

NB+C Engineering Services

Rooftop Structural Analysis

Prepared for T-Mobile: L700 4x2 Installation

SITEINFORMATION

Address	301 Maple Ave West
	Vienna, VA 22180
	Lat: 38.897942°
	Long: -77.270294°
T-Mobile Site Number	7WAC050A
T-Mobile Site Name	White Oak Tower
NB+C Project Number	100291
Date	June 15, 2020

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1.0 INTRODUCTION

The existing structure is a 81'-6" tall building located in Vienna, VA.

T-Mobile has proposed to reconfigure the site and install new antennas as shown in the table below. A structural analysis was performed to see if the new loads are safely supported by the roof structure and to verify if the existing structure is in compliance with the applicable codes and standards. Information we have received and used for this analysis includes:

- RFDS provided by T-Mobile dated May 01, 2020
- Site Audit Photos dated September 04, 2019
- Construction Drawings by NB+C Engineering Services, dated June 10, 2020

2.0 APPURTENANCES LOADING

As per the information provided to us, the following tables show the final and existing antenna and equipment installation by T-Mobile.

Mounting Level (ft)	Flovation	Number of Antennas	Antenna Manufacturer	Antenna Model	Carrier	Feed Line Size (in)	Note
		4	RFS	APXVAAR24_43-U-NA20 (95.9"x24.0"x8.7", 128.0lbs)		(4) 6x12	
74'-0" 79'-0"	74'-0" 79'-0"	4	Ericsson	Radio 4449 B71 + B85 (13.4"x16.5"x5.9", 46.0lbs)	T-Mobile	Hybrid	-
		2	Ericsson	KRY 112 489/2 (11.0"x6.1"x3.9", 15.4lbs)		Coax	

 Table 1 – Proposed/Final Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Carrier	Feed Line Size (in)	Note
		4	Ericsson	AIR32DB B66A/B2A		(4) 6x12 Hybrid ¹ (6) 1-1/4"	1
74'-0"	74'-0"	2	Andrew	TMBXX-6516-A2M			
79'-0"	79'-0"	'9'-0" 79'-0" 2 Commscope SBNHH-1D65C ¹⁻¹	T-Mobile	Coax ¹	2		
		4	Ericsson	KRY 112 489/2		(4) 7/8"	1
		2	-	Twin Style 1B		Coax ²	

Note:

1. Existing equipment to remain.

2. Existing equipment to be removed, was not considered in this analysis.

3.0 ASSUMPTIONS

This report is based on the theoretical capacity of the existing structural elements and is not an assessment of the overall suitability of the existing Structure or its components for any particular use other than specified here in this report:

- This report makes no warranties, expressed and/or implied, and disclaims any liability arising from material, fabrication and erection of the existing Structure and any other existing or proposed components or appurtenances.
- All proposed and existing antennas, mounts, coaxial cables and appurtenances are assumed to be properly installed and configured according to manufacturer requirements.
- All existing structural elements are assumed to be in place and in good condition, and were previously designed and constructed in accordance with applicable codes and standards.
- Existing anchorage to penthouse wall assumed to be ½" diameter threaded rods with Hilti HY70 adhesive and 3 1/8" min. embedment.
- Contractor to verify existing site condition including the existing structure prior to fabrication and construction. In the event the existing structure conditions are different than the assumptions made in this report, this has to be brought to the structural engineer's attention before proceeding any further with bidding, fabrication and/or erection.

4.0 APPLICABLE CODES AND STANDARDS

The existing structure was analyzed/designed per the provisions of following applicable codes and standards:

- 2015 Virginia Construction Code
- ANSI/TIA-222-G Structural Standards for Antenna Supporting Structures and Antennas
- Minimum Design Loads for Buildings and Other Structures ASCE/SEI 7-10
- AISC Manual of Steel Construction, 14th Edition ANSI/AISC 360-10

5.0 ANALYSIS

Design Loads:

- Ultimate wind speed: 115 mph
- Occupancy Category: II
- Exposure: B

Load Combinations:

- D
- D + L
- D + 0.6W
- 0.6D + 0.6W

6.0 CONCLUSIONS & RECOMMENDATIONS

The proposed appurtenances to are to be supported on the **proposed 2.5SCH40 x 11'-0" LG** mount pipes anchored to the penthouse walls. Refer to construction drawings prepared by **NB+C ES** for the proposed location of the appurtenances, and the supporting mounts.

Based on the performed analysis of this structure for applied gravity and lateral loads, the existing/proposed pipe mounts and anchorage are <u>adequate</u> to support the proposed T-Mobile appurtenances. The existing mount pipe was stressed to 6.40% of its capacity, the proposed mount pipe was stressed to 16.40% of its capacity, the existing wall mount angles were stressed to 23.60% of their capacity, and the existing anchorage was stressed to 41.0% of its capacity.

The proposed antenna installation represents an insignificant increase in gravity and lateral loads on the overall structure, therefore the installation is deemed acceptable by engineering judgement.

The conclusions reached by **NB+C ES** in this report are only applicable for the previously mentioned existing structural members supporting the T-Mobile equipment. Further, no structural qualification is made or implied by this report for existing structural members not supporting the T-Mobile equipment.

NB+C ENGINEERING SERVICES, LLC

Prepared by: Yaw O. Bonsu, E.I.T.

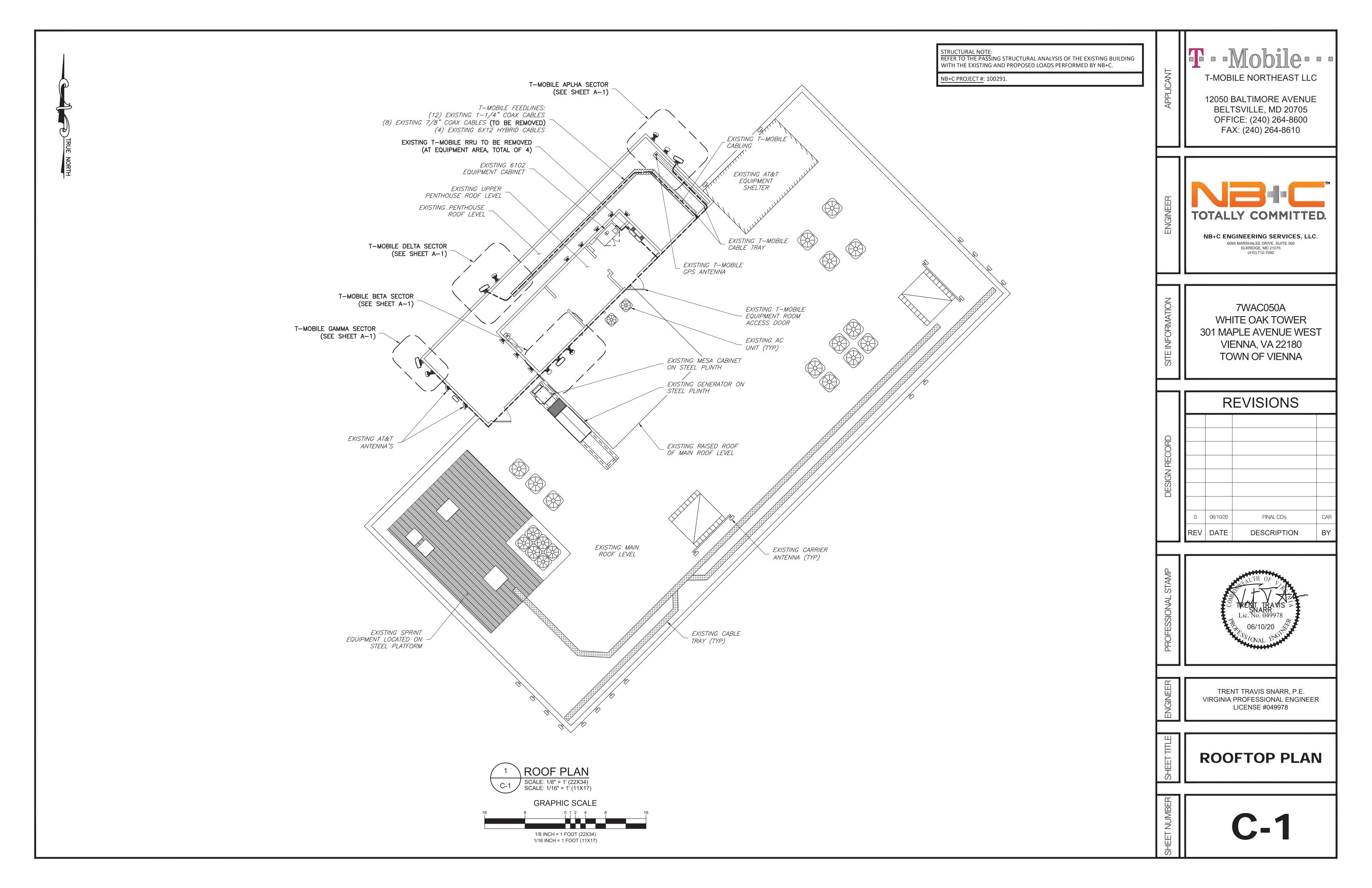
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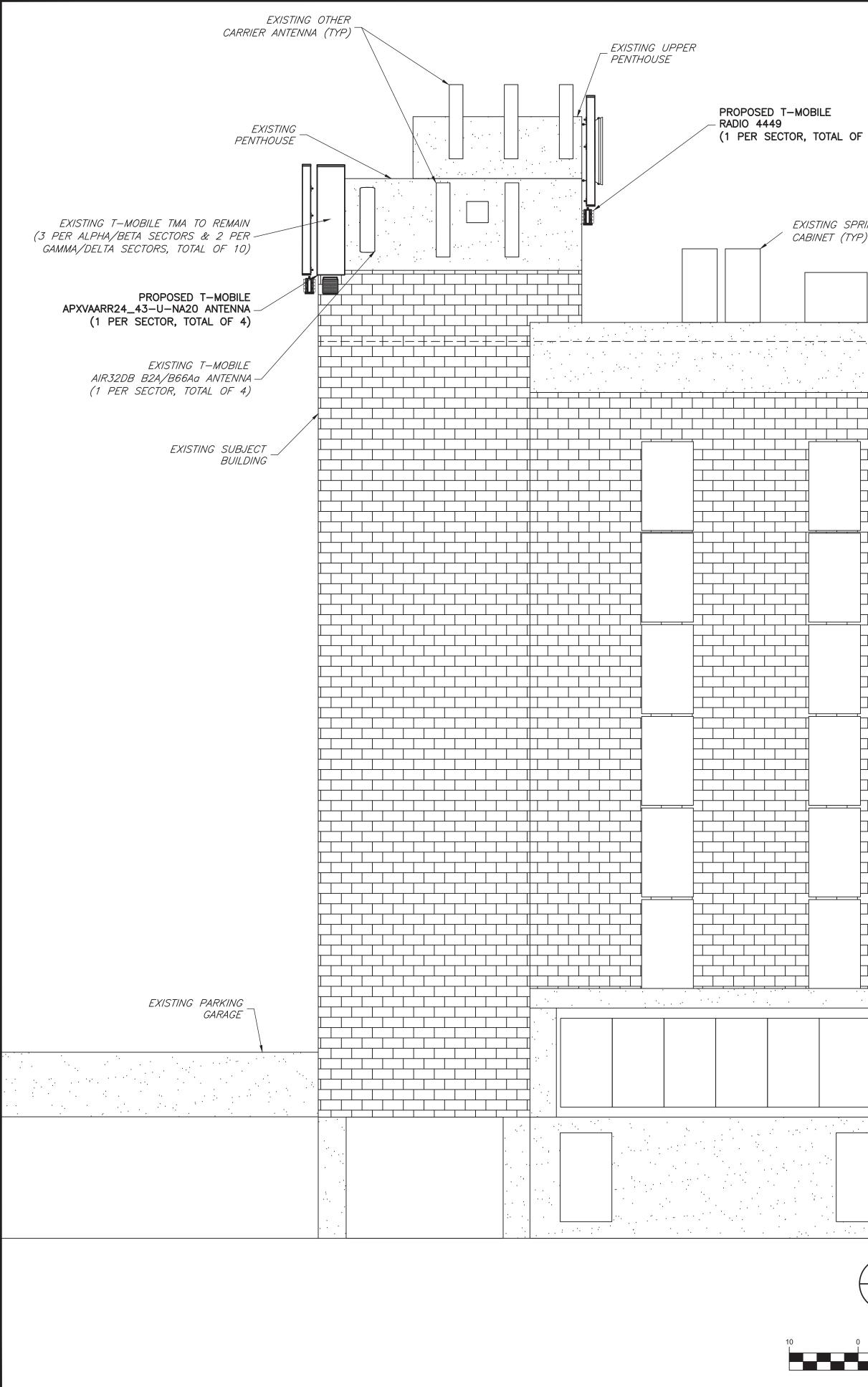
Krupakaran Kolandaivelu, P.E. Chief Engineer - Structural VA PE License # 49792



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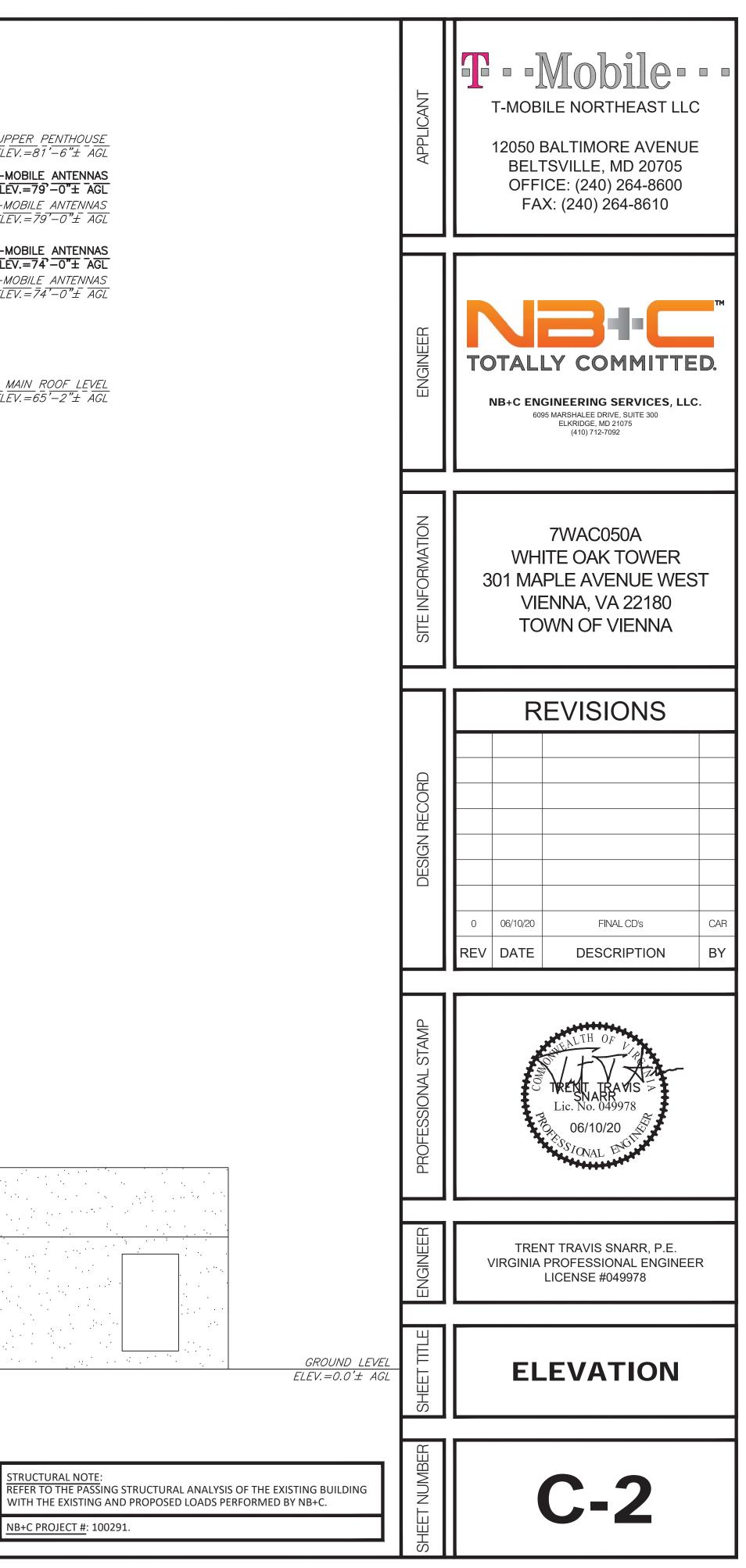
APPENDIX A: PLAN AND ELEVATION





MOBILE R, TOTAL OF 4)		TOP OF UPPER PENTHOUSE ELEV.=81'-6"± AGL PROPOSED T-MOBILE ANTENNAS (BETA) ELEV.=79'-0"± AGL EXISTING T-MOBILE ANTENNAS (BETA) ELEV.=79'-0"± AGL
XISTING SPRINT EQUIPMENT ABINET (TYP)		PROPOSED T-MOBILE ANTENNAS (ALPHA/GAMMA/DELTA) ELEV.=74'-0"± AGL EXISTING T-MOBILE ANTENNAS (ALPHA/GAMMA/DELTA) ELEV.=74'-0"± AGL
1 ELEVATIO C-2 SCALE: 1" = 10' (22X3) SCALE: 1" = 20' (11X1) GRAPHIC SCALE	N	

1 INCH = 10 FEET (22X34) 1 INCH = 20 FEET (11X17) NB+C PROJECT #: 100291.



APPENDIX B: CALCULATIONS Structural Analysis T-Mobile Site: 7WAC050A

ASCE/SEI 7-10 Reference

PURPOSE

The purpose of these calculations is to structurally qualify the existing/proposed antenna mounts for support of the proposed T-Mobile apurtenances.

Site Information:

<u>Site Number:</u> 7WAC050A <u>Address</u>: 301 Maple Avenue West, Vienna, VA22180

1) Antenna Mount Analysis:

Wind Loads:

Occupancy Category:	П	Table 1.5-1, pg. 2
Exposure:	Exp := "B"	Section 26.7.3, pg. 251
Topographic Factor:	$K_{zt} \coloneqq 1.0$	Section 26.8.2, pg. 254
Wind Directional Factor:	$K_{d} := 0.85$	Table 26.6-1, pg. 250
Gust Effect Factor:	<u> </u>	Section 26.9.1, pg. 254
Basic Wind Speed (mph):	<u>X</u> := 115	Figure 26.5-1 A-C, pgs. 247-249

Equipment Mid Height AGL (ft):	h ₁ := 79	
Velocity Pressure Coefficient:	z _g := 1200 if Exp = "B" = 1200 900 if Exp = "C" 700 if Exp = "D"	Table 26.9-1, pg. 256
	$\alpha := \begin{vmatrix} 7 & \text{if Exp} = "B" &= 7 \\ 9.5 & \text{if Exp} = "C" \\ 11.5 & \text{if Exp} = "D" \\ \frac{2}{\alpha} \end{vmatrix}$	
	$K_{z} := 2.01 \cdot \left(\frac{h_{1}}{z_{g}}\right)^{\alpha} = 0.924$	Table 29.3-1, pg. 310
Velocity Pressure (psf):	$q_{1z} := 0.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V^2 psf$	Equation 29.3-1, pg. 307
	$q_{1z} = 26.59 \cdot psf$	

Antenna Dimer	nsions:			
	<u>Antenna 1:</u> APXVAARR24 43	TMBXX 6516	<u>RRU 1:</u> 4449 B7	1+B85
Antenna Height	$\frac{h_{1}}{h_{1}} = 95.9 \text{ in}$	$h_{22} := 59.8 \text{ in}$	$h_5 := 14$	
Antenna Width	$w_1 := 24in$	$w_2 := 12.0in$	$w_5 := 13$	3.2in
Antenna Depth	$d_1 := 8.7 in$	$d_2 := 6.5 in$	$d_5 := 10$.4in
Antenna Weight	m _{ant1} := 128lbf	m _{ant2} := 34.6lbf	m _{rru1} :=	74lbf
Wind Area Front		$A_{2f} := h_2 \cdot w_2$	A _{5f} := h) - : W -
Wind Area Side	$\mathbf{A}_{1s} \coloneqq \mathbf{h}_1 \cdot \mathbf{d}_1$	$A_{2s} := h_2 \cdot d_2$	$A_{5s} := h$	5 5
Aspect Ratio	$Aspect_{1f} := \frac{h_1}{w_1} = 4$	Aspect _{2f} := $\frac{h_2}{w_2}$ =		
	$Aspect_{1s} := \frac{h_1}{d_1} = 11$	Aspect _{2s} := $\frac{h_2}{d_2}$ =	9.2 Aspect ₅₈	$a_{3} := \frac{h_{5}}{d_{5}} = 1.4$
Antenna Height	<u>RRU 2:</u> KRY 112 489/2			
Antenna Width	$h_6 := 11.0in$			
Antenna Depth	$w_6 := 6.1$ in			
Antenna Weight	$d_6 := 3.9 \text{in}$			
Wind Area Front	m _{rru2} := 15.4lbf			
Wind Area Side	$A_{6f} := h_6 \cdot w_6$			
	$A_{6s} := h_6 \cdot d_6$			
Aspect Ratio	$Aspect_{6f} := \frac{h_6}{w_6} = 1.8$			
	$Aspect_{6S} := \frac{h_6}{d_6} = 2.8$			
	$C_{f1f} = 1.35$ $C_{f2f} = 1.3^{\circ}$	7 $C_{cosc} = 1.37$	Cese = 1.3	F 00 F 4 040
Force Coeff front	$C_{f1s} = 1.53$ $C_{f2s} = 1.47$	101	101	Figure 29.5-1, pg. 312
Force Coeff side	115 128	138	158	
	$C_{f6f} = 1.31$			
	$C_{f6s} = 1.33$			

Wind Loads on Antennas:

Equation 29.5-1, pg. 308

Antenna 1:			
APXVAARR24_43	<u>Antenna 2:</u>	<u>RRU 1:</u> 4449 B71+B85	<u>RRU 2:</u> KRY 112 489/2
$W_{f1} := q_{1z} \cdot G \cdot C_{f1f} \cdot A_{1f}$	TMBXX 6516 A2M		
$W_{f1} = 487.6 \cdot lbf$	$W_{f2} := q_{1z} \cdot G \cdot C_{f2f} \cdot A_{2f}$	$W_{f5} \coloneqq q_{1z} \cdot G \cdot C_{f5f} \cdot A_{5f}$	$W_{f6} \coloneqq q_{1Z} \cdot G \cdot C_{f6f} \cdot A_{6f}$
11	$W_{f2} = 153.9 \cdot lbf$	$W_{f5} = 40.2 \cdot lbf$	$W_{f6} = 13.8 \cdot lbf$
$W_{s1} := q_{1z} \cdot G \cdot C_{f1s} \cdot A_{1s}$	12	$W_{s5} := q_{1z} \cdot G \cdot C_{f5s} \cdot A_{5s}$	$W_{s6} := q_{1z} \cdot G \cdot C_{f6s} \cdot A_{6s}$
$W_{s1} = 200.9 \cdot lbf$	$W_{s2} := q_{1z} \cdot G \cdot C_{f2s} \cdot A_{2s}$	$W_{s5} = 31.8 \cdot lbf$	
	$W_{s2} = 89.9 \cdot lbf$	$w_{s5} = 51.8.101$	$W_{s6} = 9 \cdot lbf$

Wind Loads Mount Members:

Equation 29.5-1, pg. 308

2.0" STD Pipe Member:

2.5" STD Pipe

Width: Force Coeff. Wind Load:

 $C_{fp2} := 1.2$

 $w_{p2} := 2.375 in$

 $w_{p25} := 2.875$ in $C_{fp25} := 1.2$ $\begin{array}{ll} F_{p2} \coloneqq q_{1z} \cdot G \cdot C_{fp2} \cdot w_{p2} & F_{p25} \coloneqq q_{1z} \cdot G \cdot C_{fp25} \cdot w_{p25} \\ \hline F_{p2} \equiv 5.4 \cdot \text{plf} & F_{p25} \equiv 6.5 \cdot \text{plf} \end{array}$

Antenna Mount Frame Analyzes:

Refer to attached RISA3D output.

Check Connections

The existing connections are composed of 1/2" threaded rods in Hilti HY-70 adhesive (3 1/8" embed.), assumed per site photos.

Hilti HY-70 Techinical Guide:

Spacing:	$s_b := 8in$
Max Tension Strength:	$N_n := 905lbf$
Max Shear Strength:	$V_n := 1685lbf$
Total Tension Strength:	$T := N_n = 0.91 \cdot kip$
Total Shear Strength:	$V_n = V_n = 1.69 \cdot kip$

Structural Analysis T-Mobile Site: 7WAC050A

Max Reactions From RISA 3D:

3 Envel	ope Joint Re	eactions						х
	Joint		X [k]	L	Y [k]	LC	Z [k]	L.
1	N9	max	.035	4	.48	3	.053	
2		min	035	2	367	9	072	
3	N7	max	.035	4	.48	3	.053	
4		min	035	2	367	9	072	
5	N10	max	.057	8	.484	5	.113	
6		min	057	6	364	7	095	
7	N8	max	.057	8	.484	5	.113	
8		min	057	6	364	7	095	
9	N17	max	.027	4	.095	3	.028	
10		min	027	2	049	9	035	
11	N18	max	.021	8	.095	5	.033	;
12		min	021	6	049	7	026	1
13	N19	max	.027	4	.095	3	.028	
14		min	027	2	049	9	035	ļ
15	N20	max	.021	8	.095	5	.033	;
16		min	021	6	049	7	026	

$$F_{V1} := 57lbf \qquad F_{V2} := 484lbf \qquad F_{T} := 113lbf \qquad F_{V} := \sqrt{F_{V1}^{2} + F_{V2}^{2}} = 487.3 \cdot lbf$$

Interaction := $\left(\frac{F_{T}}{T}\right) + \left(\frac{F_{V}}{V}\right) = 0.41$ <1.0; Thus OK

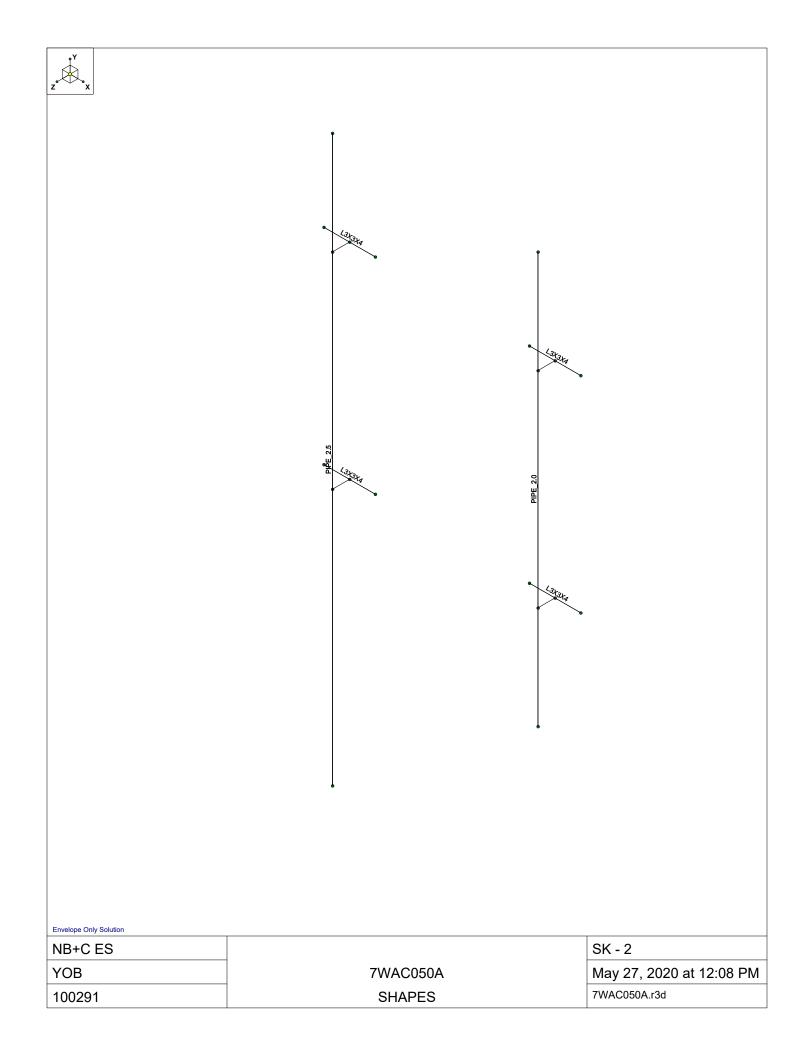
Hence the existing connections are adequate.

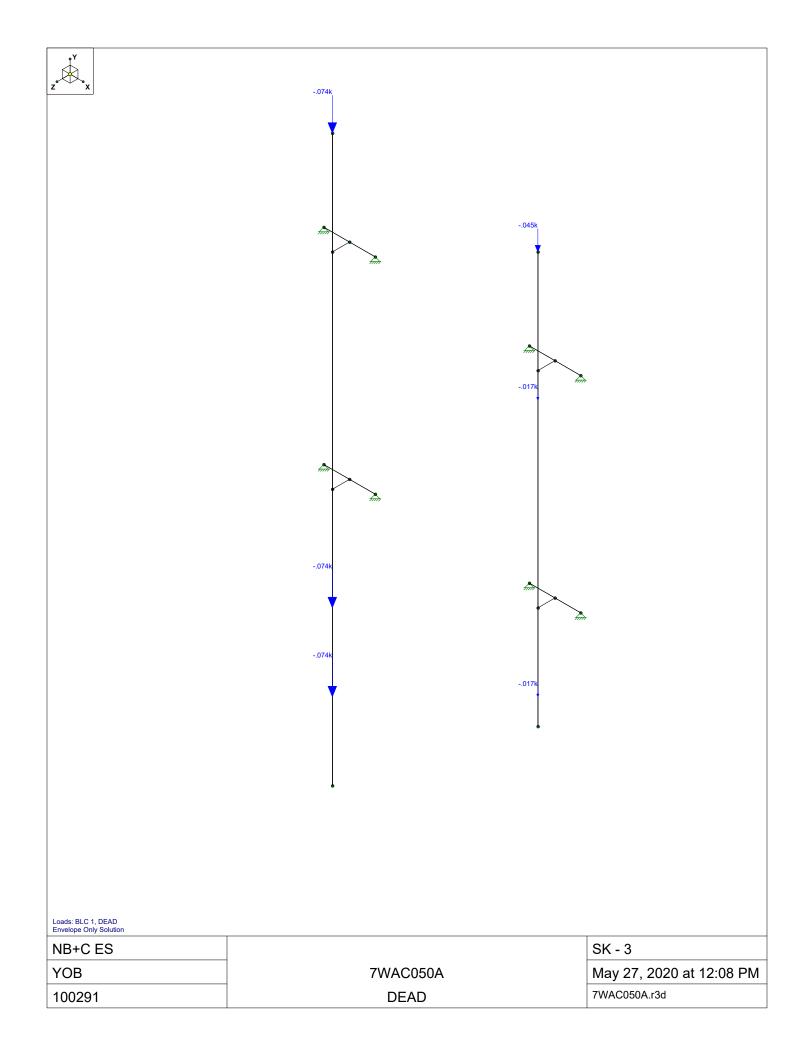
Adhesive Anchoring Systems

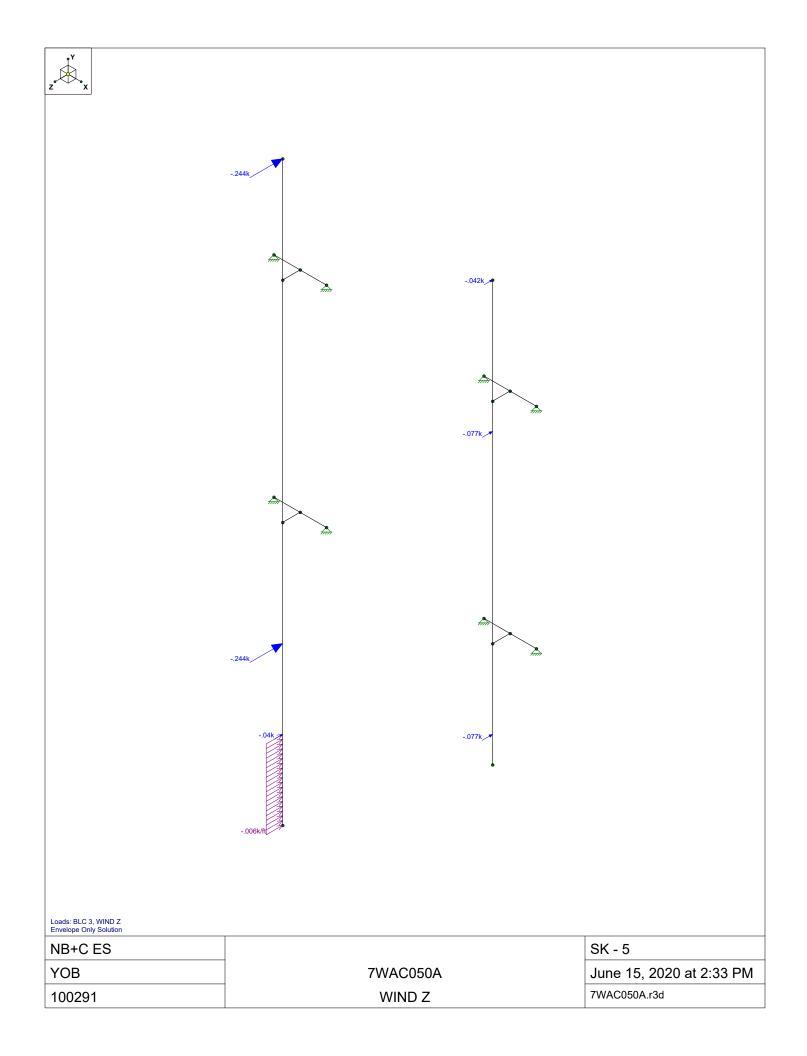
3.2.6 HIT-HY 70 Hybrid for Masonry Construction

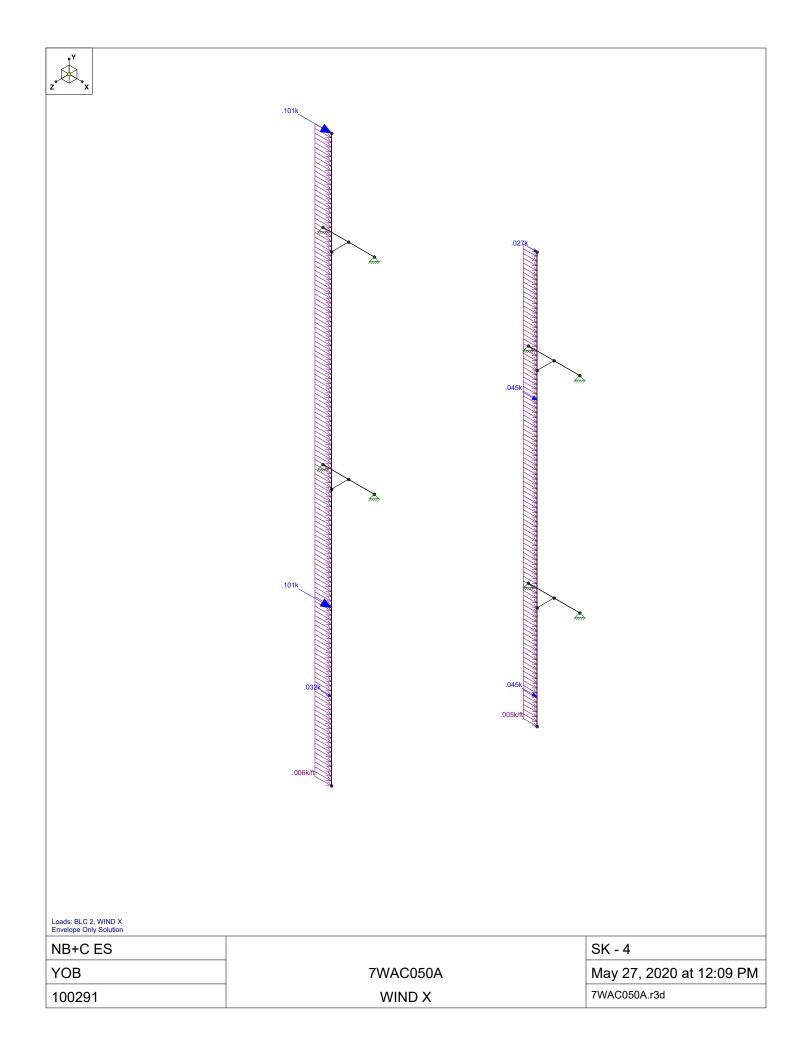
Table 10 - H	ble 10 - HIT-HY 70 allowable adhesive bond loads for threaded rods in the face of hollow brick ^{1,2,3,4,5,10}													
Nominal	Effective embedment				Minimu	um edge	Load				Edge distance ⁶			
anchor			Ten	sion	distance c _{min}		reduction	Shear		Critical c _{er}		Minimum c _{min}		Load reduction
diameter	in.	(mm)6	lb	(kN) ^{7,8}	in.	(mm) ⁹	factor @ c _{min}	lb	(kN) ^{7,8}	in.	(mm)	in.	(mm)	factor @ c _{min}
1/4			530	(2.4)	.4)	. (22.2)	1.00	370	(1.6)	12			(222)	1.00
5/16	0.1/0	(70)	735	(3.3)				595	(2.6)		(004.0)			1.00
3/8	3-1/8 (79)	(79)	905	(4.0)	8	(203)		1,045	(4.7)		(304.8) 8	8	(203)	0.76
1/2		905	(4.0)				1,685	(7.5)					0.52	

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A Ya VYf 8 jghf jVi hYX @ UXg f6 @ '' . K = B8 NL

	T^{à^¦∕Šæà^∣	Öãi^&cãji}	Ùcæ¦cÁTæ*}ãĉå^ŽĐe∰∰	EÒ}åÁTæt}ãčå^ŽĐo£2ÈÈÈ	ÈÙcæboÆG[&æetā]}ŽeÉÃá	Ò}åÆŠ[&æstā[}ŽdÊÃá
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	Ö^∙&¦ājcāj}	Ù[È	ŬËÈÙ	JÈÈÓŠÔ	Øæ&À	ĨĎŠÔ <i>Øæ</i> &Ĥ	ĐŠĈ)Øæ&⊞	ĎŠÔ	Zæ&∰	ĎŠÔ	Øæ&ÈÈ	ĎŠÔ	Øæ&ÈÈ	ĎŠÔ	Øæ&Ĥ	ĐŠÔ	Øæ&È	ĐŠÔ	Øæ&È	ĐŠÔ	Øæ&
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G	OEÙÔÒÁOEÙÖÄ ÁÇæDÁÇæD	Ϋ́^•	Ϋ́	ÖŠ	F	YËËË																
Н	OEÙÔÒÁOEÙÖÄ Á ŒĐÁA D			ÖŠ	F	ΥЩÊ																
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Î	CEÙÔÒÁCEÙÖÁÏÁÇæD	Ϋ́^•	Ϋ́	ÖŠ	Ê	YËËË																
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Ì		Ϋ́^•	Ϋ́	ÖŠ	Ê	ΥЩÊ																
J	OEÙÔÒÁOEÙÖÁÏÁÇãD	Ϋ́^•	Ϋ́	ÖŠ	Ê	ΥЩ̈́																



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	RĮą̃ic		ÝÄŽá	ŠÔ	ŸÁŽÍá	ŠÔ	ZÄÄXá	ŠÔ	ΤÝÂŽËcá	ŠÔ	ΤΫÁŽËcá	ŠÔ	TZÁŽËcá	ŠÔ
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Н	ΤF	ÚQÚÒ´GĚ́	ÈÎI	IÈG	Í	Ì€FÏ	HÈ€JI		J	FŒĬ€Ì	HHËIH	GÊUH	GÉUH	F PFËrà
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301 Maple Ave W

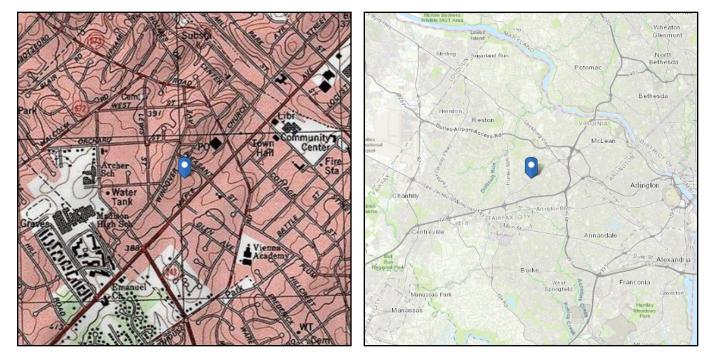
Vienna, Virginia

22180

ASCE 7 Hazards Report

Standard:ASCE/SEI 7-10Risk Category:IISoil Class:D - Stiff Soil

Elevation: 412.42 ft (NAVD 88) Latitude: 38.89827 Longitude: -77.270958



Wind

Results:

Wind Speed:	115 Vmph
10-year MRI	76 Vmph
25-year MRI	84 Vmph
50-year MRI	90 Vmph
100-year MRI	96 Vmph
Data Source:	ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1–CC-4, incorporating errata of March 12, 2014
Date Accessed:	Wed May 27 2020

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is not in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.



Poculte:

0.75 in.
15 F
30 mph
Standard ASCE/SEI 7-10, Figs. 10-2 through
Wed May 27 2020

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

10-8

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

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