Type	Height	Width	Depth	Weight	Ice Weight	Front FA	Side FA
Manalaotaloi	Model	Equipment Type	(in)	(in)	(in)	(lbs)	(lbs)	(lbs)	(lbs)
Ericsson	AIR6449 B41	Antenna	33.1	20.6	8.3	112	140.51	151.96	64.60
RFS	APXVAALL24_43-U-NA20	Antenna	95.9	24	8.5	122.8	393.03	541.35	233.55
Ericsson	Radio 4449 B71+B85	RRH	17.9	13.19	9.44	71	70.50	52.62	37.66
Ericsson	Radio 4415 B25	RRH	16.5	13.5	5.9	46	55.31	49.64	21.93

#### Dishes Table

Manufacturer	Model	Туре	Diameter(in)	Weight(lbs)	1/2" Ice Weight (lbs)

#### Results

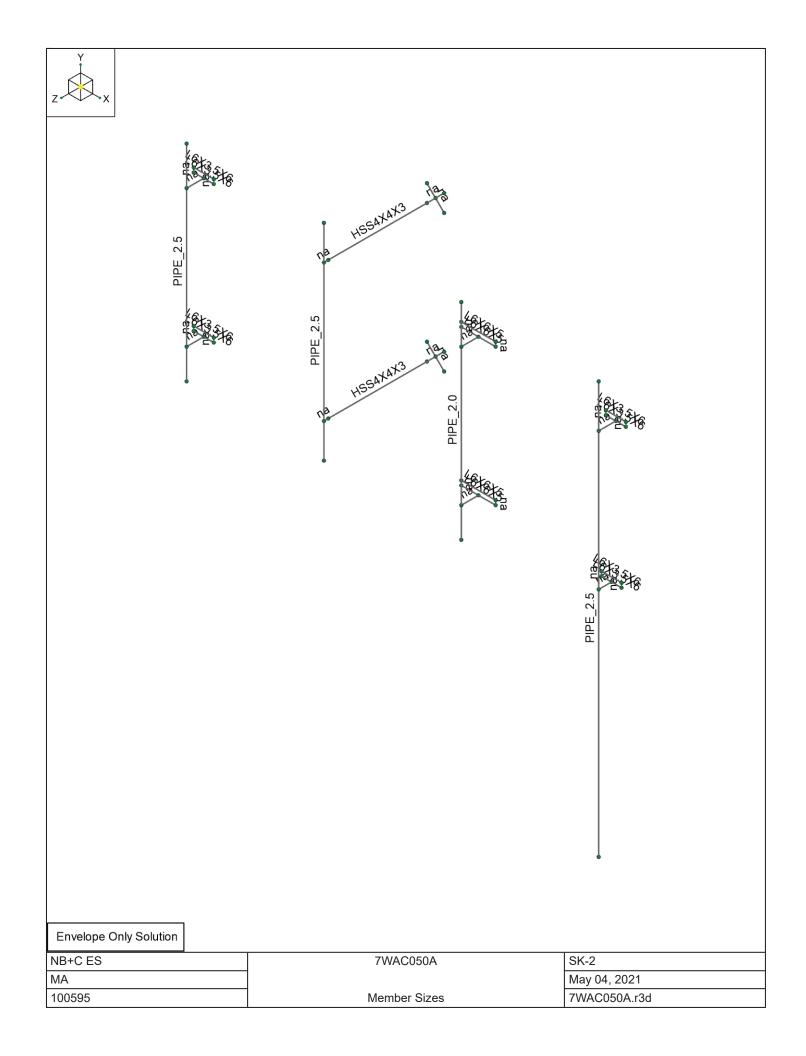
	Member Results		
Member	Unity (Bending)	Shear Check	Pass / Fail
PIPE_2.5	54.7%	3.8%	PASS
L6X3.5X6	3.5%	9.6%	PASS
HSS4X4X3	3.7%	0.9%	PASS
PIPE_2.0	6.6%	1.4%	PASS
L6X6X5	0.6%	1.9%	PASS
	0.0%	0.0%	
	0.0%	0.0%	
	0.0%	0.0%	
	0.0%	0.0%	

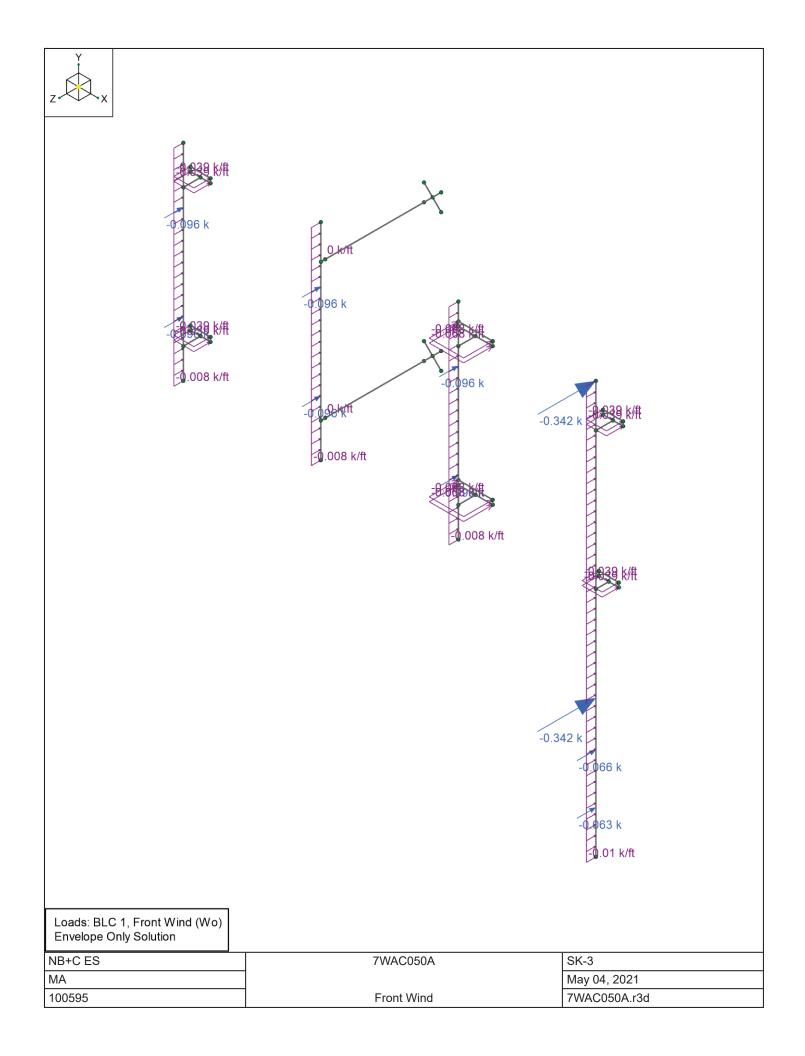
Capacities up to 105% are considered acceptable based on analysis methods used.

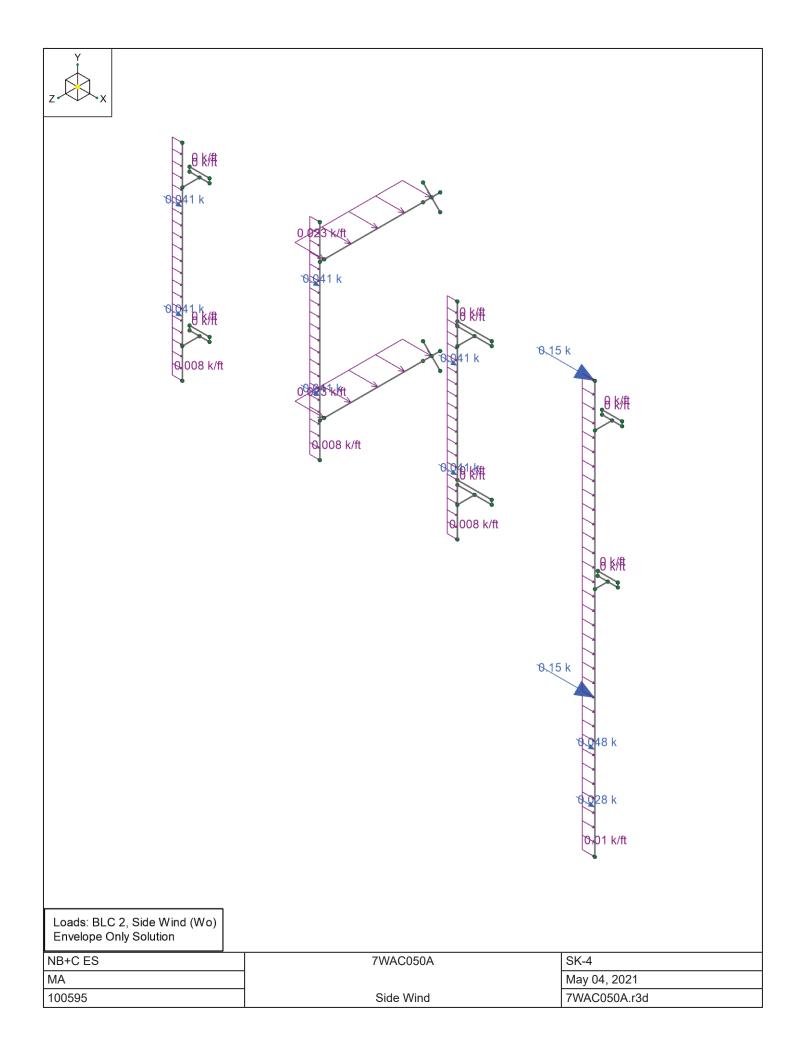
#### Maximum Mount Deflections

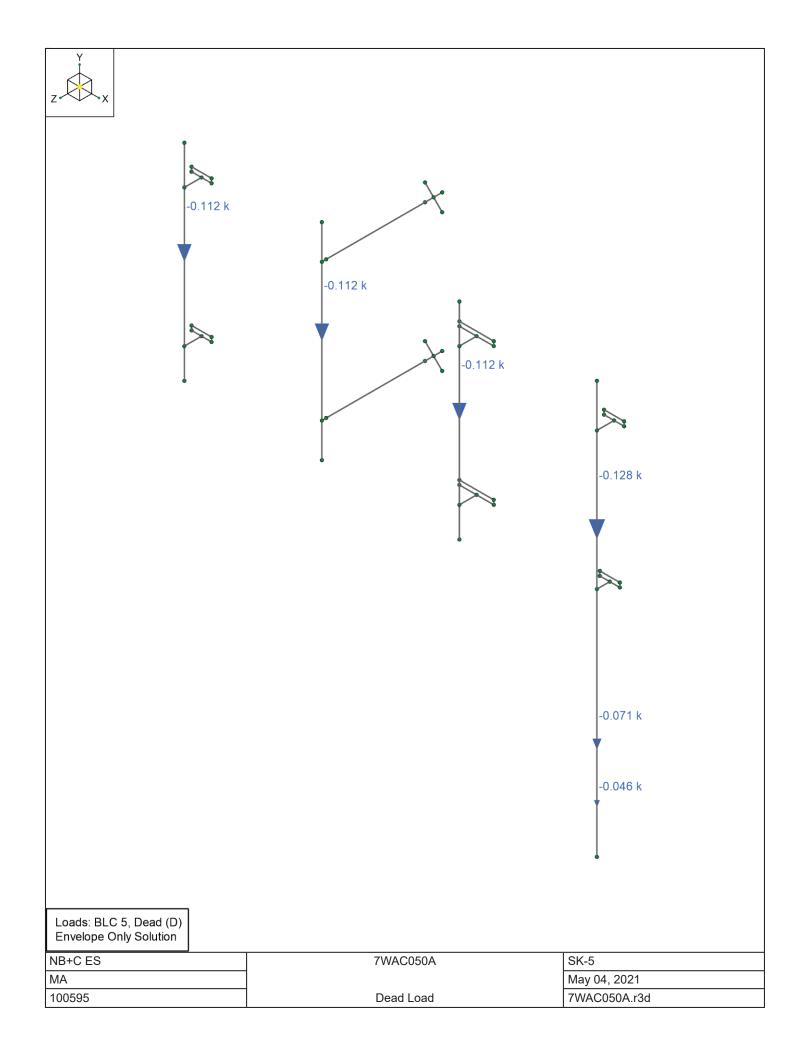
Mount Deflections	;	
Maximum Tilt	0.041	degrees
Maximum Twist	0.189	degrees
Maximum Vertical Deflection	0.009	inches

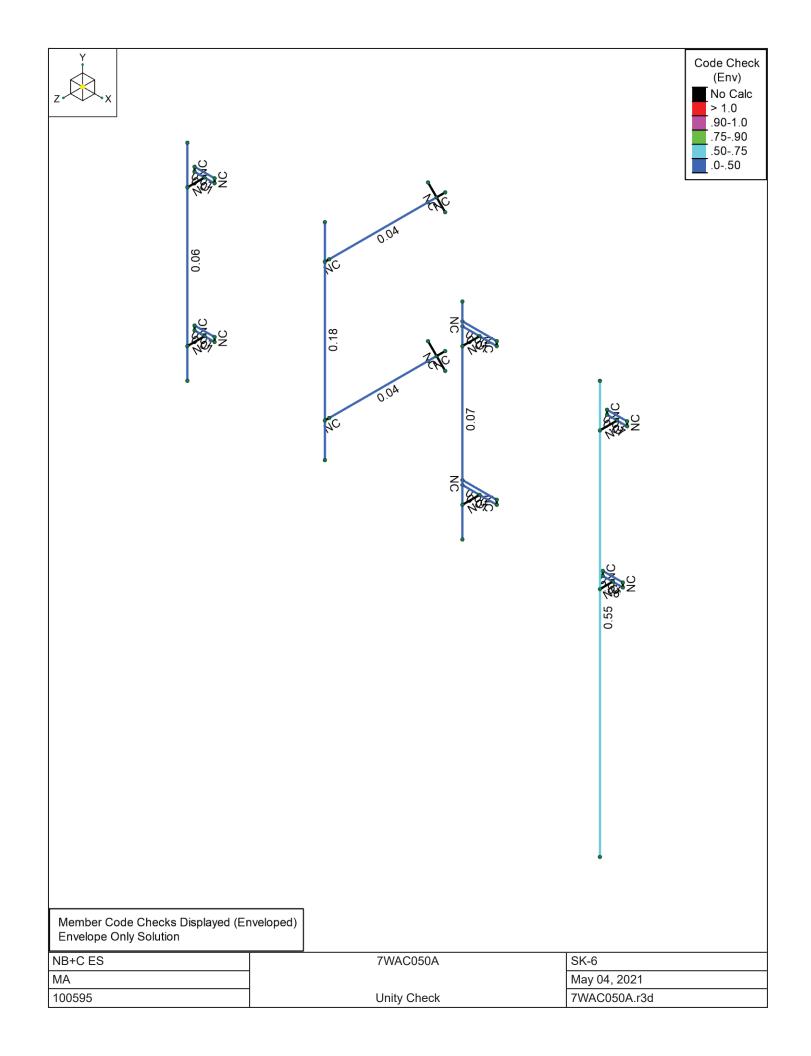
Envelope Only Solution		
NB+C ES MA	7WAC050A	SK-1 May 04, 2021
100595	Rendering	7WAC050A.r3d

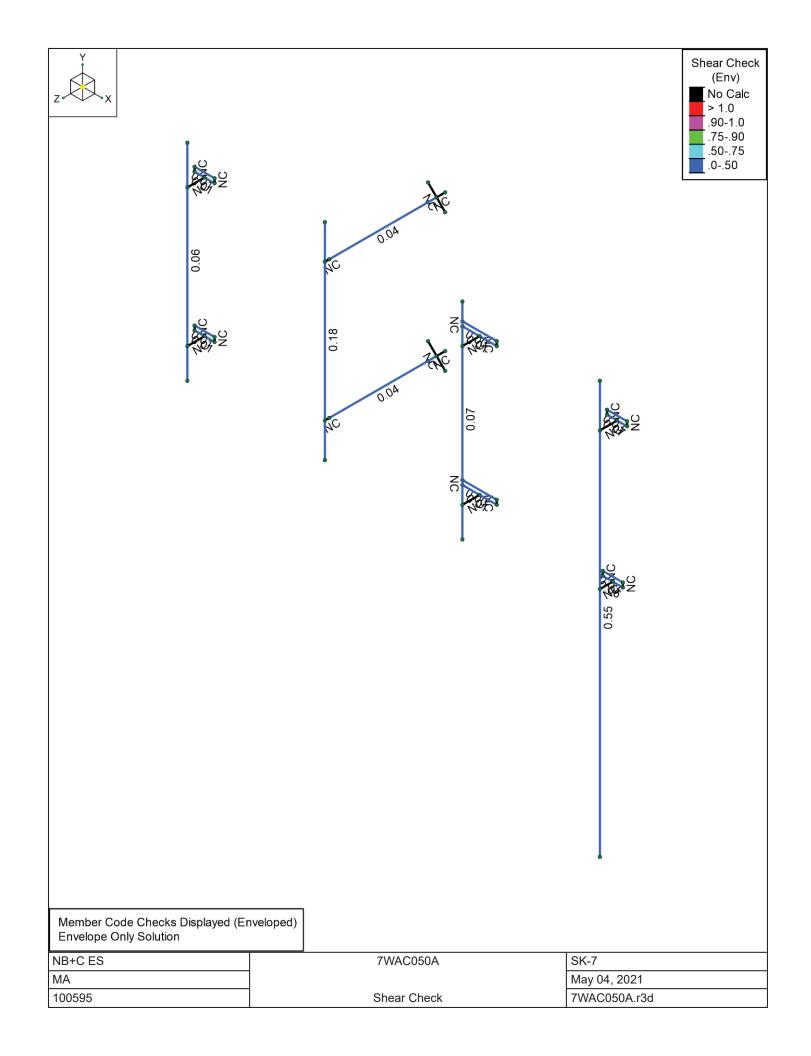














#### Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm. Coeff. [1e⁵°F⁻¹]	Density [k/ft3]	Yield [ksi]	Ry	Fu [ksi]	Rt
1	A992	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
2	A36 Gr.36	29000	11154	0.3	0.65	0.49	36	1.5	58	1.2
3	A572 Gr.50	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
4	A500 Gr.B RND	29000	11154	0.3	0.65	0.527	42	1.4	58	1.3
5	A500 Gr.B Rect	29000	11154	0.3	0.65	0.527	46	1.4	58	1.3
6	A53 Gr.B	29000	11154	0.3	0.65	0.49	35	1.6	60	1.2
7	A1085	29000	11154	0.3	0.65	0.49	50	1.25	65	1.15
8	A913 Gr.65	29000	11154	0.3	0.65	0.49	65	1.1	80	1.1

#### Hot Rolled Steel Section Sets

	Label	Shape	Туре	Design List	Material	Design Rule	Area [in <sup>2</sup> ]	lyy [in⁴]	lzz [in⁴]	J [in⁴]
1	MP1	PIPE_2.0	Column	None	A53 Gr.B	Typical	1.02	0.627	0.627	1.25
2	MP2	PIPE_2.5	Column	None	A53 Gr.B	Typical	1.61	1.45	1.45	2.89
3	MT-222	L6X3.5X6	Beam	None	A36 Gr.36	Typical	3.44	3.33	12.9	0.168
4	WWM03	HSS4X4X3	Beam	None	A500 Gr.B Rect	Typical	2.58	6.21	6.21	10
5	SP250-6	L6X6X5	Beam	None	A36 Gr.36	Typical	3.67	13	13	0.129

#### Node Coordinates

	Label	X [in]	Y [in]	Z [in]	Detach From Diaphragm
1	N1	0	72	0	
2	N2	0	144	0	
3	N3	0	82.5	0	
4	N4	0	130.5	0	
5	N6	0	130.5	-6	
6	N7	0	82.5	-6	
7	N8	-3.5	130.5	-6	
8	N9	3.5	130.5	-6	
9	N10	3.5	82.5	-6	
10	N11	-3.5	82.5	-6	
11	N12	3.5	132	-6	
12	N13	-3.5	132	-6	
13	N14	3.5	84	-6	
14	N15	-3.5	84	-6	
15	N16	144	0	0	
16	N17	144	144	0	
17	N18	144	129	0	
18	N19	144	81	0	
19	N20	144	129	-6	
20	N21	144	81	-4.5	
21	N22	140.5	129	-6	
22	N23	147.5	129	-6	
23	N24	147.5	81	-4.5	
24	N25	140.5	81	-4.5	
25	N26	140.5	130.5	-6	
26	N27	147.5	130.5	-6	
27	N28	140.5	82.5	-4.5	
28	N29	147.5	82.5	-4.5	
29	N30	48	72	0	
30	N31	48	144	0	
31	N32	48	132	0	
32	N33	48	132	-1.5	
33	N34	48	84	0	
34	N35	48	84	-1.5	
35	N36	48	132	-39	
36	N37	51	135	-39	
37	N38	45	135	-39	
38	N39	51	129	-39	



#### Node Coordinates (Continued)

	Label	X [in]	Y [in]	Z [in]	Detach From Diaphragm
39	N40	45	129	-39	
40	N41	51	87	-39	
41	N42	51	81	-39	
42	N43	45	87	-39	
43	N44	48	84	-39	
44	N45	45	81	-39	
45	N48	96	72	0	
46	N49	96	144	0	
47	N50	96	130.5	0	
48	N51	96	130.5	-6	
49	N52	102	130.5	-6	
50	N53	90	130.5	-6	
51	N54	90	132	-6	
52	N55	102	132	-6	
53	N58	90	82.5	-6	
54	N59	96	82.5	-6	
55	N60	102	82.5	-6	
56	N61	90	84	-6	
57	N62	102	84	-6	
58	N63	96	82.5	0	

#### **Basic Load Cases**

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Point	Distributed
1	Front Wind (Wo)	None				10	18
2	Side Wind (Wo)	None				10	18
3	Front Ice Wind (Wi)	None				10	18
4	Side Ice Wind (Wi)	None				10	39
5	Dead (D)	None		-1		6	
6	Ice Dead (Di)	None				6	18
7	Front Seismic	None			-1	6	
8	Side Seismic	None	-1			6	
9	Maintenance 1 (Lm)	None					
10	Maintenance 2 (Lm)	None					
11	Maintenance 3 (Lm)	None					
12	Maintenance 4 (Lm)	None					
13	Maintenance 1 (Lv)	None					
14	Maintenance 2 (Lv)	None					
15	Maintenance 3 (Lv)	None					
16	Maintenance 4 (Lv)	None					

#### Member Point Loads

	Member Label	Direction	Magnitude [k, k-ft]	Location [(in, %)]	Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]
1	ALL SECTORS	Z	-0.342	%100	Active
2	ALPHA/BETA	Z	-0.096	%73	Active
3	GAMMA	Z	-0.096	%73	Active
4	DELTA	Z	-0.096	%73	Active
5	ALL SECTORS	Z	-0.342	%33.4	Active
6	ALPHA/BETA	Z	-0.096	%27	Active
7	GAMMA	Z	-0.096	%27	Active
8	DELTA	Z	-0.096	%27	Active
9	ALL SECTORS	Z	-0.066	%22.5	Active
10	ALL SECTORS	Z	-0.063	%10.4	Active

#### Member Point Loads

1     ALL SECTORS     X     0.15     %100     Active       2     AL DHA/RETA     X     0.041     %72     Active		Member Label	Direction	Magnitude [k, k-ft]	Location [(in, %)]	Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]
	1	ALL SECTORS	Х	0.15	%100	Active
Z ALFHA/DETA A 0.041 7075 Active	2	ALPHA/BETA	Х	0.041	%73	Active



#### Member Point Loads (Continued)

	Member Label	Direction	Magnitude [k, k-ft]	Location [(in, %)]	Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]
3	GAMMA	Х	0.041	%73	Active
4	DELTA	Х	0.041	%73	Active
5	ALL SECTORS	X	0.15	%33.4	Active
6	ALPHA/BETA	Х	0.041	%27	Active
7	GAMMA	Х	0.041	%27	Active
8	DELTA	Х	0.041	%27	Active
9	ALL SECTORS	Х	0.048	%22.5	Active
10	ALL SECTORS	Х	0.028	%10.4	Active

#### Member Point Loads

_	Member Label	Direction	Magnitude [k, k-ft]	Location [(in, %)]	Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]
1	ALL SECTORS	Z	-0.027	%100	Active
2	ALPHA/BETA	Z	-0.008	%73	Active
3	GAMMA	Z	-0.008	%73	Active
4	DELTA	Z	-0.008	%73	Active
5	ALL SECTORS	Z	-0.027	%33.4	Active
6	ALPHA/BETA	Z	-0.008	%27	Active
7	GAMMA	Z	-0.008	%27	Active
8	DELTA	Z	-0.008	%27	Active
9	ALL SECTORS	Z	-0.007	%22.5	Active
10	ALL SECTORS	Z	-0.006	%10.4	Active

#### Member Point Loads

	Member Label	Direction	Magnitude [k, k-ft]	Location [(in, %)]	Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]
1	ALL SECTORS	Х	0.014	%100	Active
2	ALPHA/BETA	Х	0.004	%73	Active
3	GAMMA	X	0.004	%73	Active
4	DELTA	Х	0.004	%73	Active
5	ALL SECTORS	Х	0.014	%33.4	Active
6	ALPHA/BETA	Х	0.004	%27	Active
7	GAMMA	Х	0.004	%27	Active
8	DELTA	Х	0.004	%27	Active
9	ALL SECTORS	Х	0.007	%22.5	Active
10	ALL SECTORS	Х	0.006	%10.4	Active

## Member Point Loads

	Member Label	Direction	Magnitude [k, k-ft]	Location [(in, %)]	Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]
1	ALL SECTORS	Y	-0.128	%66.7	Active
2	ALPHA/BETA	Y	-0.112	%50	Active
3	GAMMA	Y	-0.112	%50	Active
4	DELTA	Y	-0.112	%50	Active
5	ALL SECTORS	Y	-0.071	%22.5	Active
6	ALL SECTORS	Ý	-0.046	%10.4	Active

#### Member Point Loads

	Member Label	Direction	Magnitude [k, k-ft]	Location [(in, %)]	Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]
1	ALL SECTORS	Y	-0.396	%66.7	Active
2	ALPHA/BETA	Y	-0.141	%50	Active
3	GAMMA	Y	-0.141	%50	Active
4	DELTA	Y	-0.141	%50	Active
5	ALL SECTORS	Ý	-0.071	%22.5	Active
6	ALL SECTORS	Y	-0.055	%10.4	Active



#### Member Point Loads

	Member Label	Direction	Magnitude [k, k-ft]	Location [(in, %)]	Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]
1	ALL SECTORS	Z	-0.128	%66.7	Active
2	ALPHA/BETA	Z	-0.112	%50	Active
3	GAMMA	Z	-0.112	%50	Active
4	DELTA	Z	-0.112	%50	Active
5	ALL SECTORS	Z	-0.071	%22.5	Active
6	ALL SECTORS	Z	-0.046	%10.4	Active

#### Member Point Loads

	Member Label	Direction	Magnitude [k, k-ft]	Location [(in, %)]	Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]
1	ALL SECTORS	Х	0.128	%66.7	Active
2	ALPHA/BETA	Х	0.112	%50	Active
3	GAMMA	Х	0.112	%50	Active
4	DELTA	Х	0.112	%50	Active
5	ALL SECTORS	Х	0.071	%22.5	Active
6	ALL SECTORS	Х	0.046	%10.4	Active

#### Member Distributed Loads

	Member Label Direction Start Magnitude [k/ft, F, ksf] End Magnitude [k/ft, F, ksf] Start Location [(in, %)] End Location [(in, %)] Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]									
1	ALL SECTORS	ΡZ	-0.01	-0.01	0	%100	Active			
2	ALPHA/BETA	ΡZ	-0.008	-0.008	0	%100	Active			
3	DELTA	ΡZ	-0.008	-0.008	0	%100	Active			
4	GAMMA	ΡZ	-0.008	-0.008	0	%100	Active			
5	M13	ΡZ	-0.039	-0.039	0	%100	Active			
6	M14	ΡZ	-0.039	-0.039	0	%100	Active			
7	M15	ΡZ	-0.039	-0.039	0	%100	Active			
8	M16	ΡZ	-0.039	-0.039	0	%100	Active			
9	M2	ΡZ	-0.039	-0.039	0	%100	Active			
10	M26	ΡZ	-0.023	-0.023	0	%100	Active			
11	M3	ΡZ	-0.039	-0.039	0	%100	Active			
12	M31	ΡZ	-0.023	-0.023	0	%100	Active			
13	M35	ΡZ	-0.068	-0.068	0	%100	Active			
14	M36	ΡZ	-0.068	-0.068	0	%100	Active			
15	M39	ΡZ	-0.068	-0.068	0	%100	Active			
16	M4	ΡZ	-0.039	-0.039	0	%100	Active			
17	M40	ΡZ	-0.068	-0.068	0	%100	Active			
18	M5	ΡZ	-0.039	-0.039	0	%100	Active			

#### Member Distributed Loads

	Member Label Direction Start Magnitude [k/ft, F, ksf] End Magnitude [k/ft, F, ksf] Start Location [(in, %)] End Location [(in, %)] Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]									
1	ALL SECTORS	PX	0.01	0.01	0	%100	Active			
2	ALPHA/BETA	PX	0.008	0.008	0	%100	Active			
3	DELTA	PX	0.008	0.008	0	%100	Active			
4	GAMMA	PX	0.008	0.008	0	%100	Active			
5	M13	PX	0.039	0.039	0	%100	Active			
6	M14	PX	0.039	0.039	0	%100	Active			
7	M15	PX	0.039	0.039	0	%100	Active			
8	M16	PX	0.039	0.039	0	%100	Active			
9	M2	PX	0.039	0.039	0	%100	Active			
10	M26	PX	0.023	0.023	0	%100	Active			
11	M3	PX	0.039	0.039	0	%100	Active			
12	M31	PX	0.023	0.023	0	%100	Active			
13	M35	PX	0.068	0.068	0	%100	Active			
14	M36	PX	0.068	0.068	0	%100	Active			
15	M39	PX	0.068	0.068	0	%100	Active			
16	M4	PX	0.039	0.039	0	%100	Active			
17	M40	PX	0.068	0.068	0	%100	Active			
18	M5	PX	0.039	0.039	0	%100	Active			



#### Member Distributed Loads

	Member Label Direction Start Magnitude [k/ft, F, ksf] End Magnitude [k/ft, F, ksf] Start Location [(in, %)] End Location [(in, %)] Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]									
1	ALL SECTORS	ΡZ	-0.001	-0.001	0	%100	Active			
2	ALPHA/BETA	ΡZ	-0.001	-0.001	0	%100	Active			
3	DELTA	ΡZ	-0.001	-0.001	0	%100	Active			
4	GAMMA	ΡZ	-0.001	-0.001	0	%100	Active			
5	M13	ΡZ	-0.002	-0.002	0	%100	Active			
6	M14	ΡZ	-0.002	-0.002	0	%100	Active			
7	M15	ΡZ	-0.002	-0.002	0	%100	Active			
8	M16	ΡZ	-0.002	-0.002	0	%100	Active			
9	M2	ΡZ	-0.002	-0.002	0	%100	Active			
10	M26	ΡZ	-0.001	-0.001	0	%100	Active			
11	M3	ΡZ	-0.002	-0.002	0	%100	Active			
12	M31	ΡZ	-0.001	-0.001	0	%100	Active			
13	M35	ΡZ	-0.003	-0.003	0	%100	Active			
14	M36	ΡZ	-0.003	-0.003	0	%100	Active			
15	M39	ΡZ	-0.003	-0.003	0	%100	Active			
16	M4	ΡZ	-0.002	-0.002	0	%100	Active			
17	M40	ΡZ	-0.003	-0.003	0	%100	Active			
18	M5	ΡZ	-0.002	-0.002	0	%100	Active			

#### Member Distributed Loads

	Member Label Direction Start Magnitude [k/ft, F, ksf] End Magnitude [k/ft, F, ksf] Start Location [(in, %)] End Location [(in, %)] Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]									
	ALL SECTORS	PX	0.001	0.001		%100	Active			
	ALPHA/BETA	PX	0.001	0.001	0	%100	Active			
3	DELTA	PX	0.001	0.001	0	%100	Active			
4	GAMMA	PX	0.001	0.001	0	%100	Active			
5	M13	PX	0.002	0.002	0	%100	Active			
6	M14	PX	0.002	0.002	0	%100	Active			
7	M15	PX	0.002	0.002	0	%100	Active			
8	M16	PX	0.002	0.002	0	%100	Active			
9	M2	PX	0.002	0.002	0	%100	Active			
10	M26	PX	0.001	0.001	0	%100	Active			
11	M3	PX	0.002	0.002	0	%100	Active			
12	M31	PX	0.001	0.001	0	%100	Active			
13	M35	PX	0.003	0.003	0	%100	Active			
14	M36	PX	0.003	0.003	0	%100	Active			
15	M39	PX	0.003	0.003	0	%100	Active			
16	M4	PX	0.002	0.002	0	%100	Active			
17	M40	PX	0.003	0.003	0	%100	Active			
18	M5	PX	0.002	0.002	0	%100	Active			
19	M39	PX	0.003	0.003	0	%100	Active			
20	M4	PX	0.002	0.002	0	%100	Active			
21	M40	PX	0.003	0.003	0	%100	Active			
22	ALL SECTORS	PX	0.001	0.001	0	%100	Active			
23	ALPHA/BETA	PX	0.001	0.001	0	%100	Active			
24	DELTA	PX	0.001	0.001	0	%100	Active			
25	GAMMA	PX	0.001	0.001	0	%100	Active			
26	M13	PX	0.002	0.002	0	%100	Active			
27	M14	PX	0.002	0.002	0	%100	Active			
28	M15	PX	0.002	0.002	0	%100	Active			
29	M16	PX	0.002	0.002	0	%100	Active			
30	M2	PX	0.002	0.002	0	%100	Active			
31	M26	ΡX	0.001	0.001	0	%100	Active			
32	M3	PX	0.002	0.002	0	%100	Active			
33	M31	PX	0.001	0.001	0	%100	Active			
34	M35	PX	0.003	0.003	0	%100	Active			
35	M36	PX	0.003	0.003	0	%100	Active			
36	M39	PX	0.003	0.003	0	%100	Active			
37	M4	PX	0.002	0.002	0	%100	Active			

#### Member Distributed Loads (Continued)

	Member Label Direction Start Magnitude [k/ft, F, ksf] End Magnitude [k/ft, F, ksf] Start Location [(in, %)] End Location [(in, %)] Inactive [(k, k-ft), (in, rad), (k*s <sup>2</sup> /in, k*s <sup>2*</sup> in)]									
38	M40	PX	0.003	0.003	0	%100	Active			
39	M5	PX	0.002	0.002	0	%100	Active			

#### Member Distributed Loads

	Member Label Direction Start Magnitude [k/ft, F, ksf] End Magnitude [k/ft, F, ksf] Start Location [(in, %)] End Location [(in, %)] Inactive [(k, k-ft), (in, rad), (k*s²/in, k*s²*in)]									
1	ALL SECTORS	Y	-0.009	-0.009	0	%100	Active			
2	ALPHA/BETA	Y	-0.008	-0.008	0	%100	Active			
3	DELTA	Y	-0.008	-0.008	0	%100	Active			
4	GAMMA	Y	-0.008	-0.008	0	%100	Active			
5	M13	Y	-0.019	-0.019	0	%100	Active			
6	M14	Y	-0.019	-0.019	0	%100	Active			
7	M15	Y	-0.019	-0.019	0	%100	Active			
8	M16	Y	-0.019	-0.019	0	%100	Active			
9	M2	Y	-0.019	-0.019	0	%100	Active			
10	M26	Y	-0.015	-0.015	0	%100	Active			
11	M3	Y	-0.019	-0.019	0	%100	Active			
12	M31	Y	-0.015	-0.015	0	%100	Active			
13	M35	Y	-0.03	-0.03	0	%100	Active			
14	M36	Y	-0.03	-0.03	0	%100	Active			
15	M39	Y	-0.03	-0.03	0	%100	Active			
16	M4	Y	-0.019	-0.019	0	%100	Active			
17	M40	Y	-0.03	-0.03	0	%100	Active			
18	M5	Y	-0.019	-0.019	0	%100	Active			

#### Load Combinations

$\begin{array}{c c c c c c c c c c c c c c c c c c c $		Description	Solve	PDelta	BLC	Factor	BLC	Factor	BLC	Factor	BLC	Factor
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	1	1.4D	Yes		5	1.4						
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	2	1.2D + 1.5Lv1	Yes		5	1.2	13	1.5				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	3	1.2D + 1.5Lv2	Yes		5	1.2		1.5				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		1.2D + 1.5Lv3	Yes					1.5				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		1.2D + 1.5Lv4	Yes	Y	5	1.2	16	1.5				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	6	***WIND***										
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	7	1.2D + 1.0Wo (0°)	Yes		5	1.2	1	1				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			Yes			1.2	1	0.866		0.5		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1.2D + 1.0Wo (45°)	Yes			1.2	1	0.707	2	0.707		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	1.2D + 1.0Wo (60°)	Yes				1	0.5		0.866		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	1.2D + 1.0Wo (90°)	Yes	Y		1.2			2	1		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	12	1.2D + 1.0Wo (120°)	Yes		5	1.2	1	-0.5	2	0.866		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	1.2D + 1.0Wo (135°)			5		1	-0.707	2	0.707		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	1.2D + 1.0Wo (150°)	Yes		5	1.2	1	-0.866	2	0.5		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15	1.2D + 1.0Wo (180°)	Yes		5	1.2	1	-1				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1.2D + 1.0Wo (210°)	Yes			1.2	1	-0.866	2	-0.5		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	17	1.2D + 1.0Wo (225°)	Yes		5	1.2	1	-0.707	2	-0.707		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	18	1.2D + 1.0Wo (240°)	Yes		5	1.2	1	-0.5	2	-0.866		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	1.2D + 1.0Wo (270°)	Yes		5	1.2			2	-1		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	1.2D + 1.0Wo (330°)	Yes				1	0.5	2	-0.866		
23       ***ICE***       24       1.2D + 1.0Di + 1.0Wi (0°)       Yes       Y       5       1.2       6       1       3       1         24       1.2D + 1.0Di + 1.0Wi (30°)       Yes       Y       5       1.2       6       1       3       1         25       1.2D + 1.0Di + 1.0Wi (30°)       Yes       Y       5       1.2       6       1       3       0.866       4       0.5         26       1.2D + 1.0Di + 1.0Wi (45°)       Yes       Y       5       1.2       6       1       3       0.707       4       0.707         27       1.2D + 1.0Di + 1.0Wi (60°)       Yes       Y       5       1.2       6       1       3       0.5       4       0.866         28       1.2D + 1.0Di + 1.0Wi (90°)       Yes       Y       5       1.2       6       1       3       -0.5       4       0.866         28       1.2D + 1.0Di + 1.0Wi (120°)       Yes       Y       5       1.2       6       1       3       -0.5       4       0.866         30       1.2D + 1.0Di + 1.0Wi (135°)       Yes       Y       5       1.2       6       1       3       -0.707       4       0.707	21	1.2D + 1.0Wo (315°)	Yes	Y	5	1.2	1	0.707	2	-0.707		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22		Yes	Y	5	1.2	1	0.866	2	-0.5		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	23	***ICE***										
26       1.2D + 1.0Di + 1.0Wi (45°)       Yes       Y       5       1.2       6       1       3       0.707       4       0.707         27       1.2D + 1.0Di + 1.0Wi (60°)       Yes       Y       5       1.2       6       1       3       0.5       4       0.866         28       1.2D + 1.0Di + 1.0Wi (90°)       Yes       Y       5       1.2       6       1       3       0.5       4       0.866         28       1.2D + 1.0Di + 1.0Wi (120°)       Yes       Y       5       1.2       6       1       3       -0.5       4       0.866         30       1.2D + 1.0Di + 1.0Wi (120°)       Yes       Y       5       1.2       6       1       3       -0.5       4       0.866         30       1.2D + 1.0Di + 1.0Wi (135°)       Yes       Y       5       1.2       6       1       3       -0.707       4       0.707         31       1.2D + 1.0Di + 1.0Wi (150°)       Yes       Y       5       1.2       6       1       3       -0.866       4       0.5	24	1.2D + 1.0Di + 1.0Wi (0°)	Yes		5	1.2	6	1	3	1		
27       1.2D + 1.0Di + 1.0Wi (60°)       Yes       Y       5       1.2       6       1       3       0.5       4       0.866         28       1.2D + 1.0Di + 1.0Wi (90°)       Yes       Y       5       1.2       6       1       3       0.5       4       0.866         28       1.2D + 1.0Di + 1.0Wi (90°)       Yes       Y       5       1.2       6       1       3       -0.5       4       1         29       1.2D + 1.0Di + 1.0Wi (120°)       Yes       Y       5       1.2       6       1       3       -0.5       4       0.866         30       1.2D + 1.0Di + 1.0Wi (135°)       Yes       Y       5       1.2       6       1       3       -0.707       4       0.707         31       1.2D + 1.0Di + 1.0Wi (150°)       Yes       Y       5       1.2       6       1       3       -0.866       4       0.5	25	1.2D + 1.0Di + 1.0Wi (30°)	Yes		5	1.2	6	1	3	0.866	4	0.5
28         1.2D + 1.0Di + 1.0Wi (90°)         Yes         Y         5         1.2         6         1         4         1           29         1.2D + 1.0Di + 1.0Wi (120°)         Yes         Y         5         1.2         6         1         3         -0.5         4         0.866           30         1.2D + 1.0Di + 1.0Wi (135°)         Yes         Y         5         1.2         6         1         3         -0.707         4         0.707           31         1.2D + 1.0Di + 1.0Wi (150°)         Yes         Y         5         1.2         6         1         3         -0.866         4         0.5	26	1.2D + 1.0Di + 1.0Wi (45°)	Yes	Y	5	1.2	6	1	3	0.707	4	0.707
29         1.2D + 1.0Di + 1.0Wi (120°)         Yes         Y         5         1.2         6         1         3         -0.5         4         0.866           30         1.2D + 1.0Di + 1.0Wi (135°)         Yes         Y         5         1.2         6         1         3         -0.707         4         0.707           31         1.2D + 1.0Di + 1.0Wi (150°)         Yes         Y         5         1.2         6         1         3         -0.866         4         0.5	27	1.2D + 1.0Di + 1.0Wi (60°)	Yes	Y	5	1.2	6	1	3	0.5	4	0.866
30         1.2D + 1.0Di + 1.0Wi (135°)         Yes         Y         5         1.2         6         1         3         -0.707         4         0.707           31         1.2D + 1.0Di + 1.0Wi (150°)         Yes         Y         5         1.2         6         1         3         -0.866         4         0.5	28	1.2D + 1.0Di + 1.0Wi (90°)	Yes		5	1.2	6	1			4	1
31 1.2D + 1.0Di + 1.0Wi (150°) Yes Y 5 1.2 6 1 3 -0.866 4 0.5	29	1.2D + 1.0Di + 1.0Wi (120°)	Yes		5	1.2	6	1	3	-0.5	4	0.866
	30	1.2D + 1.0Di + 1.0Wi (135°)	Yes			1.2	6	1	3	-0.707	4	0.707
	31	1.2D + 1.0Di + 1.0Wi (150°)	Yes		5	1.2	6	1	3	-0.866	4	0.5
	32	1.2D + 1.0Di + 1.0Wi (180°)	Yes	Y		1.2	6	1	3	-1		



5/4/2021 5:17:14 PM Checked By : \_\_\_

#### Load Combinations (Continued)

Description	Solve	PDelta	BLC	Factor	BLC	Factor	BLC	Factor	BLC	Factor
32 1.2D + 1.0Di + 1.0Wi (180°)	Yes	Y	5	1.2	6	1	3	-1		
33 1.2D + 1.0Di + 1.0Wi (210°)	Yes	Y	5	1.2	6	1	3	-0.866	4	-0.5
					-			-		-
34 1.2D + 1.0Di + 1.0Wi (225°)	Yes	Y	5	1.2	6	1	3	-0.707	4	-0.707
35 1.2D + 1.0Di + 1.0Wi (240°)	Yes	Y	5	1.2	6	1	3	-0.5	4	-0.866
36 1.2D + 1.0Di + 1.0Wi (270°)	Yes	Y	5	1.2	6	1			4	-1
37 1.2D + 1.0Di + 1.0Wi (300°)	Yes	Y	5	1.2	6	1	3	0.5	4	-0.866
38 1.2D + 1.0Di + 1.0Wi (315°)	Yes	Y	5	1.2	6	1	3	0.707	4	-0.707
39 1.2D + 1.0Di + 1.0Wi (330°)	Yes	Y	5	1.2	6	1	3	0.866	4	-0.5
40 ***MAINTENANCE***	163			1.2	0	- 1	5	0.000		-0.5
				1.0		4 -		0.000	-	
41 1.2D + 1.5Lm + 1.0Wm (0°)	Yes	Y	5	1.2	9	1.5	1	0.068		
42 1.2D + 1.5Lm + 1.0Wm (30°)	Yes	Y	5	1.2	9	1.5	1	0.059	2	0.034
43 1.2D + 1.5Lm + 1.0Wm (45°)	Yes	Y	5	1.2	9	1.5	1	0.048	2	0.048
44 1.2D + 1.5Lm + 1.0Wm (60°)	Yes	Y	5	1.2	9	1.5	1	0.034	2	0.059
45 1.2D + 1.5Lm + 1.0Wm (90°)	Yes	Y	5	1.2	9	1.5			2	0.068
46 1.2D + 1.5Lm + 1.0Wm (120°)	Yes	Y	5	1.2	9	1.5	1	-0.034	2	0.059
47 1.2D + 1.5Lm + 1.0Wm (135°)	Yes	Y		1.2		1.5				0.048
			5		9		1	-0.048	2	
48 1.2D + 1.5Lm + 1.0Wm (150°)	Yes	Y	5	1.2	9	1.5	1	-0.059	2	0.034
49 1.2D + 1.5Lm + 1.0Wm (180°)	Yes	Y	5	1.2	9	1.5	1	-0.068		
50 1.2D + 1.5Lm + 1.0Wm (210°)	Yes	Y	5	1.2	9	1.5	1	-0.059	2	-0.034
51 1.2D + 1.5Lm + 1.0Wm (225°)	Yes	Y	5	1.2	9	1.5	1	-0.048	2	-0.048
52 1.2D + 1.5Lm + 1.0Wm (240°)	Yes	Y	5	1.2	9	1.5	1	-0.034	2	-0.059
53 1.2D + 1.5Lm + 1.0Wm (270°)	Yes	Y	5	1.2	9	1.5	· ·	0.001	2	-0.068
54 1.2D + 1.5Lm + 1.0Wm (300°)	Yes	Y	5	1.2	9	1.5	1	0.034	2	-0.059
	-						_			
55 1.2D + 1.5Lm + 1.0Wm (315°)	Yes	Y	5	1.2	9	1.5	1	0.048	2	-0.048
56 1.2D + 1.5Lm + 1.0Wm (330°)	Yes	Y	5	1.2	9	1.5	1	0.059	2	-0.034
57 1.2D + 1.5Lm + 1.0Wm (0°)	Yes	Y	5	1.2	10	1.5	1	0.068		
58 1.2D + 1.5Lm + 1.0Wm (30°)	Yes	Y	5	1.2	10	1.5	1	0.059	2	0.034
59 1.2D + 1.5Lm + 1.0Wm (45°)	Yes	Y	5	1.2	10	1.5	1	0.048	2	0.048
$60 \ 1.2D + 1.5Lm + 1.0Wm \ (60^{\circ})$	Yes	Y	5	1.2	10	1.5	1	0.034	2	0.059
$61 1.2D + 1.5Lm + 1.0Wm (90^{\circ})$	Yes	Y	5	1.2	10	1.5		0.001	2	0.068
		Y					4	0.024		
62 1.2D + 1.5Lm + 1.0Wm (120°)	Yes		5	1.2	10	1.5	1	-0.034	2	0.059
63 1.2D + 1.5Lm + 1.0Wm (135°)	Yes	Y	5	1.2	10	1.5	1	-0.048	2	0.048
64 1.2D + 1.5Lm + 1.0Wm (150°)	Yes	Y	5	1.2	10	1.5	1	-0.059	2	0.034
65 1.2D + 1.5Lm + 1.0Wm (180°)	Yes	Y	5	1.2	10	1.5	1	-0.068		
66 1.2D + 1.5Lm + 1.0Wm (210°)	Yes	Y	5	1.2	10	1.5	1	-0.059	2	-0.034
67 1.2D + 1.5Lm + 1.0Wm (225°)	Yes	Y	5	1.2	10	1.5	1	-0.048	2	-0.048
68 1.2D + 1.5Lm + 1.0Wm (240°)	Yes	Y	5	1.2	10	1.5	1	-0.034	2	-0.059
69 1.2D + 1.5Lm + 1.0Wm (270°)	Yes	Y	5	1.2	10	1.5		-0.034		-0.068
							4	0.004	2	
70 1.2D + 1.5Lm + 1.0Wm (300°)	Yes	Y	5	1.2	10	1.5	1	0.034	2	-0.059
71 1.2D + 1.5Lm + 1.0Wm (315°)	Yes	Y	5	1.2	10	1.5	1	0.048	2	-0.048
72 1.2D + 1.5Lm + 1.0Wm (330°)	Yes	Y	5	1.2	10	1.5	1	0.059	2	-0.034
73 1.2D + 1.5Lm + 1.0Wm (0°)	Yes	Y	5	1.2	11	1.5	1	0.068		
74 1.2D + 1.5Lm + 1.0Wm (30°)	Yes	Y	5	1.2	11	1.5	1	0.059	2	0.034
$75 1.2D + 1.5Lm + 1.0Wm (45^{\circ})$	Yes	Y	5	1.2	11	1.5	1	0.048	2	0.048
$76 1.2D + 1.5Lm + 1.0Wm (60^{\circ})$	Yes	Y	5	1.2	11	1.5	1	0.040	2	0.059
		Y Y					I	0.034		
$77 1.2D + 1.5Lm + 1.0Wm (90^{\circ})$	Yes		5	1.2	11	1.5		0.004	2	0.068
78 1.2D + 1.5Lm + 1.0Wm (120°)	Yes	Y	5	1.2	11	1.5	1	-0.034	2	0.059
79 1.2D + 1.5Lm + 1.0Wm (135°)	Yes	Y	5	1.2	11	1.5	1	-0.048	2	0.048
80 1.2D + 1.5Lm + 1.0Wm (150°)	Yes	Y	5	1.2	11	1.5	1	-0.059	2	0.034
81 1.2D + 1.5Lm + 1.0Wm (180°)	Yes	Y	5	1.2	11	1.5	1	-0.068		
82 1.2D + 1.5Lm + 1.0Wm (210°)	Yes	Y	5	1.2	11	1.5	1	-0.059	2	-0.034
83 1.2D + 1.5Lm + 1.0Wm (225°)	Yes	Y	5	1.2	11	1.5	1	-0.048	2	-0.048
								-		
84 1.2D + 1.5Lm + 1.0Wm (240°)	Yes	Y	5	1.2	11	1.5	1	-0.034	2	-0.059
85 1.2D + 1.5Lm + 1.0Wm (270°)	Yes	Y	5	1.2	11	1.5			2	-0.068
86 1.2D + 1.5Lm + 1.0Wm (300°)	Yes	Y	5	1.2	11	1.5	1	0.034	2	-0.059
87 1.2D + 1.5Lm + 1.0Wm (315°)	Yes	Y	5	1.2	11	1.5	1	0.048	2	-0.048
88 1.2D + 1.5Lm + 1.0Wm (330°)	Yes	Y	5	1.2	11	1.5	1	0.059	2	-0.034
89 1.2D + 1.5Lm + 1.0Wm (0°)	Yes	Y	5	1.2	12	1.5	1	0.068	_	
		4	0	1.2	14	1.0		0.000		



5/4/2021 5:17:14 PM Checked By : \_\_\_

#### Load Combinations (Continued)

Description	Solve	PDelta	BLC	Factor	BLC	Factor	BLC	Factor	BLC	Factor
90 1.2D + 1.5Lm + 1.0Wm (30°)	Yes	Y	5	1.2	12	1.5	1	0.059	2	0.034
91 1.2D + 1.5Lm + 1.0Wm (45°)	Yes	Y	5	1.2	12	1.5	1	0.048	2	0.048
92 1.2D + 1.5Lm + 1.0Wm (60°)	Yes	Y	5	1.2	12	1.5	1	0.034	2	0.059
93 1.2D + 1.5Lm + 1.0Wm (90°)	Yes	Y	5	1.2	12	1.5			2	0.068
94 1.2D + 1.5Lm + 1.0Wm (120°)	Yes	Y	5	1.2	12	1.5	1	-0.034	2	0.059
95 1.2D + 1.5Lm + 1.0Wm (135°)	Yes	Y	5	1.2	12	1.5	1	-0.048	2	0.048
96 1.2D + 1.5Lm + 1.0Wm (150°)	Yes	Y	5	1.2	12	1.5	1	-0.059	2	0.034
97 1.2D + 1.5Lm + 1.0Wm (180°)	Yes	Y	5	1.2	12	1.5	1	-0.068		
98 1.2D + 1.5Lm + 1.0Wm (210°)	Yes	Y	5	1.2	12	1.5	1	-0.059	2	-0.034
99 1.2D + 1.5Lm + 1.0Wm (225°)	Yes	Y	5	1.2	12	1.5	1	-0.048	2	-0.048
100 1.2D + 1.5Lm + 1.0Wm (240°)	Yes	Y	5	1.2	12	1.5	1	-0.034	2	-0.059
101 1.2D + 1.5Lm + 1.0Wm (270°)	Yes	Y	5	1.2	12	1.5			2	-0.068
102 1.2D + 1.5Lm + 1.0Wm (300°)	Yes	Y	5	1.2	12	1.5	1	0.034	2	-0.059
103 1.2D + 1.5Lm + 1.0Wm (315°)	Yes	Y	5	1.2	12	1.5	1	0.048	2	-0.048
104 1.2D + 1.5Lm + 1.0Wm (330°)	Yes	Y	5	1.2	12	1.5	1	0.059	2	-0.034
105 ***SEISMIC***										
106 1.2D + 1.0Ev + 1.0Eh (0°)	Yes	Y	5	1.2	5	0.077	7	0.194		
107 1.2D + 1.0Ev + 1.0Eh (30°)	Yes	Y	5	1.2	5	0.077	7	0.168	8	0.097
108 1.2D + 1.0Ev + 1.0Eh (45°)	Yes	Y	5	1.2	5	0.077	7	0.137	8	0.137
109 1.2D + 1.0Ev + 1.0Eh (60°)	Yes	Y	5	1.2	5	0.077	7	0.097	8	0.168
110 1.2D + 1.0Ev + 1.0Eh (90°)	Yes	Y	5	1.2	5	0.077			8	0.194
111 1.2D + 1.0Ev + 1.0Eh (120°)	Yes	Y	5	1.2	5	0.077	7	-0.097	8	0.168
112 1.2D + 1.0Ev + 1.0Eh (135°)	Yes	Y	5	1.2	5	0.077	7	-0.137	8	0.137
113 1.2D + 1.0Ev + 1.0Eh (150°)	Yes	Y	5	1.2	5	0.077	7	-0.168	8	0.124
114 1.2D + 1.0Ev + 1.0Eh (180°)	Yes	Y	5	1.2	5	0.077	7	-0.194		
115 1.2D + 1.0Ev + 1.0Eh (210°)	Yes	Y	5	1.2	5	0.077	7	-0.168	8	-0.097
116 1.2D + 1.0Ev + 1.0Eh (225°)	Yes	Y	5	1.2	5	0.077	7	-0.137	8	-0.137
117 1.2D + 1.0Ev + 1.0Eh (240°)	Yes	Y	5	1.2	5	0.077	7	-0.097	8	-0.168
118 1.2D + 1.0Ev + 1.0Eh (270°)	Yes	Y	5	1.2	5	0.077			8	-0.194
119 1.2D + 1.0Ev + 1.0Eh (300°)	Yes	Y	5	1.2	5	0.077	7	0.097	8	-0.168
120 1.2D + 1.0Ev + 1.0Eh (315°)	Yes	Y	5	1.2	5	0.077	7	0.137	8	-0.137
121 1.2D + 1.0Ev + 1.0Eh (330°)	Yes	Y	5	1.2	5	0.077	7	0.168	8	-0.097

#### Envelope Node Reactions

	Node Label		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N62	max	0.032	19	0.132	25	0.14	7	0	121	0	121	0	121
2		min	-0.031	11	0	16	-0.12	15	0	1	0	1	0	1
3	N27	max	0.019	19	0.987	8	0.075	11	0	121	0	121	0	121
4		min	-0.019	11	-0.801	16	-0.115	19	0	1	0	1	0	1
5	N28	max	0.229	19	1.257	13	0.579	22	0	121	0	121	0	121
6		min	-0.229	11	-1.036	21	-0.538	14	0	1	0	1	0	1
7	N61	max	0.031	19	0.132	39	0.14	7	0	121	0	121	0	121
8		min	-0.032	11	0	14	-0.12	15	0	1	0	1	0	1
9	N26	max	0.019	19	0.987	22	0.075	19	0	121	0	121	0	121
10	_	min	-0.019	11	-0.801	14	-0.115	11	0	1	0	1	0	1
11	N29	max	0.229	19	1.257	17	0.579	8	0	121	0	121	0	121
12		min	-0.229	11	-1.036	9	-0.538	16	0	1	0	1	0	1
13	N54	max	0.033	19	0.143	30	0.116	7	0	121	0	121	0	121
14		min	-0.034	11	0.001	22	-0.136	15	0	1	0	1	0	1
15	N55	max	0.034	19	0.143	34	0.116	7	0	121	0	121	0	121
16		min	-0.033	11	0.001	8	-0.136	15	0	1	0	1	0	1
17	N12	max	0.033	19	0.119	34	0.088	8	0	121	0	121	0	121
18		min	-0.033	11	0.004	8	-0.11	16	0	1	0	1	0	1
19	N13	max	0.033	19	0.119	30	0.088	22	0	121	0	121	0	121
20		min	-0.033	11	0.004	22	-0.11	14	0	1	0	1	0	1
21	N14	max	0.032	19	0.11	26	0.111	8	0	121	0	121	0	121
22		min	-0.032	11	0.002	16	-0.089	16	0	1	0	1	0	1
23	N15	max	0.032	19	0.11	38	0.111	22	0	121	0	121	0	121



#### Envelope Node Reactions (Continued)

	Node Label		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
24		min	-0.032	11	0.002	14	-0.089	14	0	1	0	1	0	1
25	N39	max	0.042	19	0.067	35	0.431	11	0	121	0	121	0	121
26	-	min	-0.042	11	0.022	10	-0.216	19	0	1	0	1	0	1
27	N45	max	0.026	19	0.067	37	0.482	19	0	121	0	121	0	121
28		min	-0.026	11	0.022	12	-0.165	11	0	1	0	1	0	1
29	N41	max	0.042	19	0.067	27	0.216	11	0	121	0	121	0	121
30		min	-0.042	11	0.022	18	-0.431	19	0	1	0	1	0	1
31	N43	max	0.042	19	0.067	37	0.216	19	0	121	0	121	0	121
32		min	-0.042	11	0.022	12	-0.431	11	0	1	0	1	0	1
33	N37	max	0.026	19	0.067	35	0.165	11	0	121	0	121	0	121
34		min	-0.026	11	0.022	10	-0.482	19	0	1	0	1	0	1
35	N38	max	0.026	19	0.067	29	0.165	19	0	121	0	121	0	121
36		min	-0.026	11	0.022	20	-0.482	11	0	1	0	1	0	1
37	N40	max	0.042	19	0.067	29	0.431	19	0	121	0	121	0	121
38		min	-0.042	11	0.022	20	-0.216	11	0	1	0	1	0	1
39	N42	max	0.026	19	0.067	27	0.482	11	0	121	0	121	0	121
40		min	-0.026	11	0.022	18	-0.165	19	0	1	0	1	0	1
41	Totals:	max	1.03	19	2.576	26	2.107	7						
42		min	-1.03	11	1.076	16	-2.107	15						

### Envelope AISC 14th (360-10): LRFD Steel Code Checks

	Member	Shape (	Code Check	Loc[in]	LCS	Shear Check	Loc[in]	Dir	LC	phi*Pnc [k]	phi*Pnt [k]	phi*Mn y-y [k-ft]	phi*Mn z-z [k-ft]	Cb	Eqn
1	ALPHA/BETA	PIPE_2.5	0.032	10.5	7	0.009	10.5		7	37.774	50.715	3.596	3.596	1	H1-1b
2	M2	L6X3.5X6	0.006	3.5	17	0.015	7	Z	15	101.19	111.456	4.002	14.35	1.5	H2-1
3	M3	L6X3.5X6	0.003	0	18	0.003	7	z	19	101.19	111.456	4.002	13.644	1.5	H2-1
4	M4	L6X3.5X6	0.009	3.5	9	0.015	7	z	7	101.19	111.456	4.002	14.35	1.5	H2-1
5	M5	L6X3.5X6	0.004	7	20	0.003	7	Z	19	101.19	111.456	4.002	14.35	1.5	H2-1
6	ALL SECTORS	PIPE_2.5	0.547	81	15	0.038	81		22	15.797	50.715	3.596	3.596	1	H1-1b
7	M13	L6X3.5X6	0.035	3.5	8	0.027	3.5	У	8	101.19	111.456	4.002	14.35	1.5	H2-1
8	M14	L6X3.5X6	0.033	3.5	22	0.096	7	Z	7	101.19	111.456	4.002	13.644	1.5	H2-1
9	M15	L6X3.5X6	0.012	0	8	0.005	7	Z	19	101.19	111.456	3.896	12.767	1.067	H2-1
10	M16	L6X3.5X6	0.015	7	20	0.011	7	У	19	101.19	111.456	4.002	14.35	1.5	H2-1
11	GAMMA	PIPE_2.5	0.125	12	24	0.015	12		24	37.774	50.715	3.596	3.596	1	H1-1b
12	M26	HSS4X4X3	0.037	37.5	19	0.009	37.5	У	36	102.696	106.812	12.662	12.662	2.104	H1-1b
13	M31	HSS4X4X3	0.037	37.5	11	0.009	37.5	У	28	102.696	106.812	12.662	12.662	2.104	H1-1b
14	DELTA	PIPE_2.0	0.066	10.5	7	0.014	10.5		7	20.867	32.13	1.872	1.872	1	H1-1b
15	M35	L6X6X5	0.004	6	35	0.019	12	Z	15	97.867	118.908	9.302	19.858	1.481	H2-1
16	M36	L6X6X5	0.002	6	32	0.002	12	z	9	97.867	118.908	8.085	16.791	1.04	H2-1
17	M39	L6X6X5	0.006	6	8	0.019	12	Z	7	97.867	118.908	9.302	16.791	1.5	H2-1
18	M40	L6X6X5	0.003	6	7	0.002	12	Ζ	17	97.867	118.908	9.302	16.791	1.096	H2-1

# Antenna Mount Frame Analysis

Ref. to attached RISA3D output

1	Node Label		X [k]	LC	Y [k]	LC	Z [k]	LC
1	N29	max	0.229	19	1.257	17	0.579	8
2		min	-0.229	11	-1.036	9	-0.538	16
3	N28	max	0.229	19	1.257	13	0.579	22
4		min	-0.229	11	-1.036	21	-0.538	14
5	N40	max	0.042	19	0.067	29	0.431	19
6		min	-0.042	11	0.022	20	-0.216	11
7	N39	max	0.042	19	0.067	35	0.431	11
8		min	-0.042	11	0.022	10	-0.216	19
9	N41	max	0.042	19	0.067	27	0.216	11
10		min	-0.042	11	0.022	18	-0.431	19
11	N43	max	0.042	19	0.067	37	0.216	19
12		min	-0.042	11	0.022	12	-0.431	11
13	N55	max	0.034	19	0.143	34	0.116	7
14		min	-0.033	11	0.001	8	-0.136	15
15	N54	max	0.033	19	0.143	30	0.116	7
16		min	-0.034	11	0.001	22	-0.136	15
17	N12	max	0.033	19	0.119	34	0.088	8
18		min	-0.033	11	0.004	8	-0.11	16
19	N13	max	0.033	19	0.119	30	0.088	22
20		min	-0.033	11	0.004	22	-0.11	14
21	N14	max	0.032	19	0.11	26	0.111	8
22		min	-0.032	11	0.002	16	-0.089	16
23	N15	max	0.032	19	0.11	38	0.111	22
24		min	-0.032	11	0.002	14	-0.089	14
25	N62	max	0.032	19	0.132	25	0.14	7
26		min	-0.031	11	0	16	-0.12	15
27	N61	max	0.031	19	0.132	39	0.14	7
28		min	-0.032	11	0	14	-0.12	15
29	N45	max	0.026	19	0.067	37	0.482	19
30		min	-0.026	11	0.022	12	-0.165	11
31	N42	max	0.026	19	0.067	27	0.482	11
32		min	-0.026	11	0.022	18	-0.165	19
33	N37	max	0.026	19	0.067	35	0.165	11
34		min	-0.026	11	0.022	10	-0.482	19
35	N38	max	0.026	19	0.067	29	0.165	19
36		min	-0.026	11	0.022	20	-0.482	11
37	N27	max	0.019	19	0.987	8	0.075	11
38		min	-0.019	11	-0.801	16	-0.115	19
39	N26	max	0.019	19	0.987	22	0.075	19
40		min	-0.019	11	-0.801	14	-0.115	11

7

# ALPHA/BETA, ALL SECTORS ANCHORAGE.

**Check Connection** 

Proposed 1/2" Dia. threaded rods w/4" min. embedment and Hilti HY 70 adhesive

Tmax = Tension Load

Fy := 1257lbf

Tmax := Fy

Vmax = Resultant Shear Load

 $Fx:=\,229lbf$ 

 $Fz:=\,579lbf$ 

$$Fr := \sqrt{Fx^2 + Fz^2}$$

 $Vmax := Fr = 622.641 \cdot lbf$ 

Account for two (2) anchor bolts

 $Tallow := 2.905lbf = 1810\,lbf$ 

 $Vallow := 2 \cdot 1685 \cdot lbf = 3370 \, lbf$ 

Interaction.

 $\frac{\text{Tmax}}{\text{Tallow}} + \frac{\text{Vmax}}{\text{Vallow}} = 0.879 \qquad 0.876 < 1.0 \qquad \underline{\text{Bolts OKAY.}}$ 

# ALPHA/BETA, ALL SECTORS ANCHORAGE.

#### **Check Connection**

Existing 5/8" Dia. threaded rods w/ 6" min. embedment Hilti HY 20 adhesive

Tmax = Tension Load

Fy := 1257lbf

Tmax := Fy

Vmax = Resultant Shear Load

Fx:= 229lbf

Fz := 579lbf

$$Fr := \sqrt{Fx^2 + Fz^2}$$

Vmax:= Fr = 622.641.lbf

Account for two (2) anchor bolts

Tallow := 2.815lbf = 1630lbf

$$\underset{}{\text{Vallow}} := 2 \cdot 1355 \cdot \text{lbf} = 2710 \, \text{lbf}$$

Interaction.

 $\frac{\text{Tmax}}{\text{Tallow}} + \frac{\text{Vmax}}{\text{Vallow}} = 1.001 \qquad 0.997 < 1.0 \text{ <u>Bolts OKAY.</u>}$ 

GAMMA, DELTA ANCHORAGE.

**Check Connection** 

Proposed 5/8" Dia. threaded rods w/ 5 5/8" min. embedment and Hilti HY 200 adhesive

Tmax = Tension Load

Fz.:= 482lbf Tmax.:= Fz

Vmax = Resultant Shear Load

Fx:= 42lbf Fy:= 67lbf

$$Fr := \sqrt{Fx^2 + Fy^2}$$

Vmax := Fr = 79.076 · lbf

Tallow := 4010.0.61.0.6.lbf = 1467.66 lbf

$$\underbrace{\text{Vallow}}_{:=} 8640 \cdot 0.54 \cdot 0.61 \cdot \text{lbf} = 2846.016 \text{ lbf}$$

Interaction.

 $\frac{\text{Tmax}}{\text{Tallow}} + \frac{\text{Vmax}}{\text{Vallow}} = 0.356 \qquad 0.356 < 1.0 \text{ Bolts OKAY.}$ 

# **Conclusion:**

The proposed and existing antennas mounts and connections are sufficient to support the T-Mobile appurtenances.

Adhesive Anchoring Systems

# 3.2.6 HIT-HY 70 Hybrid for Masonry Construction

#### Table 10 - HIT-HY 70 allowable adhesive bond loads for threaded rods in the face of hollow brick<sup>1, 2, 3, 4, 5, 10</sup>

Nominal	Effe	ctive			Minim	um edge	Load					Edge	distance <sup>6</sup>	
anchor		dment	Ter	sion		nce c <sub>mn</sub>	reduction	Sh	ear	Crit	ical c <sub>o</sub>	Minim	num c <sub>min</sub>	Load reduction
diameter	in.	(mm)⁵	lb	(kN) <sup>7,8</sup>	in.	(mm) <sup>9</sup>	factor @ c <sub>min</sub>	lb	(kN) <sup>7,8</sup>	in.	(mm)	in.	(mm)	factor @ c <sub>min</sub>
1/4			530	(2.4)				370	(1.6)					1.00
5/16			735	(3.3)		10.001	4.00	595	(2.6)				(000)	1.00
3/8	3-1/8	(79)	905	(4.0)	8	(203)	1.00	1,045	(4.7)	12	(304.8)	8	(203)	0.76
1/2	1		905	(4.0)				1,685	(7.5)					0.52

# Table 11 - HIT-HY 70 allowable adhesive bond loads for HIT-IC inserts in the face of hollow brick<sup>1, 2, 3, 4, 5, 10</sup>

	Effe	ctive			Minim	um edge	Load					Edge of	distance <sup>6</sup>	118
Thread	embe	dment	Ten	nsion	1997 (A. 1997)	nce c <sub>min</sub>	reduction	Sh	ear	Criti	cal c <sub>er</sub>	Minim	num c <sub>min</sub>	Load reduction
size	in.	(mm)⁵	lb	(kN)7,8	in.	(mm) <sup>9</sup>	factor @ c <sub>min</sub>	lb	(kN) <sup>7,8</sup>	in.	(mm)	in.	(mm)	factor @ c <sub>mn</sub>
#14 Screw	2	(51)	51) 170 (0.8)	3		222	(1.0)	2		13. 1		1.00		
5/16-18 UNC			880	(3.9)		(000)	4.00	650	(2.9)	40	(004.0)		(000)	1.00
3/8-16 UNC	3-1/8	(79)	880	(3.9)	8	(203)	1.00	1,290	(5.7)	12	(304.8)	8	(203)	0.63
1/2-13 UNC			990	(4.4)				1,780	(7.9)			-		0.47

# HIT-HY 20 Allowable Loads for Threaded HAS-E Rods in Multi-Wythe Solid Brick Walls $^{\rm 1,\,2}$

Anchor Diameter in. (mm)	Embedment Depth in. (mm)	Allowable Tension Ib (kN)	Allowable Shear Ib (kN)
	6	685	590
3/8	(152)	(3.1)	(2.6)
(9.5)	10	815	590
	(254)	(3.6)	(2.6)
	6	745	930
1/2	(152)	(3.3)	(4.1)
(12.7)	10	1270	930
	(254)	(5.6)	(4.1)
	6	815	1355
5/8	(152)	(3.6)	(6.0)
(15.9)	10	1285	1355
	(254)	(5.7)	(6.0)
	8	1400	1800
3/4	(203)	(6.2)	(8.0)
(19.1)	13	2100	1800
	(330)	(9.3)	(8.0)

#### **Combined Shear and Tension Loading**

 $\left(\frac{N_{c}}{N_{rec}}\right)$ 

$$+\left(\frac{V_{d}}{V_{rec}}\right) \le 1.0$$
 (Ref. Section 3.1.8.3)

<sup>1</sup> Values based on mortar shear strength of 45 psi or greater.

<sup>2</sup> Based on using a safety factor of 5.

#### Structural Analysis for T-Mobile Anchor Installation 7WAC050A

Nominal			Tension	— ΦΝ <sub>n</sub>			Shear	— ΦV <sub>n</sub>	
anchor	Effective	f' = 2,500 psi	f' = 3,000 psi	f' = 4,000 psi	f' <sub>c</sub> = 6,000 psi	f' <sub>c</sub> = 2,500 psi	f' <sub>c</sub> = 3,000 psi	f' <sub>c</sub> = 4,000 psi	f' <sub>c</sub> = 6,000 ps
diameter	embed.	(17.2 MPa)	(20.7 MPa)	(27.6 MPa)	(41.4 MPa)	(17.2 MPa)	(20.7 MPa)	(27.6 MPa)	(41.4 MPa)
in.	in. (mm)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)
	2-3/8	2,020	2,215	2,560	3,135	2,180	2,385	2,755	3,375
	(60)	(9.0)	(9.9)	(11.4)	(13.9)	(9.7)	(10.6)	(12.3)	(15.0)
3/8	3-3/8	3,425	3,755	4,335	5,170	7,380	8,085	9,335	11,430
3/0	(86)	(15.2)	(16.7)	(19.3)	(23.0)	(32.8)	(36.0)	(41.5)	(50.8)
	4-1/2	5,170	5,170	5,170	5,170	11,360	12,445	14,370	17,600
	(114)	(23.0)	(23.0)	(23.0)	(23.0)	(50.5)	(55.4)	(63.9)	(78.3)
	2-3/4	2,520	2,760	3,185	3,905	5,425	5,945	6,865	8,405
	(70)	(11.2)	(12.3)	(14.2)	(17.4)	(24.1)	(26.4)	(30.5)	(37.4)
1/0	4-1/2	5,275	5,780	6,670	7,110	11,360	12,445	14,370	17,600
1/2	(114)	(23.5)	(25.7)	(29.7)	(31.6)	(50.5)	(55.4)	(63.9)	(78.3)
	6	7,110	7,110	7,110	7,110	17,490	19,160	22,120	27,095
	(152)	(31.6)	(31.6)	(31.6)	(31.6)	(77.8)	(85.2)	(98.4)	(120.5)
	3-3/4	4,010	4,395	5,075	6,215	8,640	9,465	10,930	13,390
	(95)	(17.8)	(19.5)	(22.6)	(27.6)	(38.4)	(42.1)	(48.6)	(59.6)
5/8	5-5/8	7,370	8,075	9,325	11,420	15,875	17,390	20,080	24,595
5/6	(143)	(32.8)	(35.9)	(41.5)	(50.8)	(70.6)	(77.4)	(89.3)	(109.4)
	7-1/2	11,350	12,430	13,905	13,905	24,440	26,775	30,915	37,865
	(191)	(50.5)	(55.3)	(61.9)	(61.9)	(108.7)	(119.1)	(137.5)	(168.4)
	4	4,420	4,840	5,590	6,845	9,520	10,430	12,040	14,750
	(102)	(19.7)	(21.5)	(24.9)	(30.4)	(42.3)	(46.4)	(53.6)	(65.6)
3/4	6-3/4	9,690	10,615	12,255	15,010	20,870	22,860	26,395	32,330
5/4	(171)	(43.1)	(47.2)	(54.5)	(66.8)	(92.8)	(101.7)	(117.4)	(143.8)
	8-1/2	13,690	15,000	17,320	18,155	29,490	32,305	37,300	45,685
	(216)	(60.9)	(66.7)	(77.0)	(80.8)	(131.2)	(143.7)	(165.9)	(203.2)

# Table 4 - HIT-HY 200 design strength with concrete/pullout failure for HIT-Z(-R) rods in cracked concrete 1,2,3,4,5,6,7,8,9,10

### Table 15 - Load adjustment factors for 5/8-in. diameter HIT-Z and HIT-Z-R rods in cracked concrete 1,2

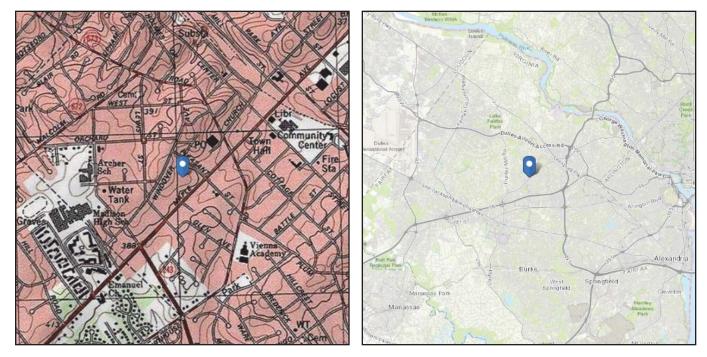
													Edg	je distar	nce in sh	iear				
5/8	-in. HIT-2	7(_B)		cing fact tension	tor in		distance n tensio		Spa	cing fact shear <sup>3</sup>	or in	То	⊥ ward ed	00		∥ Toedge			rete thic tor in sh	
1.1.24	ked con											10		ge		· ·		lac		cai
orac	Red Con			f <sub>AN</sub>	-		f <sub>RN</sub>			f <sub>AV</sub>	-		f <sub>RV</sub>			f <sub>RV</sub>			f <sub>HV</sub>	
Ember	ment h.	in.	3-3/4	5-5/8	7-1/2	3-3/4	5-5/8	7-1/2	3-3/4	5-5/8	7-1/2	3-3/4	5-5/8	7-1/2	3-3/4	5-5/8	7-1/2	3-3/4	5-5/8	7-1/2
		(mm)	(95)	(143)	(191)	(95)	(143)	(191)	(95)	(143)	(191)	(95)	(143)	(191)	(95)	(143)	(191)	(95)	(143)	(191)
(uuu)	3-1/8	(79)	0.64	0.59	0.57	0.67	0.56	0.50	0.55	0.54	0.53	0.18	0.10	0.07	0.35	0.20	0.13	n/a	n/a	n/a
	3-1/4	(83)	0.64	0.60	0.57	0.69	0.56	0.51	0.55	0.54	0.53	0.19	0.11	0.07	0.38	0.22	0.14	n/a	n/a	n/a
Ē.	3-3/4	(95)	0.67	0.61	0.58	0.75	0.60	0.53	0.56	0.54	0.53	0.23	0.13	0.09	0.47	0.27	0.17	n/a	n/a	n/a
- (	4	(102)	0.68	0.62	0.59	0.78	0.62	0.55	0.57	0.55	0.53	0.26	0.15	0.10	0.51	0.30	0.19	n/a	n/a	n/a
s (h),	5	(127)	0.72	0.65	0.61	0.91	0.70	0.60	0.58	0.56	0.54	0.36	0.21	0.13	0.72	0.41	0.27	n/a	n/a	n/a
Concrete thickness	5-1/2	(140)	0.74	0.66	0.62	0.98	0.74	0.63	0.59	0.56	0.55	0.41	0.24	0.15	0.83	0.48	0.31	0.61	n/a	n/a
ž	6	(152)	0.77	0.68	0.63	1.00	0.78	0.66	0.60	0.57	0.55	0.47	0.27	0.18	0.94	0.54	0.35	0.64	n/a	n/a
thic	7	(178)	0.81	0.71	0.66	1.00	0.87	0.72	0.62	0.58	0.56	0.59	0.34	0.22	1.00	0.68	0.44	0.69	n/a	n/a
ete	7-3/8	(187)	0.83	0.72	0.66	1.00	0.90	0.74	0.62	0.59	0.56	0.64	0.37	0.24	1.00	0.74	0.48	0.70	0.59	n/a
ICIE	8	(203)	0.86	0.74	0.68	1.00	0.96	0.78	0.63	0.59	0.57	0.73	0.42	0.27	1.00	0.84	0.54	0.73	0.61	n/a
Ś	9	(229)	0.90	0.77	0.70	1.00	1.00	0.85	0.65	0.60	0.58	0.87	0.50	0.32	1.00	1.00	0.65	0.78	0.65	n/a
	9-1/4	(235)	0.91	0.77	0.71			0.86	0.66	0.61	0.58	0.90	0.52	0.34			0.68	0.79	0.66	0.57
(c <sub>a</sub> )	10	(254)	0.94	0.80	0.72			0.91	0.67	0.62	0.59	1.00	0.58	0.38			0.76	0.82	0.68	0.59
1Ce	11	(279)	0.99	0.83	0.74			0.98	0.69	0.63	0.60		0.67	0.44			0.88	0.86	0.72	0.62
star	12	(305)	1.00	0.86	0.77			1.00	0.70	0.64	0.60		0.77	0.50			1.00	0.90	0.75	0.65
ö	14	(356)	1.00	0.91	0.81				0.74	0.66	0.62		0.97	0.63			1.00	0.97	0.81	0.70
Edge Distance	16	(406)		0.97	0.86				0.77	0.69	0.64		1.00	0.77				1.00	0.86	0.75
/ Ec	18	(457)		1.00	0.90				0.80	0.71	0.66			0.92					0.92	0.79
(s)	24	(610)			1.00				0.90	0.78	0.71			1.00					1.00	0.92
	30	(762)							1.00	0.85	0.76									1.00
Spacing	36	(914)								0.92	0.81									
Sp	> 48	(1219)								1.00	0.92									
	2 40	(1210)					L			1.00	0.02								I	



# ASCE 7 Hazards Report

Standard:ASCE/SEI 7-10Risk Category:IISoil Class:D - Stiff Soil

Elevation: 412.92 ft (NAVD 88) Latitude: 38.898201 Longitude: -77.270861



# Wind

# **Results:**

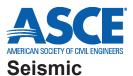
115 Vmph
76 Vmph
84 Vmph
90 Vmph
96 Vmph

### Date &oceseed:

**ASGE/SIG12020**, Fig. 26.5-1A and Figs. CC-1–CC-4, and Section 26.5.2, incorporating errata of March 12, 2014

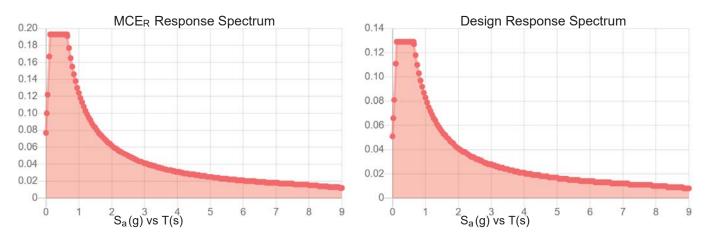
Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is not in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2.



Site Soil Class: Results:	D - Stiff Soil			
S <sub>s</sub> :	0.121	S <sub>DS</sub> :	0.129	
S <sub>1</sub> :	0.052	S <sub>D1</sub> :	0.083	
F <sub>a</sub> :	1.6	T <sub>L</sub> :	8	
F <sub>v</sub> :	2.4	PGA :	0.057	
S <sub>MS</sub> :	0.193	PGA M :	0.091	
S <sub>M1</sub> :	0.124	F <sub>PGA</sub> :	1.6	
		l <sub>e</sub> :	1	

# Seismic Design Category B



Data Accessed: Date Source:

### Fri Apr 16 2021

USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.



# lce

### **Results:**

Ice Thickness:	0.75 in.
Concurrent Temperature:	15 F
Gust Speed:	30 mph
Data Source:	Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Date Accessed:	Fri Apr 16 2021

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

# Snow

Results:	
Ground Snow Load, p <sub>g</sub> :	25 lb/ft <sup>2</sup>
Elevation:	412.9 ft
Data Source:	ASCE/SEI 7-10, Fig. 7-1.
Date Accessed:	Fri Apr 16 2021
	Values provided are ground snow loads. In areas designated "case study required," extreme local variations in ground snow loads preclude mapping at this scale. Site-specific case studies are required to establish ground snow

loads at elevations not covered.



The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.



# **ASCE 7 Hazards Report**

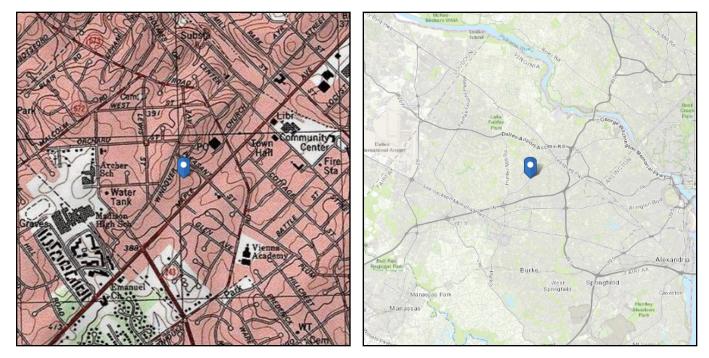
Address: 301 Maple Ave W Vienna, Virginia 22180

Standard:ASCE/SEI 7-10Risk Category:IISoil Class:D - Stiff Soil

 Elevation:
 412.42 ft (NAVD 88)

 Latitude:
 38.898269

 Longitude:
 -77.270956



# Wind

# **Results:**

115 Vmph
76 Vmph
84 Vmph
90 Vmph
96 Vmph

#### Date Socessed:

ASCHARFIOT 2021 ig. 26.5-1A and Figs. CC-1–CC-4, and Section 26.5.2, incorporating errata of March 12, 2014

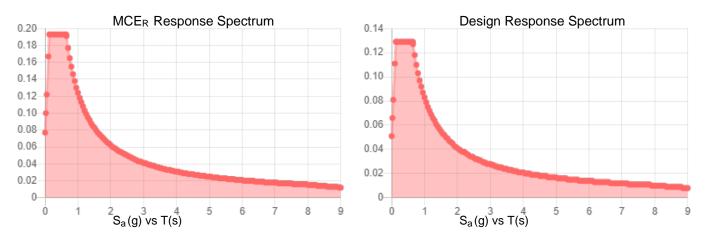
Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is not in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2.



Site Soil Class: Results:	D - Stiff Soil			
S <sub>s</sub> :	0.121	S <sub>DS</sub> :	0.129	
S <sub>1</sub> :	0.052	<b>S</b> <sub>D1</sub> :	0.083	
F <sub>a</sub> :	1.6	T∟ :	8	
F <sub>v</sub> :	2.4	PGA :	0.057	
S <sub>MS</sub> :	0.193	PGA M:	0.091	
S <sub>M1</sub> :	0.124	F <sub>PGA</sub> :	1.6	
		l <sub>e</sub> :	1	

# Seismic Design Category B



Data Accessed: Date Source:

### Wed May 05 2021

USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.



# Ice

### **Results:**

Ice Thickness:	0.75 in.
Concurrent Temperature:	15 F
Gust Speed:	30 mph
Data Source:	Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Date Accessed:	Wed May 05 2021

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

# Snow

Results:	
Ground Snow Load, p <sub>g</sub> :	25 lb/ft <sup>2</sup>
Elevation:	412.4 ft
Data Source:	ASCE/SEI 7-10, Fig. 7-1.
Date Accessed:	Wed May 05 2021
	Values provided are ground snow loads. In areas designated "case study required," extreme local variations in ground snow loads preclude mapping at this scale. Site-specific case studies are required to establish ground snow

loads at elevations not covered.



The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.