SHEET INDEX

SHEET 1

SHEET 1G

SHEET 1M

SHEET 2

SHEET 2K

SHEET 2K(1)

SHEET 2K(6)

PROJECT LOCATION

STATE LINE COUNTY LINE

FENCE LINE

WATER LINE

TRAVELED WAY GUARD RAIL RETAINING WALL

GAS LINE

RAILROADS

BRIDGES CULVERTS

HEDGE

TREES

DROP INLET

POWER POLES

HEAVY WOODS

GROUND ELEVATION

GRADE ELEVATION

CITY, TOWN OR VILLAGE RIGHT OF WAY LINE

FENCED PROPERTY LINE

ELECTRIC UNDERGROUND CABLE

SANITARY SEWER LINE

BASE OR SURVEY LINE

LEVEE OR EMBANKMENT

TELEPHONE OR TELEGRAPH POLES

TELEPHONE OR TELEGRAPH LINES

SHEET 3-4

SHEET 5

SHEET 1G(1) SHEET 1G(2) SHEET 1L-1L(1) Title Sheet for Westbriar Drive NE Sidewalk West

Horizontal Alignment Data
Geometric Data and Signage Panel & Post Details
Erosion & Sediment Control Notes & Details
Erosion & Sediment Control Phases 1 & 2

Survey Control & Horizontal Alignment Data

Existing Drainage & Sanitary Descriptions

General Notes & Details

Existing Drainage Map

Plan & Typical Sections

THIS PROJECT WAS DEVELOPED UTILIZING THE DEPARTMENT'S

VICINITY MAP

CONVENTIONAL SIGNS

SHEET 2K(2) Proposed Drainage Map
SHEET 2K(3)-2K(5) Storm Drainage Computations

ENGINEERING DESIGN PACKAGE (GEOPAK).

GEOPAK Computer Identification No. 41031

Outfall Analysis

Grading Plan

WESTBRIAR DRIVE N.E. - URBAN LOCAL - ROLLING

Fr: Maple Avenue E. (Rte. 123)

To: St. Bernard Drive N.E.

AADT

AWDT

D (%)

T (%)

V (MPH) N/A

N/A

N/A

N/A

N/A

N/A

PLAN AND PROFILE OF PROPOSED

PEDESTRIAN ACCESS IMPROVEMENTS

WESTBRIAR DRIVE N.E. SIDEWALK (WEST) PEDESTRIAN ACCESS IMPROVEMENTS

From: Maple Avenue E.(Rte.123) To: St. Bernard Drive N.E. DESCRIPTION REFERENCES End Proj.at Intersection of Westbriar Drive N.E.and St. Bernard Drive N.E.

Maple Ave. E. Service Drive

Maple Ave.E.Rte.123

To: Route 66

Begin Constr.

Sta.19.92.72

------======== DESCRIPTION REFERENCES D======= Begin Proj.at Intersection of \bullet \bullet \bullet \bullet Westbriar Drive N.E. and Maple Avenue E. .00000 $\sim \sim \sim \sim \sim \sim$ DATUM LINE DATUM LINE

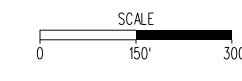
THE COMPLETE ELECTRONIC PDF VERSION OF THE PLAN ASSEMBLY AS AWARDED, HAS BEEN <u>SEALED AND SIGNED</u> USING DIGITAL SIGNATURES AND THE OFFICIAL PLAN ASSEMBLY IN ELECTRONIC FORMAT IS STORED IN THE VDOT CENTRAL OFFICE PLAN LIBRARY, INCLUDING ALL SUBSEQUENT REVISIONS, WILL BE THE OFFICIAL CONSTRUCTION PLANS. FOR INFORMATION RELATIVE TO ELECTRONIC FILES AND LAYERED PLANS, SEE THE GENERAL NOTES.

DESIGN FEATURES RELATING TO CONSTRUCTION OR TO REGULATION AND CONTROL OF TRAFFIC MAY BE SUBJECT TO CHANGE AS DEEMED NECESSARY BY THE DEPARTMENT.

THIS PROJECT IS TO BE CONSTRUCTED IN ACCORDANCE WITH THE DEPARTMENT'S 2007 ROAD AND BRIDGE SPECIFICATIONS, 2008 ROAD AND BRIDGE STANDARDS, 2009 MUTCD, 2011 VIRGINIA SUPPLEMENT TO THE MUTCD, 2011 VIRGINIA WORK AREA PROTECTION MANUAL AND AS AMENDED BY CONTRACT PROVISIONS AND THE COMPLETE ELECTRONIC PDF VERSION OF THE PLAN ASSEMBLY.

ALL CURVES ARE TO BE SUPERELEVATED, TRANSITIONED AND WIDENED IN ACCORDANCE WITH STANDARD TC-5.11U, EXCEPT WHERE OTHERWISE NOTED.

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To: Route 7

Maple Ave. Service Drive N.E

Maple Ave. E. Rte. 123

LO	CALLY ADMINISTERED PROJECTS
	Town of Vienna, Virginia
	NAME OF LOCALITY
NAME OF	(SIGNATURE) RESPONSIBLE LOCAL GOVERNMENT OFFICAL (TYPED)
REC	OMMENDED FOR APPROVAL FOR CONSTRUCTION
	Dennis Johnson, P.E.
DATE	Director of Depart. of Public Works, Town of Vienn

PROJECT SHEET NO.

T MANAGER STED BY SIGN BY RINKEL DE VEYE IGN B

S K S M

PR SUI DE

PROJECT MANAGER Dennis Johnson P.E. (Town of Vienna)

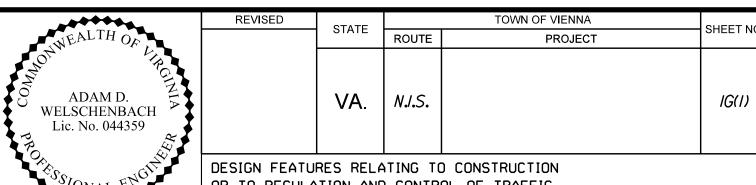
SUBSURFACE UTILITY BY "Miss_Utility" DATE: July 2013_

SURVEYED BY Rinker Design Associates P.C., DATE: July 2013

DESIGN BY Adam_D.Welschenbach_P.E. - Rinker_Design_Associates_P.C.(703) 368-7373

Horizontal Alignment Data

11,839,232.1143



OR TO REGULATION AND CONTROL OF TRAFFIC MAY BE SUBJECT TO CHANGE AS DEEMED NECESSARY BY THE DEPARTMENT

Rinker Design Associates Manassas, Virginia PROFESSIONAL ENGINEER

Maple Avenue Service Drive Construction Baseline

1 Describe Chain 123SERVRD

Chain 123SERVRD contains: SERVRD01 SERVRD02

Beginning chain 123SERVRD description

N 7,017,810.8512 E 11,839,450.3350 Sta 10+00.00 Course from SERVRD01 to SERVRD02 N 58° 47' 52.4499" E Dist 1,750.0000

N 7.018.717.4533 E 11,840,947.1893 Sta Point SERVRD02

-----Ending chain 123SERVRD description

Westbriar Drive Construction Baseline

2 Describe Chain WESTBRIAR

Chain WESTBRIAR contains: WESTB01 CUR WESTB01 CUR WESTB02 WESTB06

Beginning chain WESTBRIAR description

Feature: DEFAULT_POINT

N 7,017,759.5305 E 11,839,481.4185 Sta 20+00.00

Course from WESTB01 to PC WESTB01 N 31° 12' 07.5503" W Dist 413.1666

Curve Data

*----Curve WESTB01 Feature: DEFAULT_POINT

P.I. Station 24+81.23 N 7,018,171.1467 E 64° 55' 12.0001" (RT) 53° 32' 50.8470"

Degree 68.0615 Tangent 121.2382 Length Radius 107.0000 19.8124 External = Long Chord 114.8561

16.7170 Mid. Ord. • P.C. Station 24+13.17 N 7,018,112.9306 E 11,839,267.3742 7,018,227.7590 E 11,839,269.8956 P.T. Station 25+34.40 N N 7,018,168.3628 E 11,839,358.8961 N 31° 12' 07.5503" W

- N 33° 43' 04.4498" E Ahead Chord Bear • N 1° 15' 28.4497" E

Course from PT WESTB01 to PC WESTB02 N 33° 43' 04.4493" E Dist 79.5766

Curve WES	STB02			
P.I. Statio	n	26+68.53 N	7,018,339.3191 E	11,839,344.3473
Delta	•	5° 29' 14.0014" (RT)	·	·
Degree	-	5° 02' 01.6993''		
Tangent	•	54.5454		
Length	-	109.0074		
Radius	-	1,138.2200		
		'. =		

Curve Data

*----

Lengt Radius External • Long Chord 1.3047 Mid. Ord. -7,018,293.9493 E P.C. Station 26+13.98 N 11,839,314.0689 27+22.99 N 7,018,381.5857 E 11,839,378.8254 P.T. Station N 7,017,662.1184 E 11,840,260.8183 - N 33° 43' 04.4485"

- N 39° 12' 18.4500" E Ahead Chord Bear = N 36° 27' 41.4492" E

Course from PT WESTB02 to WESTB06 N 39° 12' 18.4501" E Dist 777.0100

Point WESTB06 N 7,018,983.6814 E 11,839,869.9723 Sta

Ending chain WESTBRIAR description

Saint Bernard Drive Construction Baseline

3 Describe Chain STBERNARD

Chain STBERNARD contains: STBERNO1 CUR STBERNO1 STBERNO4

Beginning chain STBERNARD description

N 7,018,597.8712 E 11,839,555.2557 Sta 30.00.00

Course from STBERN01 to PC STBERN01 S 57° 26' 45.5502" E Dist 535.2084

Curve Data *----

35+82.02 N 7,018,284.6908 E 11,840,045.8292 26° 15' 33.3160" (RT) 28° 33' 02.9411" Tangent Length Radius 200.6800 External =

Long Chord Mid. Ord. -P.C. Station 35+35.21 N

Curve STBERN01

7,018,309.8785 E 7,018,244.6463 E 11,840,006.3746 P.T. Station 11,840,070.0684 N 7,018,140.7284 E 11,839,898.3898 - S 57° 26' 45.5502" E

- S 31° 11' 12.2342" E Ahead Chord Bear - S 44° 18' 58.8922" E

Course from PT STBERN01 to STBERN04 S 31° 11' 12.2330" E Dist 49.9866

N 7,018,201.8836 E 11,840,095.9529 Sta Point STBERN04 36+77.17

Ending chain STBERNARD description

Saint Andrews Drive Construction Baseline

4 Describe Chain STANDREWS

Chain STANDREWS contains: STAND01 CUR STAND01 STAND04

Point STAND01

Beginning chain STANDREWS description

N 7,018,878.7352 E 11,839,784.3646 Sta

Course from STAND01 to PC STAND01 S 57° 26' 45.5501" E Dist 600.4584

Curve Data *----

Curve STAND01 P.I. Station 46+80.49 N 7,018,512.5689 E 11,840,357.9366 26° 15' 11.6298" (RT) 16° 41' 43.9706" Degree

Tangent Length Radius 343.1800 External • Long Chord 155.8749 8.9671 Mid. Ord. •

7,018,555.6318 E 11,840,290.4817 7,018,444.1101 E 11,840,399.3849 P.C. Station 46+00.46 N 47+57.71 N P.T. Station N 7,018,266.3707 E 11,840,105.8185 - S 57° 26' 45.5501" E

- S 31° 11' 33.9202" E Ahead Chord Bear - S 44° 19' 09.7351" E

Course from PT STAND01 to STAND04 S 31° 11' 33.9216" E Dist 102.2918

Point STAND04 N 7,018,356.6066 E 11,840,452.3637 Sta

Ending chain STANDREWS description

> **PROJECT** SHEET NO. IG(1)

48+60.00

40+00.00

Erosion and Sediment Control Narrative

Project Description: The project proposes approximately 1,020 linear feet of concrete sidewalk on the west side of Westbriar Drive N.E. from the Maple Avenue Service Drive to St. Bernard Drive N.E. The project also proposes the installation and reconstruction of curb ramps within the project site.

Existing Site Conditions: The project site consists of a curb & gutter section roadway with a golf course fronting the roadway. The site generally drains from the edge of the golf course towards the roadway and the roadway drains from the north to the south. Vegetation within the project site consists of landscaped grass areas with mature trees and bushes. Storm runoff is collected by drop inlets at the intersection of Westbriar Drive N.E. and the Maple Avenue Service Drive and is then conveyed westward along the existing roadway via an existing closed storm sewer

Adjacent Areas: Areas adjacent to the project are residential in nature.

Off-site Areas: There will be impacts to adjacent parcels associated with the construction of this project. All necessary right-of-way, easements, and provisions will be acquired prior to the start of construction. The Contractor shall be responsible for the locations of acceptable borrow and/or disposal sites, and these shall be in accordance with Town of Vienna or as directed by the Town.

Soils: See soils map located on this sheet.

Critical Areas: There are no critical areas within the project site.

Erosion and Sediment Control Measures: Water quality and sediment/erosion control are of extreme importance. Care must be taken to avoid discharge of sediment into the existing storm water system. In order to best control impacts on this watershed. all vegetative and structural sediment control practices shall be constructed and maintained according to minimum standards and specifications of the Virginia Erosion and Sediment Control Handbook. Strict compliance with this program and standards is required. We are therefore specifying a plan to minimize impacts on the ad jacent properties.

At the time of land disturbing activities within the Town right-of-way, the Contractor shall have a representative with Erosion and Sediment Control Contractor Certification (ESCCC) at the project site. The Town and Contractor is responsible for complying with applicable Local, State, and Federal Environmental Laws and Regulations, including acquiring clearances/authorizations from appropriate regulatory agencies.

Land Disturbing/Construction Sequence - Phase I

I. The Contractor shall install the silt fence, inlet protection, and tree protection as shown on the Erosion & Sediment Control plan.

2. After the silt fence, inlet protection, and tree protection have been installed, the Contractor shall obtain the site inspector's approval of these controls. 3. After the site inspector's approval of the initial controls, clear and grub the site as

Land Disturbing/Construction Sequence - Phase 2

I. Fine grade the site.

necessary.

2. Install sidewalk and entrance base course and concrete pavement.

3. Install all permanent seeding and fertilize all grassed areas.

4. Clean site of all trash and debris. 5. Have the inspector inspect all areas to determine if they are adequately stabilized.

Maintenance Program: The Contractor shall make a visual inspection of all mechanical controls and newly stabilized areas (i.e. seeded, mulched, or sodded areas) on a daily basis and after each rainfall event to insure that all controls are functioning properly. The following items will be checked in particular: inlet protection will be checked regularly for sediment buildup which will prevent drainage, and if the gravel is clogged by sediment, it shall be removed and cleaned or replaced; the silt fence barrier will be checked regularly for undermining or deterioration of the fabric, and sediment shall be removed when the level of sediment deposition reaches halfway to the top of the barrier; and the seeded areas will be checked regularly to ensure that a good stand is maintained, and areas shall be fertilized and reseeded as needed. Any damaged controls shall be repaired by the end of the work day, including reseeding and mulching if necessary. The Contractor may install additional measures should he or she deem it necessary at the inspector's approval. All erosion & sediment controls shall be removed within seven (7) days after the project is stabilized.

Structural Practices:

I. Silt Fence Barrier (3.05) - Silt fence barriers will be installed downslope of areas with minimal grades to filter sediment-laden runoff from sheet flow as indicated in the Erosion and Sediment control plans.

2. Storm Drain Inlet Protection (3.07) - All storm sewer inlets shall be protected during construction. Sediment-laden water shall be filtered before entering the storm

3. Temporary Seeding (3.31) - All denuded areas which will be left dormant for extended periods of time shall be seeded with fast germinating temporary vegetation immediately following grading. Selection of the seed mixture will depend on the time of year it is applied.

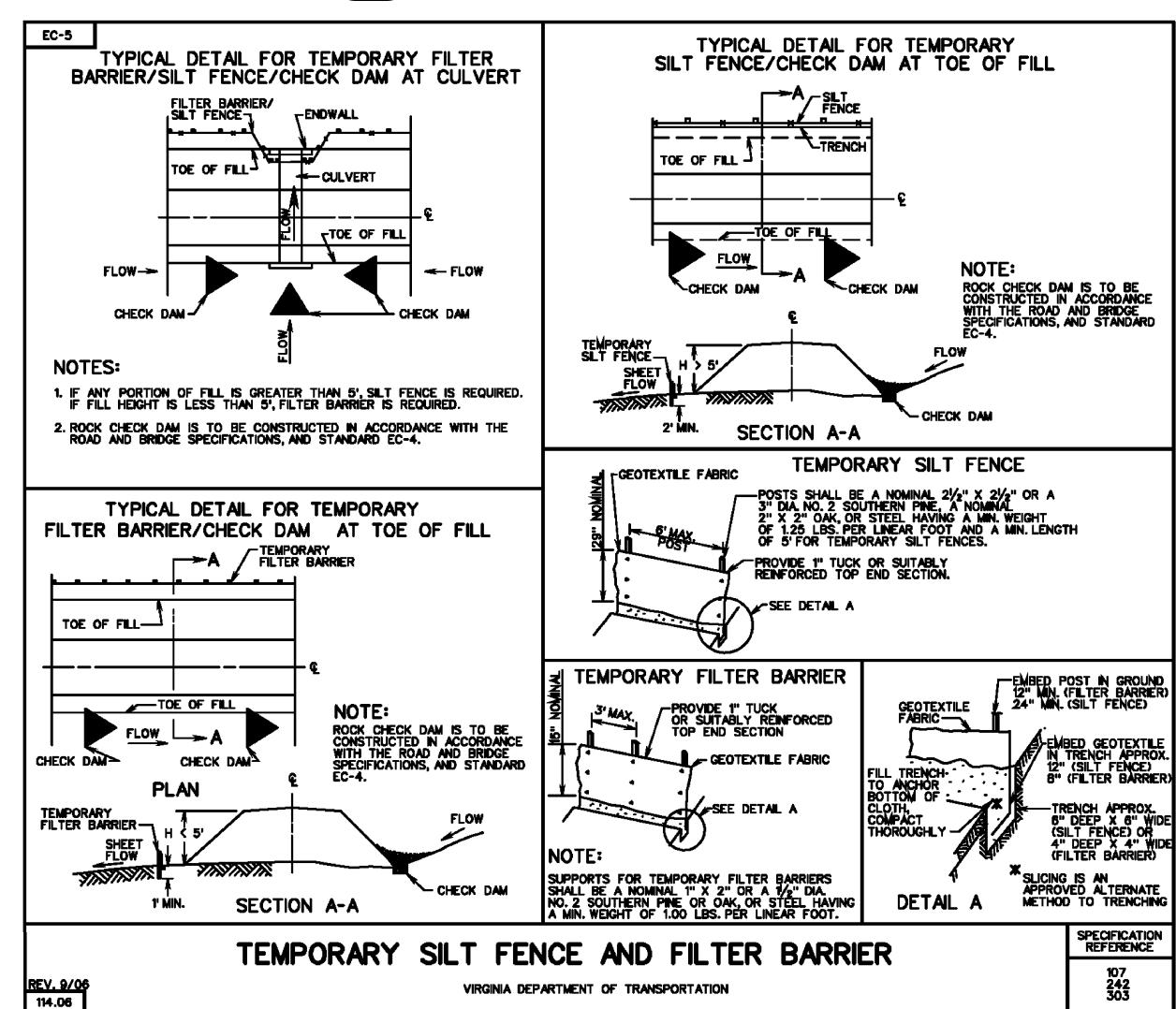
4. Permanent Seeding (3.32) - Perennial vegetative cover shall be established on disturbed areas by planting seed to reduce erosion and decrease sediment yield and to permanently stabilize disturbed areas. Selection of the seed mixture will depend on the time of year it is applied.

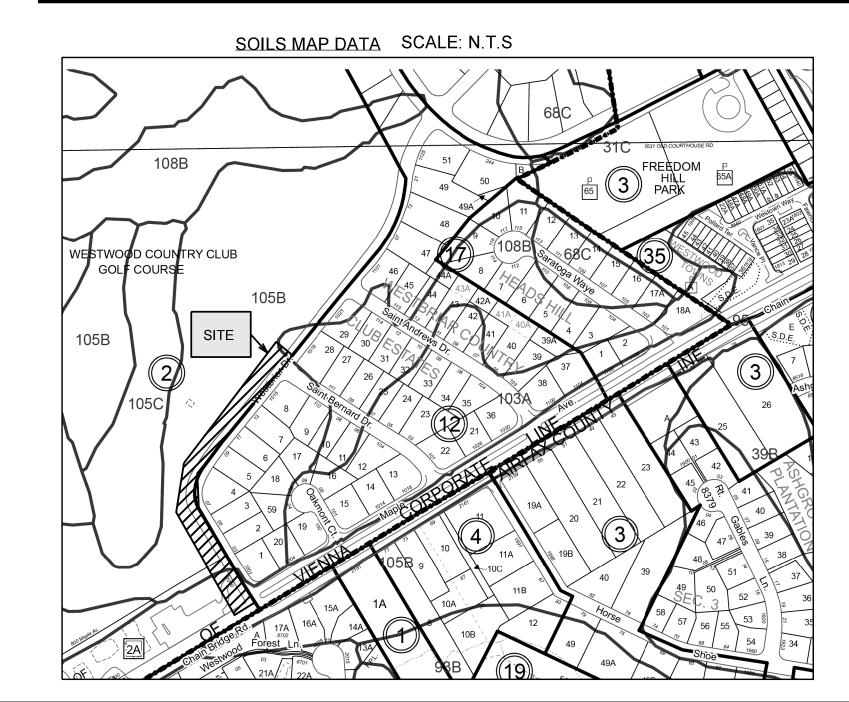
5. Permanent Stabilization - Permanent stabilization shall be done in accordance with the VESCH and all Town of Vienna seeding standards.

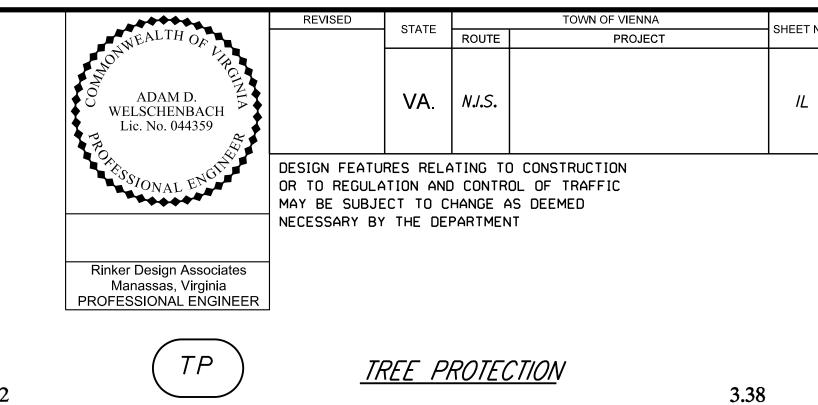
Stormwater Runoff Considerations: See sheet 2K(6) for Outfall Analysis for this

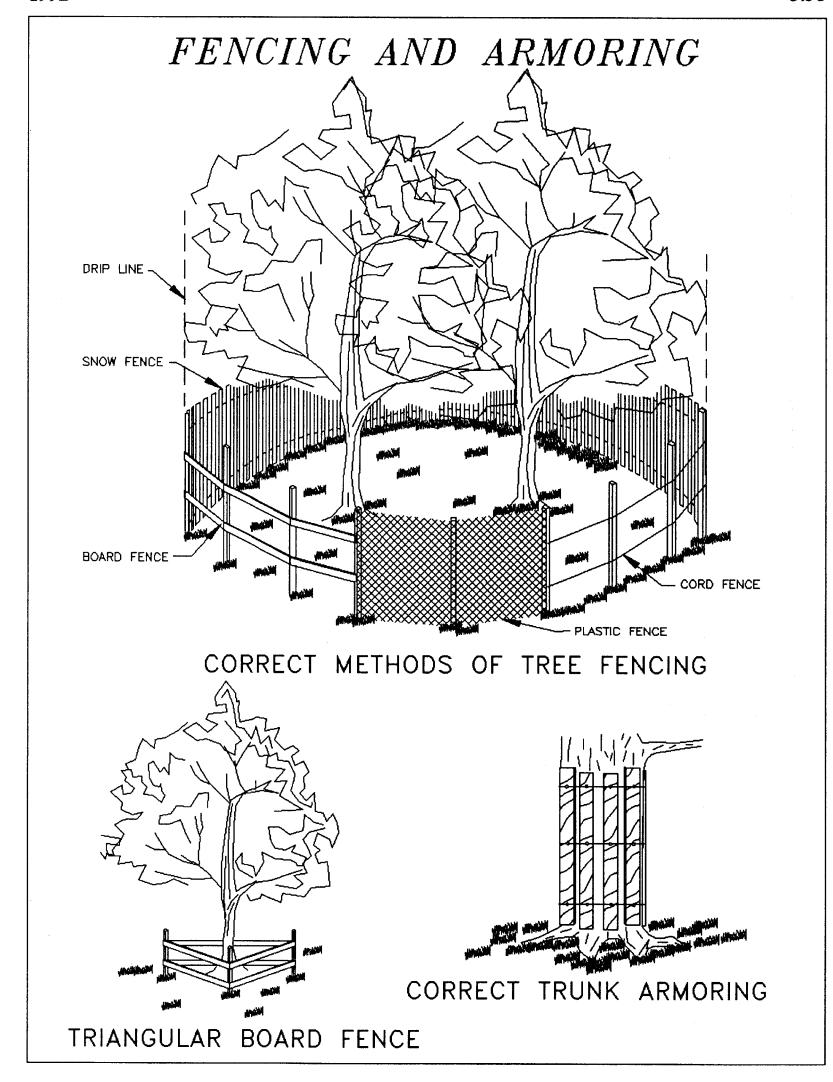
Erosion & Sediment Control Notes & Details

TEMPORARY SILT FENCE









Source: Va. DSWC

Plate 3.38-2

SOILS MAP SO	DURCE: ⊠COUNTY MAP; □	PRIVATE SOILS	SCIENTIST	(FOR UNMAPI	PED SITES)
SOIL ID NUMBERS	SOIL SERIES NAME	FOUNDATION SUPPORT	SOIL DRAINAGE	EROSION POTENTIAL	PROBLEM CLASS
95	URBAN LAND	N/A	N/A	N/A	IVB
105B	WHEATON GLENELG COMPLEX	GOOD	GOOD	HIGH	IVB
108B	WHEATON SUMERDUCK COMPLEX	MARGINAL	POOR	MEDIUM	IVB

IS THE SITE LOCATED WITHIN NATURALLY OCCURING ASBESTOS SOILS? YES □ NO ⊠

AREAS THAT MAY CONTAIN NATURALLY OCCURING ASBESTOS SOILS ARE LOCATED ON THE ORANGE SOILS TAX MAP GRIDS ON THE COUNTY WEBSITE. SPECIAL PRECAUTIONS REGARDIND THESE SOILS OR FILL ORIGINATING FROM THESE SOILS ARE REQUIRED BY OCCUPATIONAL SAFETY AND HEALTH REGULATIONS ENFORCED BY THE VIRGINIA DEPARTMENT OF LABOR AND INDUSTRY AND SPECIAL GUIDANCE HAS BEEN ISSUED BY THE U.S. ENVIRONMENTAL PROTECTION AGENCY

SOILS MAPPED OVER NATUALLY OCCURING BEDROCK. THESE SOILS OCCUR WITHIN A GEOLOGIC FORMATION KNOWN AS THE PINEY BRANCH COMPLEX, LOCALLY KNOWN AS GREENSTONE. NATURALLY-OCCURRING ASBESTOS MINERALS, PREDOMINANTLY ACTINOLITE AND TREMOLITE, ARE KNOWN TO OCCUR IN THIS FORMATION. EXCAVATIONS IN BEDROCK OR EARTH MOVING ACTIVITIES WITHIN THIS FORMATION MAY EXPOSE THESE MINERALS TO THE ATMOSPHERE, ALLOWING THE FIBERS TO BECOME AIRBORNE.

PROJECT	SHEET NO.
	IL.
	_

ROJECT MANAGER*Dennis Johnson_P.E.(Town of Vienna)* SURVEYED BY *Rinker Design Associates P.C., DATE: July 2013* DESIGN BY Adam D. Welschenbach P.E. - Rinker Design Associates P.C. (703) 368-7373 SUBSURFACE UTILITY BY "Miss_Utility" DATE: July 2013_

Frosion & Sediment Control Notes & Details

ROUTE **PROJECT** ADAM D. WELSCHENBACH IL(I) **VA**. | *N.I.S*. Lic. No. 044359 DESIGN FEATURES RELATING TO CONSTRUCTION OR TO REGULATION AND CONTROL OF TRAFFIC

MAY BE SUBJECT TO CHANGE AS DEEMED NECESSARY BY THE DEPARTMENT

Rinker Design Associates Manassas, Virginia PROFESSIONAL ENGINEER

4V AC50-30-40. Minimum Standards. (MS-19) A VESCP must be consistent with the following criteria, techniques and methods: 17. Where construction vehicle access routes intersect paved or public roads, I. Permanent or temporary soil stabilization shall be applied to denuded areas within

seven days after final grade is reached on any portion of the site. Temporary soil stabilization shall be applied within seven days to denuded areas that may not be at final grade but will remain dormant for longer than 14 days. Permanent stabilization shall be applied to areas that are to be left dormant for more than one

2.During construction of the project, soil stock piles and borrow areas shall be stabilized or protected with sediment trapping measures. The applicant is responsible for the temporary protection and permanent stabilization of all soil stockpiles on site as well as borrow areas and soil intentionally transported from the project site.

3.A permanent vegetative cover shall be established on denuded areas not otherwise permanently stabilized. Permanent vegetation shall not be considered established until a ground cover is achieved that is uniform, mature enough to survive and will inhibit erosion.

4. Sediment basins and traps, perimeter dikes, sediment barriers and other measures intended to trap sediment shall be constructed as a first step in any land-disturbing activity and shall be made functional before upslope land disturbance takes place.

5. Stabilization measures shall be applied to earthen structures such as dams, dikes and diversions immediately after installation.

6. Sediment traps and sediment basins shall be designed and constructed based upon the total drainage area to be served by the trap or basin.

a. The minimum storage capacity of a sediment trap shall be 134 cubic yards per acre of drainage area and the trap shall only control drainage areas less than three acres.

b. Surface runoff from disturbed areas that is comprised of flow from drainage areas greater than or equal to three acres shall be controlled by a sediment basin. The minimum storage capacity of a sediment basin shall be 134 cubic yards per acre of drainage area. The outfall system shall, at a minimum, maintain the structural integrity of the basin during a 25-year storm of 24-hour duration. Runoff coefficients used in runoff calculations shall correspond to a bare earth condition or those conditions expected to exist while the sediment basin is utilized.

7.Cut and fill slopes shall be designed and constructed in a manner that will minimize erosion. Slopes that are found to be eroding excessively within one year of permanent stabilization shall be provided with additional slope stabilizing measures until the problem is corrected.

8.Concentrated runoff shall not flow down cut or fill slopes unless contained within an adequate temporary or permanent channel, flume or slope drain structure.

9. Whenever water seeps from a slope face, adequate drainage or other protection shall be provided.

10. All storm sewer inlets that are made operable during construction shall be protected so that sediment-laden water cannot enter the conveyance system without first being filtered or otherwise treated to remove sediment.

II. Before newly constructed stormwater conveyance channels or pipes are made operational, adequate outlet protection and any required temporary or permanent channel lining shall be installed in both the conveyance channel and receiving channel.

12. When work in a live watercourse is performed, precautions shall be taken to minimize encroachment, control sediment transport and stabilize the work area to the greatest extent possible during construction. Non-erodible material shall be used for the construction of causeways and cofferdams. Earthen fill may be used for these structures if armored by non-erodible cover materials.

13. When a live watercourse must be crossed by construction vehicles more than twice in any six-month period, a temporary vehicular stream crossing constructed of non-erodible material shall be provided.

14. All applicable federal, state and local chapters pertaining to working in or crossing live watercourses shall be met.

15. The bed and banks of a watercourse shall be stabilized immediately after work in the watercourse is completed.

16. Underground utility lines shall be installed in accordance with the following standards in addition to other applicable criteria:

a. No more than 500 linear feet of trench may be opened at one time.

b. Excavated material shall be placed on the uphill side of trenches.

c. Effluent from dewatering operations shall be filtered or passed through an approved sediment trapping device, or both, and discharged in a manner that does not adversely affect flowing streams or off-site property.

d.Material used for backfilling trenches shall be properly compacted in order to minimize erosion and promote stabilization.

e. Restabilization shall be accomplished in accordance with this chapter.

f. Applicable safety chapters shall be complied with.

- provisions shall be made to minimize the transport of sediment by vehicular tracking onto the paved surface. Where sediment is transported onto a paved or public road surface, the road surface shall be cleaned thoroughly at the end of each day. Sediment shall be removed from the roads by shoveling or sweeping and transported to a sediment control disposal area. Street washing shall be allowed only after sediment is removed in this manner. This provision shall apply to individual development lots as well as to larger land-disturbing activities.
- 18. All temporary erosion and sediment control measures shall be removed within 30 days after final site stabilization or after the temporary measures are no longer needed, unless otherwise authorized by the VESCP authority. Trapped sediment and the disturbed soil areas resulting from the disposition of temporary measures shall be permanently stabilized to prevent further erosion and sedimentation.
- 19. Properties and waterways downstream from development sites shall be protected from sediment deposition, erosion and damage due to increases in volume, velocity and peak flow rate of stormwater runoff for the stated frequency storm of 24-hour duration in accordance with the following standards and criteria. Stream restoration and relocation projects that incorporate natural channel design concepts are not man-made channels and shall be exempt from any flow rate capacity and velocity requirements for natural or man-made channels:
- a. Concentrated stormwater runoff leaving a development site shall be discharged directly into an adequate natural or man-made receiving channel, pipe or storm sewer system. For those sites where runoff is discharged into a pipe or pipe system, downstream stability analyses at the outfall of the pipe or pipe system shall be performed.
- b. Adequacy of all channels and pipes shall be verified in the following manner: I) The applicant shall demonstrate that the total drainage area to the point of analysis within the channel is one hundred times greater than the contributing drainage area of the project in question; or

a) Natural channels shall be analyzed by the use of a two-year storm to verify that stormwater will not overtop channel banks nor cause erosion of channel bed or banks.

b) All previously constructed man-made channels shall be analyzed by the use of a ten-year storm to verify that stormwater will not overtop its banks and by the use of a two-year storm to demonstrate that stormwater will not cause erosion of channel bed or banks; and

c) Pipes and storm sewer systems shall be analyzed by the use of a ten-year storm to verify that stormwater will be contained within the pipe or system.

c. If existing natural receiving channels or previously constructed man-made channels or pipes are not adequate, the applicant shall:

I) Improve the channels to a condition where a ten-year storm will not overtop the banks and a two-year storm will not cause erosion to channel the bed or banks: or

2) Improve the pipe or pipe system to a condition where the ten-year storm is contained within the appurtenances:

3) Develop a site design that will not cause the pre-development peak runoff rate from a two-year storm to increase when runoff outfalls into a natural channel or will not cause the pre-development peak runoff rate from a ten-year storm to increase when runoff outfalls into a man-made channel; or

4)Provide a combination of channel improvement, stormwater detention or other measures which is satisfactory to the VESCP authority to prevent downstream erosion.

d. The applicant shall provide evidence of permission to make the improvements. e. All hydrologic analyses shall be based on the existing watershed characteristics and the ultimate development condition of the subject project.

f. If the applicant chooses an option that includes stormwater detention, he shall obtain approval from the VESCP of a plan for maintenance of the detention facilities. The plan shall set forth the maintenance requirements of the facility and the person responsible for performing the maintenance.

g. Outfall from a detention facility shall be discharged to a receiving channel, and energy dissipators shall be placed at the outfall of all detention facilities as necessary to provide a stabilized transition from the facility to the receiving channel.

h. All on-site channels must be verified to be adequate.

i. Increased volumes of sheet flows that may cause erosion or sedimentation on ad jacent property shall be diverted to a stable outlet, adequate channel, pipe or pipe system, or to a detention facility.

j.In applying these stormwater management criteria,individual lots or parcels in a residential, commercial or industrial development shall not be considered to be separate development projects. Instead, the development, as a whole, shall be considered to be a single development project. Hydrologic parameters that reflect the ultimate development condition shall be used in all engineering calculations.

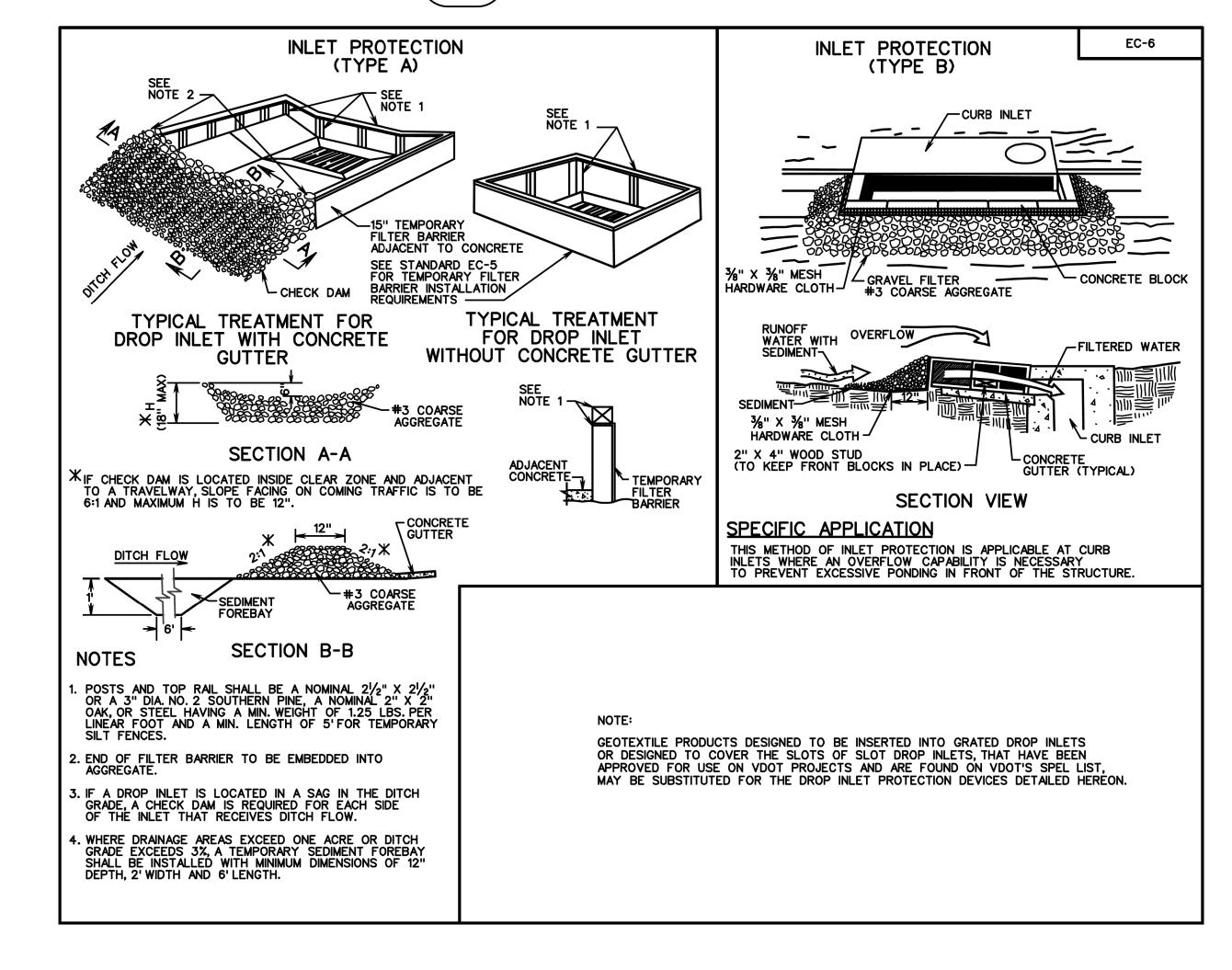
k. All measures used to protect properties and waterways shall be employed in a manner which minimizes impacts on the physical, chemical and biological integrity of rivers, streams and other waters

I. Any plan approved prior to July 1,2014, that provides for stormwater management that addresses any flow rate capacity and velocity requirements for natural or man-made channels shall satisfy the flow rate capacity and velocity requirements for natural or man-made channels if the practices are designed to (i) detain the water quality volume and to release it over 48 hours; (ii) detain and release over a 24-hour period the expected rainfall resulting from the one year, 24-hour storm; and (iii) reduce the allowable peak flow rate resulting from the 1.5, 2, and 10-year, 24-hour storms to a level that is less than or equal to the peak flow rate from the site assuming it was in a good forested condition, achieved through multiplication of the forested peak flow rate by a reduction factor that is equal to the runoff volume from the site when it was in a good forested condition divided by the runoff volume from the site in its proposed condition, and shall be exempt from any flow rate capacity and velocity requirements for natural or man-made channels as defined in any regulations promulgated pursuant to IO.J-562 or 10.1-570 of the Act.

m.For plans approved on and after July 1,2014, the flow rate capacity and velocity requirements of IOJ-561 A of the Act and this subsection shall be satisfied by compliance with water quantity requirements in the Stormwater Management Act (IOJ-603.2 et seq.of the Code of Virginia) and attendant regulations, unless such land-disturbing activities are in accordance with 4VAC50-60-48 of the Virginia Stormwater Management Program (VSMP) Permit Regulations.

n. Compliance with the water quantity minimum standards set out in 4VAC50-60-66 of the Virginia Stormwater Management Program (VSMP) Permit Regulations shall be deemed to satisfy the requirements of Minimum Standard 19.

INLET PROTECTION



GENERAL NOTES

construction.

EROSION AND SEDIMENT CONTROL (ESC) GENERAL NOTES

See Sheets IL and IL(I) for the Erosion & Sediment Control General Notes and Legend.

ROJECT MANAGER*Dennis Johnson_P.E.(T.own of Vienna)* SURVEYED BY *Rinker Design Associates P.C., DATE: July 2013* DESIGN BY Adam_D.Welschenbach_P.E. - Rinker_Design_Associates_P.C.(703) 368-7373 SUBSURFACE UTILITY BY "Miss_Utility" DATE: July 2013

General Notes & Details

OWN OF VIENNA REVISED **PROJECT** ROUTE ADAM D. WELSCHENBACH **VA**. | *N.J.S*. DESIGN FEATURES RELATING TO CONSTRUCTION

OR TO REGULATION AND CONTROL OF TRAFFIC MAY BE SUBJECT TO CHANGE AS DEEMED NECESSARY BY THE DEPARTMENT

Rinker Design Associates Manassas, Virginia PROFESSIONAL ENGINEER

edition of the VDOT Road and Bridge Standards, current VDOT insertable sheets to the Road and Bridge Standards, and all special provisions in effect at the time the plan is approved. The Contractor is to also perform all work in accordance with all current revisions to the Road and Bridge Standards, as applicable. The Contractor shall replace all structure tops within the project limits as noted on the plans. Only structure tops are to be replaced. All related incidental work and adjacent curb/pavement replacement/repair shall be incidental to the cost of structure top replacement.

The Contractor shall conduct a post installation visual/video camera inspection of all storm sewer

-All entrances shall remain open during non-working hours or as directed by the Town.

All work shall be in accordance with the current edition of the Manual on Uniform Traffic Control <u>Devices</u> (MUTCD), the current edition of the VDOT <u>Road and Bridge Specifications</u>, the current

pipes and a selected number of pipe culverts in accordance with the requirements of Section

302.03(d) of the VDOT 2007 Supplemental Road & Bridge Specifications and VTM 123.

The Contractor shall present a TMP/SOC plan to the Town for approval prior to the start of

The Contractor shall follow all Town of Vienna requirements for planting trees (including installing any tree root barrier when trees are to be installed adjacent to proposed curb) at no additional cost to the project.

6. The Town of Vienna shall determine what species of tree(s) to plant. Unless otherwise directed by the Town the following tree types shall be used:

a) Tree Type I = Red Maple b) Tree Type 2 = Willow Oak c) Tree Type 3 = Northern Red Oak

7. a) The Contractor is responsible for locating all utilities. Utilities shown on plans are not guaranteed. Any disruption/impact in utility service is the sole responsibility of the Contractor. The Contractor is responsible for all utility relocation efforts/coordination to ensure utilities are relocated and/or reset (as needed for utility boxes, pole guys etc.) and/or sidewalk guy wires are installed. The Contractor is responsible for all costs not covered by the Town of Vienna's utility franchise agreement(s). Coordination with Town of Vienna is required.

b) The Town of Vienna's forces will relocate as needed (due to construction conflicts) any other waterline conflicts, fire hydrants, and water meters. The Contractor shall coordinate with the Town of Vienna for construction scheduling to ensure continued service.

The Contractor shall plant trees in accordance with VDOT's 2007 Road and Bridge Specifications. Section 605.05,(b) of VDOT's 2007 Road and Bridge Specifications is amended to establish the "Establishment Period" for trees planted to be one full year. Additionally, Section 605.05,*I,b) is amended to add that the Contractor is required to water the trees once a week June OI through September 31. Lastly, Section 605.05 *4 is amended to replace the last sentence as follows: Any future trees to be replaced shall be at the Contractor's expense, through the end of the "Establishment Period."

The Contractor shall provide Construction Surveying in accordance with VDOT's 2007 Road and Bridge Specifications under the direction of a Virginia Licensed Land Surveyor. Additionally the Contractor shall provide Construction Engineering Inspection (CEI) services as directed the Town (if required) at no additional cost to the project.

DRAINAGE GENERAL NOTES

Road and Bridge Specifications.

GRADING GENERAL NOTES

The horizontal location of all drainage structures shown on these plans is approximate only, with the exception of structures showing specific stations, special design bridges and storm sewer

The cost of removal of all existing concrete items located in the area to be graded, including, but

Footings, Light Pole Foundations, End Walls, Drop Inlets, Manholes, Pipes, Concrete Slabs, Curb and Gutter, Concrete or Asphalt Sidewalk, Paved Ditches, Foundation Slabs, and Base or Brick items.

measurement and payment shall be made in accordance with Section 303 of the applicable VDOT

The borrow or embankment material for this project shall be a minimum CBR 6 or as approved

by the Town Engineer. Material classified as CH or MH in its natural state according to ASTM

not limited to the following, shall be included in the price bid for regular excavation: Small

2. If, during construction, it is deemed necessary to change the depth more than I foot (0.3 m) or the

limits of such excavation, such change shall be made at the direction of the Engineer and

D 2487 or ASTM D 2488 shall not be hauled on-site as borrow material.

- The horizontal location and invert elevations shown for proposed culverts and storm sewer outfall pipes are based on existing survey data and required design criteria. If, during construction, it is found that the horizontal location or invert elevations shown on the plans differ significantly from the horizontal location or elevations of the stream or swale in which the culvert or storm sewer outfall pipe is to be placed, the Engineer shall confer with, and get approval from the applicable Town Engineer before installing the culvert or storm sewer outfall
- The "H" dimensions shown on the plans for drop inlets and junction boxes and the "L.F.(m)" dimensions shown for manholes are for estimating purposes and are based on the proposed invert elevations shown for the structure and the anticipated top (rim) elevation based on existing or proposed finished grade. The actual "H" or "L.F.(m)" dimensions are to be determined by the Contractor from field conditions.
- Existing drainage facilities being utilized as a part of the drainage system, including three structures downstream of the project area, shall be cleaned out as directed by the Engineer. The cost to perform this work shall be not be covered as a separate pay item, and shall be considered incidental to the project.
- Proposed drop inlet tops with a height (H) less than the standard minimum shown in the VDOT Road and Bridge Standards shall be considered and paid for as Standard Drop Inlets for the type specified.
- When Standard CG-6 or Mod.CG-6 (see this sheet for Town's detail) is specified on a radius (such as at a street intersection), the Engineer may approve a decrease in the cross slope of the gutter to facilitate proper drainage.
- St'd.SL-I Safety slab locations are based on the assumed use of precast structures.If cast-in-place structures are utilized, and the interior chamber dimensions (length and width, or diameter) are less than four feet, the safety slabs shall not be installed.
- All excavated areas shall be restored and/or patched the same day. Prior to beginning the work, the Contractor shall submit an acceptable contingency plan to the Town outlining temporary protective measures to be utilized should the Contractor be unable to complete the restoration prior to the end of the work day.

PAVEMENT GENERAL NOTES

For bidding purposes, the Contractor shall utilize the typical section on this sheet. Prior to the start of construction, the Contractor shall obtain pavement cores (as directed by the Town) and submit a pavement design for approval by the Town. Proposed pavement is required in all locations adjacent to proposed curb (I' width) in accordance with VDOT's WP-2 standard.

INCIDENTAL GENERAL NOTES

- Certain trees shall be preserved as noted on plans or as directed by the Engineer.
- When Standard slope roundoffs would damage trees, bushes or other desirable vegetation, they shall be omitted when so ordered by the Town.
- Clearing and grubbing shall be confined to those areas needed for construction. No trees or shrubs in ungraded areas shall be cut without the permission of the Town.
- When no centerline alignment is shown for a proposed entrance, the entrance shall be constructed in the same location as the existing entrance.
- St'd.RM-I Right of Way Monuments shall be set by the Contractor. Any disturbed by the Contractor shall be restored at the Contractor's cost.
- The "Underground Utilities" survey data on this project has been provided by "Miss Utility."
- All pavement markings and traffic flow arrows shown on the roadway construction plans are schematic only. The actual location and application of pavement markings shall be in accordance with Section 704 of the applicable VDOT Road and Bridge Specifications, MUTCD, and as directed by the Town. All proposed pavement marking work shall be incidental to the project and not paid for as a separate pay item.
- The following outside sources, under contract with VDOT, have provided information on this pro ject:

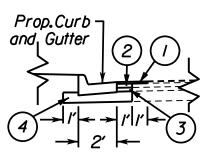
Hydraulic Design Rinker Design Associates, P.C. Sidewalk Design <u>Rinker Design Associates P.C.</u> Utility Designation "Miss Utility"

Utility Location "Miss Utility"

Survey Rinker Design Associates, P.C. If questions or problems arise during construction, please contact the Project Designer. DO NOT CONTACT THE OUTSIDE SOURCES.

9. All electronic plan assemblies will include the construction plans in one format: .pdf files.Only the .pdf files will be considered as part of the official plan assembly.

Recommended Pavement Typical



*For all locations with Prop.Curb and Gutter (per WP-2 St'd). For more information, see Pavement Note I on this sheet.

- Surface Course (1.5") Asph. Conc., Type SM-9.5A
- Intermediate Course (3") Asph. Conc., Type IM-19.0A
- Base Course (3") Asph. Conc., Type BM-25.0A
- Sub-base Course (8") Aggregate Base Material, Type I, Size No. 21B

PRIVATE ENTRANCES *See Plan Sheets for Sidewalk Typicals

TYPE I Crusher Run Aggr.

Asphalt 6" Crusher Run Asphalt Conc. Type Aggr. 25 or 26

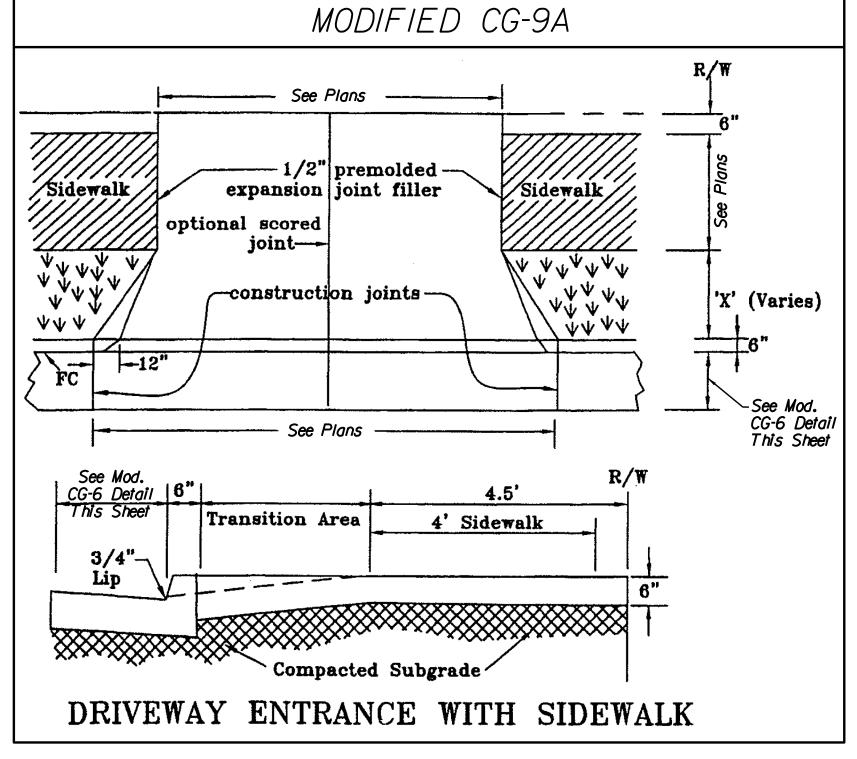
SM-9.5A or SM-9.5D @ 220 Lbs. per S.Y. 4" Aggr. Base Mat'l. Ty. I No. 21A or 21B

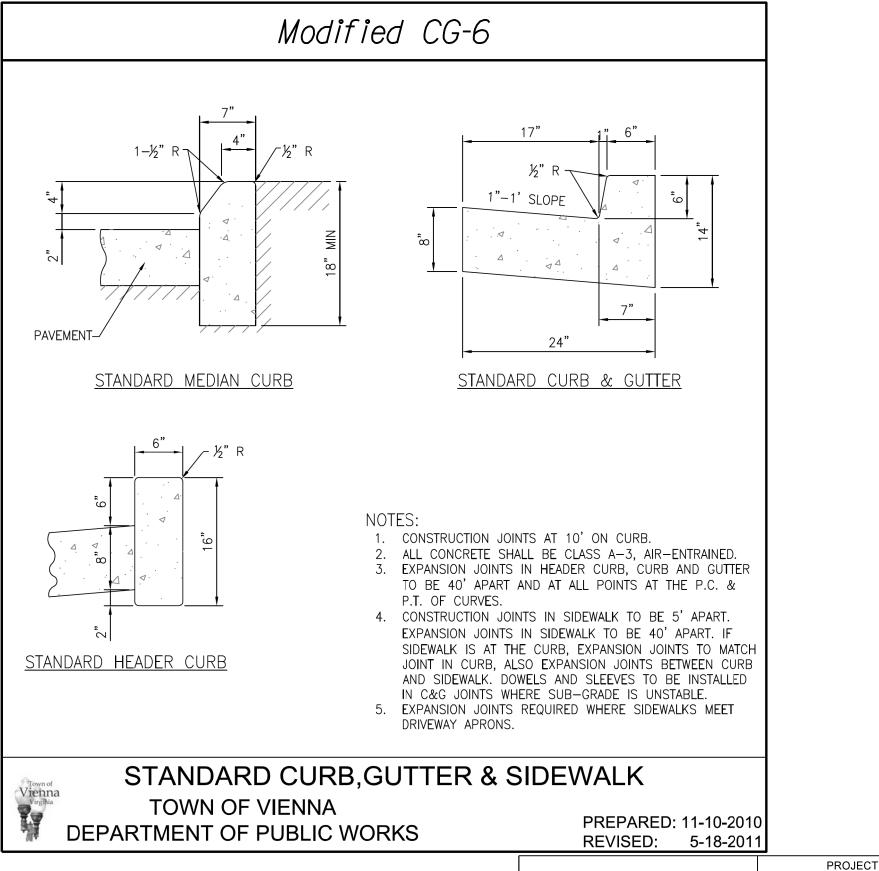
TYPE III

NOT TO SCALE

I. The type of entrance (I or III) to be constructed will be determined by the existing condition at the time of construction or as directed by the Town Engineer.

2. Contractor shall ensure all driveway grading activities provide for positive drainage during and post-construction of the project. Any ponding/drainage issues arising due to construction activities are the sole responsibility (including costs) of the Contractor. The Contractor shall coordinate with the Town and property owners/residents prior to the start of construction.





SHEET NO.

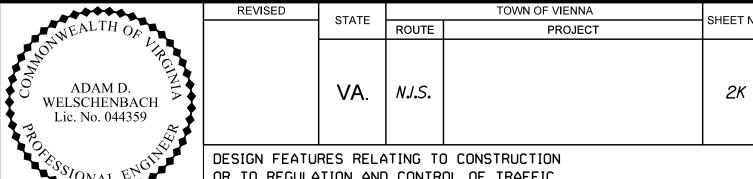
ROJECT MANAGER*Dennis Johnson_P.E.(T.own of Vienna)*

SUBSURFACE UTILITY BY "Miss_Utility" DATE: July 2013_

SURVEYED BY *Binker Design Associates P.C., DATE: July 2013*

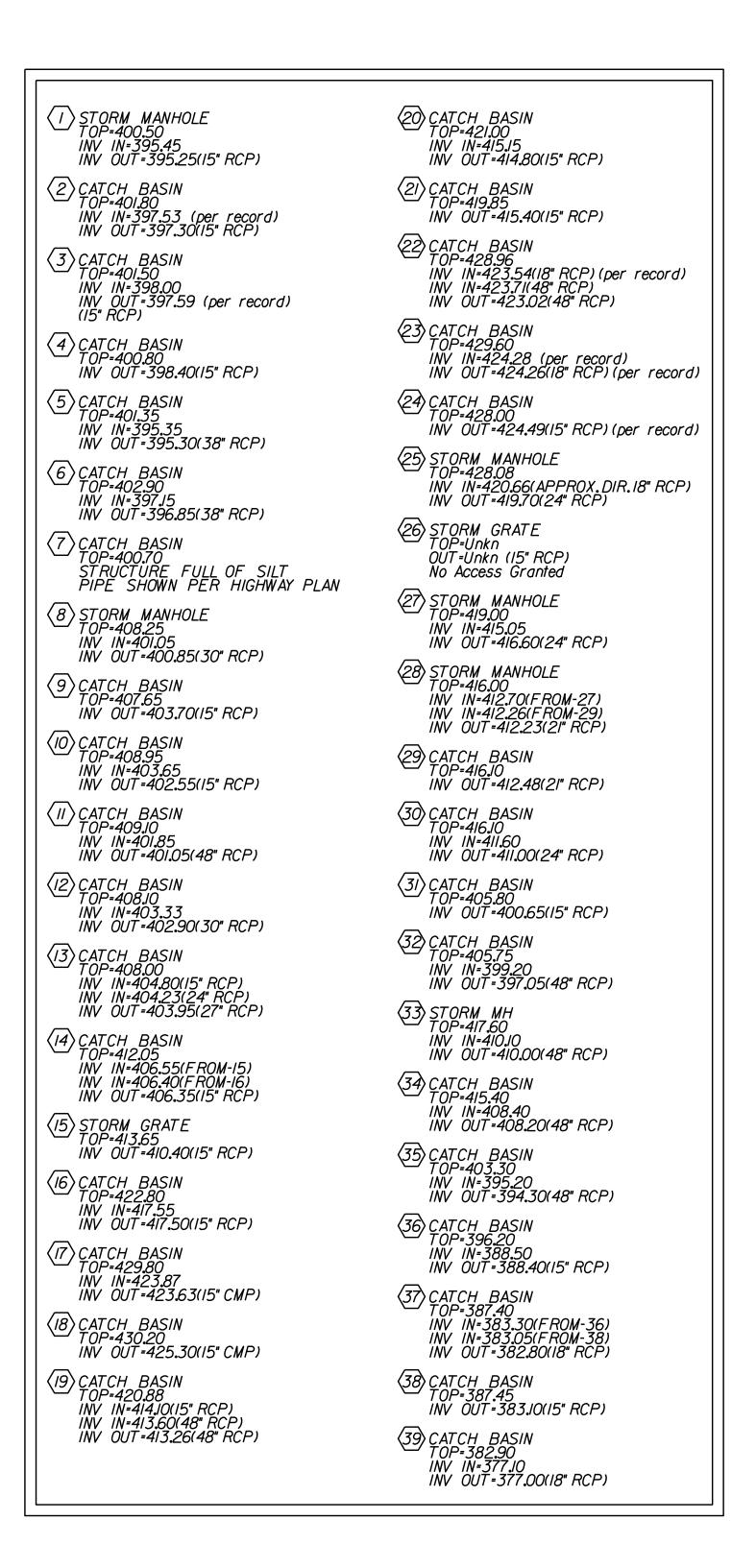
DESIGN BY Adam_D.Welschenbach_P.E.-Rinker_Design_Associates.P.C.(703) 368-7373

Existing Drainage & Sanitary Descriptions



OR TO REGULATION AND CONTROL OF TRAFFIC MAY BE SUBJECT TO CHANGE AS DEEMED NECESSARY BY THE DEPARTMENT

Rinker Design Associates Manassas, Virginia PROFESSIONAL ENGINEER



SANITARY SEWER A SAN MH TOP=406.90 INV IN=397.65 INV OUT=397.60(8") B SAN MH TOP=412,50 INV IN=403,35 INV OUT=403,30(8") SAN MH TOP=421,50 INV OUT=414,00(8") © SAN MH TOP=400.75 INV IN=392.45(FROM-A) INV IN=392.15(FROM-E) INV OUT=392.10(8") © SAN MH TOP=404.87 © SAN MH TOP=405.45 © SAN MH TOP=408.25 ® SAN MH TOP=410.80 INV IN=401.00(BOTH) INV OUT=400.95(8") () SAN MH TOP=413.30 ① SAN MH TOP=407.95 INV IN=401.65 INV OUT=401.60(8") © SAN MH TOP=409,25 INV IN=402,70 INV OUT=402,65(8") © SAN MH TOP=420,65 INV OUT=411.35(8") (M) SAN MH TOP=424.65 © SAN MH TOP=416,15 INV IN=410,30 INV OUT=410,25(8") © SAN MH TOP=421.60 INV IN=412.25 INV OUT=412.24(8") © SAN MH TOP=428JO INV IN=417.95 INV OUT=417.75(8") ® SAN MH TOP=438.35 INV OUT=428.85(8") S SAN MH TOP=423.36 ① SAN MH TOP=441.25

> PROJECT SHEET NO. 2K

PROJECT MANAGER*Dennis Jahnson_P_E.(Town of Vienna)* SURVEYED BY Binker Design Associates P.C., DATE: July 2013

Storm Drainage Computations

DESIGNED BY: JW

TOWN OF VIENNA PROJECT ROUTE ADAM D. WELSCHENBACH Lic. No. 044359 **VA**. | *N.*/.*S*. 2K(3) DESIGN FEATURES RELATING TO CONSTRUCTION

OR TO REGULATION AND CONTROL OF TRAFFIC MAY BE SUBJECT TO CHANGE AS DEEMED NECESSARY BY THE DEPARTMENT

Rinker Design Associates Manassas, Virginia PROFESSIONAL ENGINEER

10/28/2013

DATE: 10/28/2013

UNITS: ENGLISH

PRE-DEVELOPMENT INLET COMPUTATIONS

FORM LD-204

INLET COMPUTATIONS

DESIGN BY Adam_D.Welschenbach_P.E.-Rinker_Design_Associates.P.C.(703) 368-7373
SUBSURFACE_UTILITY_BY "Miss_Utility" DATE: July 2013_

ROU	'E: Maj	ole Aven	ue																									CHEC	KED	BY:	AW		UN	ITS:	ENGLISH
	Inlet																3														Sa	g Inlets	Only		
Number	Туре	Length (Ft)	Station	Draiange Area (Ac)	U	CA	Sum CA	I (In/Hr)	Q Incr.(CFS)	Oc Carryover (CFS)	<i>QT Gutter Flow</i> (CFS)	S Gutter Slope (F1/F1)	Sx Cross Slope (Ft/Ft)	T (Spread)(Ft)	W (Gutter Width) (Ft)	T/W	Sw (Gutter Slope) (F1/F1)	SW/Sx	Eo (App.9C-8)	0	N,S	Se	Computed Length (Ft)	L. Specified Length (Ft)	רעד	E (App.9C-18)	O Intercepted (CFS)	Ob Carryover (CFS)	Depth at Curb (In)	Allowable Ponding Depth (Ft)	Height of Curb Opening h (Ft)	q/p	Depth at Inlet (In)	T Spread @ SAG (Ft)	Remarks
ExO	6 <i>DI-4B</i>	8	14+17	2.78	0.48	1.33																													
							1.33	4.00	5.33	0.00	5.33	0.0230	0.0800	4.7	1.5	0.317	0.0833	1.0413	0.642	1.56	0.0866	0,1356	16,104	8	0.497	0.709	3.78	1.55	4.601			 _		—	
Exi	DI-3B	8	<i>16•45</i>	0.40	0.84	0.34																											<u> </u>	 	
	<i>, Di 30</i>	-	10 43	0.40	0.07	0.54	0.34	4.00	1.35	0.00	1.35	0.0083	0.0200	7.4	1.5	0.204	0.0833	4.1650	0.588	2.64	0.1466	0,1062	7,709	8	1.038	1,000	1.35	0.00	2.906					 	
							0.0	1000	1.00		1,00		0.0200					1.000	0.000			0.002	10.00		1.000	1.000	100							\dagger	
Exl	DI-4B	8	<i>16•45</i>	4.08	0.47	1.92																													
							1.92	4.00	7.68	3.98	11,66	0.0075	0.0200	18.3	1.5	0.082	0.0833	<i>4,</i> 1650	0.241	2.64	0.1466	0.0553	27.367	8	0.292	0.463	5 .4 0	6.26	5.542			<u> </u>		<u> </u>	T > 8.0 ft
	2 0/ 70	<u> </u>	75.40	0.05	0.00	0.05																											<u> </u>	—	0.444
Exiz	2 <i>DI-3C</i>	4	35•49	0.05	0.90	0.05	0.05	4.00	0,18	0.00																						 	 	┼	Back/Lt. Back/Lt.
				0.80	0.57	0.45	0.05	7.00	0.10	0.00																								 	Ahead/Rt.
		1		0.00	0.57	0.75	0.45	4.00	1.81	0.00		0.0500	0.0470	3.4	1.5	0.435	0.0833	1.7723		2,15														 	Ahead/Rt.
								1				0.0500						100 1 20						4			1,99		3.066	0.4	0.031	12.00	4.6	5.4	Weir Flow
Ex3	2 <i>DI-4B</i>	8	13.84	0.52	0.60	0.31																													
							0.31	4.00	1,24	6.26	7.50	0.0067	0.0200	15.8	1.5	0.095	0.0833	4,1650	0.282	2.64	0.1466	0.0613	20.659	8	0.387	0.586	4. 39	3,10	4.927						T > 8.0 ft
	2 2: 72		10.00			0.74									<u> </u>																	<u> </u>		—	
Ex3	6 <i>DI-3B</i>	4	10.00	0.39	0.87	0.34	+	400	1.37	204	<i>3.41</i>	00133	0.0200	100	15	0.150	00022	11650	0 4 47	261	OVACE	0.0856	14021	1	0.260	0.430	1.46	1.94	7577				 	 	T \ 90 ft
							0.34	4.00	11	2.04	J .4 1	0.0133	0.0200	10,0	<i>1.</i> 5	0.150	0.0033	4,1650	U.44/	Z.0 4	0.1400	0.0000	14.321	 "	0.200	0.430	1.46	1.34	3.533			\vdash		 	T > 8.0 ft
Ex3	7 <i>DI-3B</i>	4	10.00	0.39	0.75	0.29									+																				
							0.29	4.00	1,17	1.94	3,11	0.0115	0.0200	9.9	1.5	0,151	0.0833	4.1650	0.450	2.64	0.1466	0.0860	13.713	4	0.292	0.462	1.44	1,67	3.516						T > 8.0 ft

POST-DEVELOPMENT INLET COMPUTATIONS

FORM LD-204

INLET COMPUTATIONS

DESIGNED BY: JW ROUTE: Maple Avenue CHECKED BY: AW

	Inlet																														Sag	g Inlets	Only		
Number	Туре	Length (Ft)	Station	Draiange Area (Ac)	S	CA	Sum CA	I (In/Hr)	0 Incr.(CFS)	Oc Carryover (CFS)	OT Gutter Flow (CFS)	S Gutter Slope (F1/F1)	Sx Cross Slope (Ft/Ft)	T (Spread)(Ft)	W (Gutter Width) (Ft)	T/W	Sw (Gutter Slope) (Ft/Ft)	SW/Sx	Ео (Арр.9С-8)	0	Sʻw	Se	Computed Length (Ft)	L, Specified Length (Ft)	רינד	E (App.9C-18)	Q Intercepted (CFS)	Ob Carryover (CFS)	Depth at Curb (In)	Allowable Ponding Depth (Ft)	Height of Curb Opening h (Ft)	4/p	Depth at Inlet (In)	T Spread @ SAG (Ft)	Remarks
Ex06	DI-4B	8	14+17	2.76	0.48	1.32																													
							1.32	4.00	5.29	0.00	5.29	0.0230	0.0800	4.7	1.5	0.318	0.0833	1.0413	0.643	1.56	0.0866	0.1357	16.046	8.000	0.499	0.711	3.76	1.53	4.588					1	
ExIO	DI-3B	8	<i>16•4</i> 5	0.40	0.84	0.34																													
							0.34	4.00	1.35	0.00	1.35	0.0083	0.0200	7.4	1.5	0.204	0.0833	<i>4,</i> 1650	0.588	2.64	0.1466	0,1062	7.709	8.000	1.038	1.000	<i>1.</i> 35	0.00	2.906						
		_																					ļ						ļ				<u> </u>		
ExII	DI-4B	8	<i>16•4</i> 5	4.08	0.47	1.92		100	7.00	7.00		0.0075	0.000	10.7	ļ . . .	0.000	0.0077	4:050	0.04	0.04	0.466	0.055	7 07 707		0.000	0.407	5.40	0.00	5.5.40			 	 	<u> </u>	T > 00 6
							1.92	4.00	7.68	3.98	11,66	0.0075	0.0200	18.3	1.5	0.082	0.0833	4,1650	0.241	2.64	<i>0.14</i> 66	0.0553	3/.36/	8.000	0.292	0.463	5 .4 0	6.26	5.542				├──		T > 8.0 ft
ExI2	DI-3C	4	<i>35•49</i>	0.07	0.81	0.06																	<u> </u>												Back/Lt.
							0.06	4.00	0.23	0.00																									Back/Lt.
				0.80	0,61	0.49																													Ahead/Rt.
							0.49	4.00	1.94	0.00			0.0470	<i>3.</i> 6	1.5	0.422	0.0833	1.7723		<i>2,</i> 15															Ahead/Rt.
											2,17	0.0500												4.000			2,17		3.248	0.4	0.031	12.00	4.7	5.8	Weir Flow
Ex32	DI-4B	8	13•84	0.52	0.60	0.31					<u> </u>																		<u> </u>				<u> </u>	<u> </u>	
							0.31	4.00	1.24	6.26	7.50	0.0067	0.0200	15.8	1.5	0.095	0.0833	<i>4,1650</i>	0.282	2.64	0,1466	0.0613	20.659	8.000	0.387	0.586	4.39	3,10	4.927			 	 		T > 8.0 ft
Ex36	DI-3B	4	10.00	0.39	0.87	0.34																	1						1				 		
	5. 55	•		0.00		1 0.0 .	0.34	4.00	1.37	2.04	3.41	0.0133	0.0200	10.0	1.5	0,150	0.0833	4,1650	0.447	2.64	0.1466	0.0856	14.921	4.000	0.268	0.430	1.46	1.94	3.533						T > 8.0 ft
Ex37	DI-3B	4	10.00	0.39	0.75	0.29																										<u> </u>	<u> </u>		
							0.29	4.00	1,17	1.94	3,11	0.0115	0.0200	9.9	1.5	0,151	0.0833	<i>4,1650</i>	0.450	2.64	0.1466	0.0860	13.713	4.000	0.292	0.462	1.44	1.67	3.516			<u> </u>	<u> </u>		T > 8.0 ft

PROJECT	SHEET NO
	2K(3)

Storm Drainage Computations

DESIGNED BY: JW

DATE: 10/28/2013

*****	REVISED	STATE		TOWN OF VIENNA	SHEET
WEALTH OF		SIAIL	ROUTE	PROJECT	SHEET
ADAM D. WELSCHENBACH Lic. No. 044359		VA.	N.J.S.		2K(4
SONAL ENGIN	DESIGN FEATU OR TO REGULA			O CONSTRUCTION OL OF TRAFFIC	

*** MAY BE SUBJECT TO CHANGE AS DEEMED NECESSARY BY THE DEPARTMENT Rinker Design Associates

Manassas, Virginia PROFESSIONAL ENGINEER

PRE-DEVELOPMENT STORM COMPUTATIONS, 10-YEAR STORM

FORM LD-229

STORM SEWER DESIGN COMPUTATIONS

STORM SEWER DES	IGN COMP	UTATION	N S																	DESIG	ENED B	Y: JW			DATE	: /(1/28/2013
STORM FREQUENCY	_1	0-Year																		CHEC	KED B	Y: AW	•		UNIT	S: <i>E</i>	NGLISH
5:	From F	Point	To Pol	int	Drain		C	4	Total	Rain	Rur		Invert El	evations	Length	Slope	Size	Shape	Number Capac	ityFriction	η		nal Flow			Flow	
Pipe No.	Reference	Sta.	Reference	Sta.	Area "A" (Acre)	Runoff Coeff. "C"	Incre- ment	Accum- ulated	Inlet Time (Minutes)		Lateral (CFS)	Total Q (CFS)	Upper End	Lower End	of Pipe		Dia.or Span/Rise (In)		of Pipes	1 Slope	Denth of	Area of Flow, An (SqFt)	Hm (Ft)	Vn (Ft/Sec)	En (Ft)		Remarks
ExOltoEx36	ExOI		Ex36	10.00	0.00		0.00	<i>2.</i> 35	10.32	5.39	0.00	12.77	<i>395,25</i>	388.50	155.00	0.04355	<i>1</i> 5	Circular	1 13.4	3 0.0408 (0.97	1.02	0.38	12.5	<i>3.40</i>	12	
Ex36toEx37	Ex36	10•00	Ex37	10.00	0.39	0 . 87	0.34	2. 69	10.52	5.3 5	0.00	14.40	<i>388.40</i>	<i>383.30</i>	298.00	0.01711	<i>1</i> 5	Circular	1 8.4	0.05190	1.25	1.23	0.31	11.7	3.39	<i>2</i> 5	Pressure Flow
Ex37toEx39	Ex37	10•00	Ex39		0.39	0.75	0.29	<i>3.44</i>	10.95	5 .2 7	0.00	18,12	<i>382.80</i>	<i>377,</i> 10	346.00	0.01647	18	Circular	1 13.4	3 0.03100	1.50	1.77	0.38	10.3	3.13	34	Pressure Flow
ExI2toEx08	ExI2	<i>35•49</i>	Ex08		0.85	0.59	0.50	11.81	11,16	5.23	0.00	61.79	402.90	401.05	101.00	0.01832	30	Circular	/ 55.5	2 0.0236	2.50	4,91	0.63	12.6	4.9 6	8	Pressure Flow
Ex08toEx06	Ex08		Ex06	14+17	0.00		0.00	11.81	11,29	5 . 21	0.00	61.79	400.85	<i>397.1</i> 5	288.00	0.01285	30	Circular	1 46.5	0.0236	2.50	4,91	0.63	12.6	4.9 6	23	Pressure Flow
Ex06toEx05	Ex06	14•17	Ex05	II · 79	2.78	0.48	1.33	13.15	11.67	5 . 14	0.00	<i>67.53</i>	<i>396.</i> 85	<i>395.35</i>	232.00	0.00647	<i>3</i> 6	Circular	1 53.6	5 <i>0.01060</i>	3.00	7.07	0.75	9.6	4.42	24	Pressure Flow
ExIOtoExII	ExIO	<i>16•4</i> 5	ExII	<i>16•4</i> 5	0.40	0.84	0.34	0.53	5 . 07	<i>6.</i> 75	0.00	<i>3.</i> 59	<i>402,</i> 55	401.85	78.00	0.00897	<i>1</i> 5	Circular	l 6.12	0.0032	0.69	0.69	0.33	5.2	1,11	15	
ExIItoEx32	ExII	<i>16•4</i> 5	Ex32	13•84	4.08	0.47	1.92	19.50	56.90	2.23	0.00	<i>57.94</i>	401 . 05	399 . 20	260.00	0.00712	48	Circular	1 121.	0.00170	1.95	6.08	0.98	9. 5	<i>3.36</i>	27	
Ex32toEx35	Ex32	13•84	Ex35	II•67	0.52	0.60	0.31	19.99	<i>57.35</i>	2.22	0.00	<i>59,16</i>	<i>397.</i> 05	<i>395,20</i>	210.00	0.00881	48	Circular	1 1342	3 0.00180	1.85	5.70	0.95	10.4	<i>3.</i> 53	20	

POST-DEVELOPMENT STORM COMPUTATIONS, 10-YEAR STORM

FORM LD-229

STORM SEWER DESIGN COMPUTATIONS

STORM	FREQUENCY	10-Year

STORM FREQUENCY	. []	10-Year]																		CHECK	KED BY	: AW			UNITS	S: <i>E</i>	ENGLISH
Diag	From F	Point	To Po	nint	Drain		C		Total	Rain		nof f		levations	Length of Pipe	Slope	Size	Shape	Number	Capacity	Friction			al Flow		_	Flow	
Pipe No.	Reference	Sta.	Reference	Sta.	Area "A" (Acre)	Runoff Coeff. "C"	Incre- ment	Accum- ulated	Inlet Time (Minutes)		Lateral (CFS)	Total Q (CFS)	Upper End	Lower End	1	(Ft/Ft)	Dia.or Span/Rise (In)		of Pipes	(CFS)	Slope (Ft/Ft)	Depth of Flow,dn (Ft)	Area of Flow, An (SqFt)	Hm (Ft) (Vn 'Ft/Sec)	En (Ft)	Time (Sec)	Remarks
Pr3-2toEx36	Prop3-2		Ex36	10.00	0.00		0.00	2.47	10.30	5 . 39	0.00	13.41	395.25	388.50	155.00	0.04355	15	Circular	1	13.48	0.04500	1.02	1,07	0.38	12.5	<i>3.</i> 45	12	
Ex36toEx37	Ex36	10.00	Ex37	10•00	0.39	0 . 87	0.34	2,81	10.51	5.3 5	0.00	15.04	<i>388.40</i>	<i>383.30</i>	298,00	0,01711	<i>1</i> 5	Circular	1	<i>8.</i> 45	0.05660	1.25	1.23	0.31	12.3	3.58	24	Pressure Flow
Ex37toEx39	Ex37	10•00	Ex39		0.39	<i>0.</i> 75	0.29	<i>3.</i> 55	10.92	5 . 28	0.00	18.71	382.80	<i>377.</i> J0	346.00	0.01647	18	Circular	1	13.48	0.03310	1.50	1.77	0.38	10.6	3.24	33	Pressure Flow
ExI2toEx08	ExI2	<i>35•49</i>	E x08		0.87	0.63	0.54	12,01	11,15	5.23	0.00	62.81	402.90	401.05	101.00	0 . 01832	30	Circular	1	55.52	0 . 02440	2,50	4. 91	0.63	12.8	5.04	8	Pressure Flow
Ex08toEx06	Ex08		Ex06	14+17	0.00		0.00	12.01	11.29	5.21	0.00	62.81	400.85	<i>397,1</i> 5	288.00			Circular	1		0.02440		4.91	0.63	12.8	5.04	23	Pressure Flow
Ex06toEx05	Ex06	14+17	Ex05	11•79	2.76	0.48	1.32	13.33	11.66	5,14	0.00	68.51	<i>396.</i> 85	395.35	232.00	0.00647	36	Circular	1	<i>53.</i> 65	0.01090	<i>3.00</i>	7,07	0.75	9.7	4.46	24	Pressure Flow
ExIOtoExII	ExIO	<i>16•45</i>	ExII	<i>16•45</i>	0.40	0.84	0.34	0.56	5.07	<i>6.</i> 75	0.00	3.80	<i>4</i> 02 . 55	401.85	78.00	0 . 00897	15	Circular	1	6,12	0.00360	0.71	0.72	0.34	5.3	1,14	15	
ExIItoEx32	ExII	16•45	Ex32	13.84	4.08	0.47	1.92	19.57	56.90	2.23	0.00	58.38	401,05		260.00			Circular	1	-			6,11	0.99	9.6	<i>3.3</i> 7	27	
Ex32toEx35	Ex32	13:84	Ex35	II•67	0.52	0.60	0.31	20.06	<i>57.35</i>	2.22	0.00	59.61	397.05	<i>395,20</i>	210.00	0.00881	48	Circular	1	134.83	0.00180	1.86	<i>5.73</i>	0.95	10.4	3.54	20	

PROJECT	SHEET NO
	2K(4)

9.5 0.353

5.2 0.104

13.7

Storm Drainage Computations

DESIGNED BY: JW

CHECKED BY:

0.02 0.029 0.941 0.688 0.941 YES 0.47 0.84 399.24 405.25

0.02 0.060 1.438 4.279 1.438 YES

0.00 0.000

Ad j.Ht

TOWN OF VIENNA ROUTE PROJECT ADAM D. WELSCHENBACH Lic. No. 044359 VA. N.J.S. 2K(5) DESIGN FEATURES RELATING TO CONSTRUCTION OR TO REGULATION AND CONTROL OF TRAFFIC

MAY BE SUBJECT TO CHANGE AS DEEMED

NECESSARY BY THE DEPARTMENT

Rinker Design Associates PROFESSIONAL ENGINEER

10/28/2013

O.K.

ENGLISH

UNITS:

1.16 403.56

Top of MH

Manassas, Virginia

PRE-DEVELOPMENT HGL COMPUTATIONS

FORM LD-347

HYDRAULIC GRADE LINE ANALYSIS

NCIDENC	E PROBABIL	ITY [10-Year					
INLET		INVERT	DEPTH	OUTLET	DIA.	DESIGN	LENGTH	FRICTION
OR JUNCTION	STA.	EL.	OF FLOW	WATER	PIPE	DISCH.	PIPE	SLOPE, Sfo
	33	OUTFLOW	OUTFLOW	SURF ACE	Do	Qo	Lo	(FT/FT)
JONET ION		PIPE	PIPE	ELEV.	(In/mm)	(CFS/CMS)	(Ft/M)	(M/M)
<i>(1)</i>	(2)			(3)	(4)	(5)	(6)	(7)

OR	STA.	EL.	OF FLOW	WATER	PIPE	DISCH.	PIPE	SLOPE, Sfo	LOSS		Contr.			Hî (Expn)	SKEW		Bend	Sum	SURF ACE	1.3	Shaping?	0.5	FINAL	Water	Top of Inlet	Ad justment
JUNCTION		OUTFLOW	OUTFLOW	SURF ACE	<u>Do</u>	Qo	Lo	(FT/FT)	Hf	Vo	Но	Vi	Vi*2/2g	0.35*MAX.	Angle	K	Н	HL	FLOW	Ht		Ht	Н	Surface	Elev.	
		PIPE	PIPE	ELEV.	(In/mn	m) (CFS/CMS)	(Ft/M)	(M/M)	(Ft/M)		(Ft/M)			(Vî2/2g)			(Ft/M)	(Ft/M)		(Ft/M)	Y/N	(Ft/M)	(Ft/M)	Elevation	APPROX.	
(1)	(2)			(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)		(12)	(13)		(14)	(15)		(16)		(16)	(17)	(18)	(19)	
Ex39																								<i>378.30</i>		
Ex37	10•00	<i>377,</i> 10	1.50	<i>378.</i> 60	18	18,12	<i>34</i> 6	0.03112	10.767	10.3	0.408	11.7	2.1	0.748	90	0.70	0.069	1,225	1.544	1,225	YES	0.61	II . 38	<i>389.98</i>	<i>386.90</i>	ADJUST
Ex36	10+00	383.30	1.25	389.98	15	14.40	298	0.05195	<i>15.480</i>	11.7	0.534	12.5	2.4	0.849	17	0,21	0.501	1.884	1.830	1.884	YES	0.94	<i>16.42</i>	406.40	<i>3</i> 95 . 70	ADJUST
Ex0I		388.50	1.25	406.40	<i>1</i> 5	12,77	155	0.04085	<i>6.332</i>	12.5	0.606	8.0	1.0	0.349	58	0.54	0.310	1,265	0.000	1,265	YES	0.63	<i>6.9</i> 6	413.37	400 . 50	ADJUST
Ex05																								397.88		
Ex06	14+17	<i>395.35</i>	<i>3.00</i>	<i>398.</i> 35	36	67.53	232	0.01072	<i>2.486</i>	9.6	0.354	12.6	2. 5	0.861	0	0.00	0.000	1.215	<i>6.848</i>	1,215	YES	0.61	<i>3.</i> 09	401.44	402.40	O.K.
Ex08		397,15	2.50	401.44	30	61.79	288	0.02372	6.831	12.6	0.615	12.6	2.5	0.861	<i>82</i>	0.65	1.589	<i>3.</i> 065	0.000	<i>3.</i> 065	YES	1.53	<i>8.36</i>	409.81	408.25	ADJUST
ExI2	<i>35•49</i>	401.05	2.50	409,81	30	61.79	101	0.02372	2.396	12.6	0.6/5	14.9	<i>3.</i> 5	1,208	65	0.58	2.001	<i>3.</i> 825	2.605	<i>3.82</i> 5	YES	1,91	4.31	414,12	407,60	ADJUST
Ex35																								<i>398.40</i>		

1.4 0.494

2.9 1.025

0.047

JUNCTION LOSS

POST-DEVELOPMENT HGL COMPUTATIONS

395.20 4.00 398.40 48 59.16 210 0.00177 0.372 10.4 0.418 9.5

4.00 | 402.40 | 48 | 57.94 | 260 | 0.00170 | 0.442 |

FORM LD-347

Ex32

ExII Ex10

HYDRAULIC GRADE LINE ANALYSIS

13-84

HYDRAUL	IC GRADE I	LINE AN	ALYSIS																	DE	SIGNED	BY:	JW	D	ATE: /	0/28/2013
INCIDENC	E PROBABII	_ITY [10-Year																	CH	ECKED	BY:	AW	U	NITS: E	ENGLISH
INLET		INVERT	DEPTH	OUTLET	DIA.	DESIGN	LENGTH	FRICTION	FRICTION			JU	NCTION	LOSS		•				Ad j.Ht	Inlet			Inlet	Top of MH	
OR	STA.	EL.	OF FLOW	WATER	PIPE	DISCH.	PIPE	SLOPE, Sfo	LOSS		Contr.			Hî (Expn)	SKEW		Bend	Sum	SURF ACE	1.3	Shaping?	0.5	FINAL	Water	Top of Inlet	Ad justment?
JUNCTION		OUTFLOW	OUTFLOW	SURF ACE	Do	Qo	Lo	(FT/FT)	Hf	Vo	Но	Vī	Vi*2/2g	0.35*MAX.	Angle	K	Н	HL	FLOW	Ht		Ht	н	Surface	Elev.	
JONETION		PIPE	PIPE	ELEV.	(In/mm)	(CFS/CMS)	(Ft/M)	(M/M)	(Ft/M)		(Ft/M)			(V12/2g)			(Ft/M)	(Ft/M)		(Ft/M)	Y/N	(Ft/M)	(Ft/M)	Elevation	APPROX.	
(1)	(2)			(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)		(12)	(13)		(14)	(15)		(16)		(16)	(17)	(18)	(19)	
Ex39																								378.30		
Ex37	10.00	<i>377,</i> 10	1.50	<i>378.</i> 60	18	18.71	346	0.03315	11 .4 69	10.6	0.435	12.3	2.3	0.816	90	0.70	0.065	1.316	1 . 546	1.316	YES	0.66	12.13	390.73	<i>386.90</i>	ADJUST
Ex36	10•00	383.30	1.25	390.73	15	15.04	298	0.05664	16.880	12.3	0.583	12.5	2.4	0.852	17	0.21	0.503	1.938	1.831	1.938	YES	0.97	17.85	408.58	<i>395.</i> 70	ADJUST
Prop3-2		388.50	I . 25	408.58	/5	13.41	155	0.04506	<i>6.985</i>	12.5	0.609	<i>8.</i> 4	IJ	0.379	52	0.51	0.254	1,242	0.000	1,242	YES	0.62	7,61	416,18	400.50	ADJUST
Ex05																								397.88		
Ex06	14-17	395.35	3.00	<i>398.</i> 35	<i>3</i> 6	68.51	232	0.01103	2.558	9.7	0.365	12.8	2.5	0.890	0	0.00	0.000	1.254	6.799	1.254	YES	0.63	3.19	401.54	402.40	O.K.
Ex08		<i>397,</i> 15	2.50	401 . 54	30	62.81	288	0.02451	7.060	12.8	0.636	12.8	2.5	0.890	82	0.65	1.642	<i>3,</i> 167	0.000	<i>3,</i> 167	YES	1.58	8.64	410,18	408.25	ADJUST
ExI2	<i>35</i> •49	401.05	2.50	410,18	30	62.81	101	0.02451	2.476	12.8	0.636	15.1	<i>3.</i> 5	1,240	65	0.58	2.054	3.930	2.840	<i>3.930</i>	YES	1.97	4.44	414,62	407,60	ADJUST
Ex35																								<i>398.40</i>		+
Ex32	<i>13</i> •84	395.20	4.00	<i>398.40</i>	48	59.61	210	0.00180	0.378	10.4	0.420	9.6	1.4	0.496	1	0.02	0.029	0.945	0.688	0.945	YES	0.47	0.85	399.25	405.25	O.K.
ExII	<i>16•45</i>	399.20	4.00	402.40	48	<i>58.38</i>	260	0.00173	0.449	9,6	0.354	13.7	2.9	1.027	1	0.02	0.060	1.442	4.2 79	1.442	YES	0.72	1,17	403.57	408,60	O.K.
ExIO	<i>16•45</i>	401.85	1.25	<i>403.</i> 57	15	<i>3.80</i>	78	0.00362	0.282	5.3	0,107	<i>3.</i> 0	O.J	0.050	0	0.00	0.000	0,158	2.274	0.205	YES	OJO	0.38	403.95	408.45	O.K.

PROJECT

2K(6)

ROJECT MANAGER*Dennis_Johnson_P_E.(Town of Vienna)* SURVEYED BY *Binker Design Associates P.C., DATE: July 2013* DESIGN BY Adam_D.Welschenbach_P.E. - Rinker_Design_Associates_P.C.(703) 368-7373 SUBSURFACE UTILITY BY "Miss_Utility" DATE: July 2013_

Outfall Analysis

****	REVISED	STATE		
WEALTH OF		SIAIL	ROUTE	
ADAM D. WELSCHENBACH Lic. No. 044359		VA.	N.J.S.	
ESSIONAL ENGINE	DESIGN FEATUR OR TO REGULA MAY BE SUBJE	TION AND	CONTR	OL O
***	INHI DE SOBJE	יט נו	THINGE F	וט כוּ

INSTRUCTION OF TRAFFIC DEEMED NECESSARY BY THE DEPARTMENT

Rinker Design Associates Manassas, Virginia PROFESSIONAL ENGINEER

OUTFALL ANALYSIS SUMMARY TABLE

					141 141 .	21101	1 / 1							CHECKED	BY:	AW UNITS: ENGL!	
			Drainage Area (ac)				I-Value		[Outfall Rec	eiving Channe	<i>?</i> /			
	Outfall	Outf all	_	Added	_	l Tc	(in	/hr)	(c	fs)	Channel	Natural	Manmade	Stormdrain	Outf all		
Outfall	1	Total Area	Impervious (C=0.90)	Cw	(min)	2-yr	IO-yr	2-yr 10-yr		Velocity 2-yr Check (ft/s)	Channel 2-yr Avail. Depth (in)	Channel 10-yr Avail. Depth (in)	System IO-yr Pipe Capacity (cf s)	Adequacy Yes/No			
Outfall *I	Maple Avenu	<i>i</i> e															
Existing	850' West	Ex.39	5 . 54	-	0.62	11,0	4.04	5 . 27	13.83	<i>18.</i> 05	N/A	N/A	N/A	13.48	No	Existing Storm System	
Post-Dev.	850' West	Ex.39	5 . 54	0.20	0.64	11.0	4.04	5 . 27	14.30	18.67	N/A	N/A	N/A	13.48	No	Existing Storm System	
								Change •	0.47	0.61							
Outfall *2	Maple Avenu	e Service Dr	ive														
Existing	<i>II∙80 LT</i>	Ex.05	26.34	-	0.50	11.7	3.93	5,14	51.66	67.51	N/A	N/A	N/A	<i>53.</i> 65	No	Existing Storm System	
Post-Dev.	II•80 LT	Ex.05	26.34	0.31	0.51	11.7	3.93	5,14	52.39	68.46	N/A	N/A	N/A	<i>53.</i> 65	No	Existing Storm System	
								Change •	0.72	0.95							
Outfall *3	Maple Avenu	ne															
Existing	11•70 RT	Ex.35	41.58	-	0.50	<i>57.4</i>	1.57	2.22	<i>32.48</i>	45.77	N/A	N/A	N/A	134.83	Yes	Existing Storm System	
Post-Dev.	II•70 RT	Ex.35	41.58	OJI	0.50	<i>57.4</i>	I . 57	2.22	<i>32.61</i>	45.96	N/A	N/A	N/A	134.83	Yes	Existing Storm System	
		,						Change •	0,13	0.18							

Outfall Narrative

<u>Project Overview:</u> This outfall analysis is for five projects located in the same residential area in the Town of Vienna, Virginia. These five projects are linear pedestrian access improvement projects that will be constructed at approximately the same time. Since these projects all have the same three outfalls, these three outfalls have been analyzed collectively for the pre-developed condition (prior to any of the projects being constructed) and the post-developed condition (after all five projects have been constructed). The projects propose to add a 5' concrete sidewalk for a total of 6,180 feet. The sidewalks will be installed along the east side of Westbriar Drive NE, the west side of Westbriar Drive NE, the south side of the Maple Avenue Service Drive NE, the east and west sides of Saint Bernard Drive NE. and the east and west sides of Saint Andrews Drive NE. In the existing condition, these roadways have curb and gutter and existing closed storm sewer systems. The projects are located in the Wolftrap Creek watershed management area which is within the greater Difficult Run watershed.

Outfall Descriptions: Drainage for these projects impact three outfalls as described below.

Outfall *I - This outfall is existing storm sewer. The drainage consists of 5.54 acres of sheetflow from the roadway, existing median, and surrounding residential areas. These projects increase the amount of impervious area going to this outfall by 0.20 acre, and the C-value increases slightly from 0.62 to 0.64. The peak flows for the 2- and 10-year storm events increase a negligible amount by 0.47 cfs and 0.61 cfs respectively as shown in the Outfall Analysis Summary Table on this sheet. Storm Computations on Sheets 2K(3) through 2K(5) for three pipes downstream of the projects show that the existing system is not adequate to convey the flows in the existing condition. This is true also for the proposed condition.

Outfall *2 - This outfall is existing storm sewer. The drainage consists of 26.34 acres of sheetflow from the roadway, existing median, and surrounding residential areas. These projects increase the amount of impervious area going to this outfall by 0.31 acre, and the C-value increases slightly from 0.50 to 0.51. The peak flows for the 2- and 10-year storm events increase a negligible amount by 0.72 cfs and 0.95 cfs respectively as shown in the Outfall Analysis Summary Table on this sheet. Storm Computations on Sheets 2K(3) through 2K(5) for three pipes downstream of these projects show that the existing system is not adequate to convey the flows for the IO-year storm in the existing condition or the proposed condition. The existing system is adequate to convey the flows for the 2-year storm for both the existing and proposed conditions.

Outfall *3 - This outfall is existing storm sewer. The drainage consists of 41.58 acres of sheetflow from the roadway, existing median, and surrounding residential areas. These projects increase the amount of impervious area going to this outfall by O.JI acre, however the C-value remains the same at 0.50. The peak flows for the 2- and IO-year storm events increase a negligible amount by 0.13 cfs and 0.18 cfs respectively as shown in the Outfall Analysis Summary Table on this sheet. Storm Computations on Sheets 2K(3) through 2K(5) for three pipes downstream of these projects show that the existing system is adequate to convey these increased flows.

<u>Drainage Area</u>: The total project area for these projects is 7.03 acres. These projects combined propose the addition of 0.61 acre of impervious area within 2.14 acres of disturbed area.

<u>Final Opinion</u>: The existing storm sewer has adequate capacity to convey the proposed flow for Outfall *3.It is our opinion that the requirements of MS-19 are satisfied for Outfall *3 and that Outfall *3 will not be adversely impacted by the proposed walkway addition. Outfall *I and Outfall *2 at their points of analysis are inadequate in the existing condition. The increases in peak runoff to these two outfalls due to the proposed projects are negligible. There are no known flooding problems at the points of analysis for Outfall *I and Outfall *2. However, Outfall *I and Outfall *2 do not satisfy the requirements of MS-19 in the existing condition. The Town has determined that it is not feasible to satisfy the requirements of MS-19 for the proposed condition as part of the scope of these pedestrian access improvement projects.

WQN/WQL Narrative

10/28/2013

DESIGNED BY: CW

These projects propose to add a 5' concrete sidewalk for a total of 6,180 feet. The sidewalks will be installed along the east side of Westbriar Drive NE, the west side of Westbriar Drive NE, the south side of the Maple Avenue Service Drive NE, the east and west sides of Saint Bernard Drive NE, and the east and west sides of Saint Andrews Drive NE.The projects are located in the Wolftrap Creek watershed management area which is within the greater Difficult Run watershed. These projects have three outfalls as described in the Outfall Narrative. The Drainage Maps can be found on sheets 2K(I) and 2K(2) and Storm Computations can be found on sheets 2K(3), 2K(4), and 2K(5). From the computations, it can be seen that:

- I. There will be negligible increases in peak flow rates for all outfalls. 2. The existing storm sewer system is adequate to convey the flows for Outfall *3 but is not adequate for the existing or proposed conditions of Outfall *I and Outfall *2 at the points of analysis.
- 3. There are no additional anticipated flooding or erosion problems downstream.

No water quantity control requirements are required for Outfall *3. No water quantity control requirements are proposed for Outfall *1 and Outfall *2.

Further, at the points of analysis, it can be seen that:

I. The increase in peak flow rates downstream of the discharge points are negligible. 2. There are no additional anticipated flooding or erosion problems downstream of the discharge points.

Additionally, per the Town of Vienna's MS-4 permit and per direction from the Town to RDA, public road and linear projects within the Town are exempt from the performance criteria for water quality requirements as long as the plan provides adequate erosion and sediment controls. The Erosion and Sediment Controls for this project can be found on the IL and IM sheet series.

PROJECT	SHEET N
	2K(6.

