NB+C Engineering Services
Rooftop Structural Analysis
Prepared for T-Mobile: L700 4x2 Installation

## SITE INFORMATION

| Address | 301 Maple Ave West |
| :--- | :--- |
|  | Vienna, VA 22180 |
|  | Lat: $38.897942^{\circ}$ |
|  | Long: -77.270294 |
| T-Mobile Site Number | 7WAC050A |
| T-Mobile Site Name | White Oak Tower |
| NB+C Project Number | 100291 |
| Date | June 15, 2020 |

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### 1.0 INTRODUCTION

The existing structure is a $81^{\prime}-6{ }^{\prime \prime}$ tall building located in Vienna, VA.
T-Mobile has proposed to reconfigure the site and install new antennas as shown in the table below. A structural analysis was performed to see if the new loads are safely supported by the roof structure and to verify if the existing structure is in compliance with the applicable codes and standards. Information we have received and used for this analysis includes:

- RFDS provided by T-Mobile dated May 01, 2020
- Site Audit Photos dated September 04, 2019
- Construction Drawings by NB+C Engineering Services, dated June 10, 2020


### 2.0 APPURTENANCES LOADING

As per the information provided to us, the following tables show the final and existing antenna and equipment installation by T-Mobile.

Table 1 - Proposed/Final Antenna and Cable Information

| Mounting Level (ft) | Center Line Elevation (ft) | $\left\|\begin{array}{c} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array}\right\|$ | Antenna Manufacturer | Antenna Model | Carrier | Feed Line Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 74^{\prime}-0 "{ }^{\prime \prime} \\ & 79^{\prime}-0^{\prime \prime} \end{aligned}$ | $\begin{aligned} & 74^{\prime}-0 " \prime \\ & 79^{\prime}-0^{\prime \prime} \end{aligned}$ | 4 | RFS | APXVAAR24 43-U-NA20 (95.9"x24.0"x8.7", 128.01bs) | T-Mobile | (4) $6 \times 12$ Hybrid <br> (6) 1-1/4" Coax | - |
|  |  | 4 | Ericsson | Radio 4449 B71 + B85 (13.4"x16.5"x5.9", 46.0lbs) |  |  |  |
|  |  | 2 | Ericsson | KRY 112 489/2 $\left(11.0 " \times 6.1 " \times 3.9^{\prime \prime}, 15.4 \mathrm{lbs}\right)$ |  |  |  |

Table 2 - Existing Antenna and Cable Information

| Mounting <br> Level (ft) | Center <br> Line <br> Elevation <br> $(\mathrm{ft})$ | Number of Antennas | Antenna Manufacturer | Antenna Model | Carrier | $\begin{array}{\|l\|l} \text { Feed Line } \\ \text { Size (in) } \end{array}$ | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 74^{\prime}-0 " \\ & 79^{\prime}-0 " \end{aligned}$ | $\begin{aligned} & 74^{\prime}-0 "{ }^{\prime \prime} \\ & 79^{\prime}-0 \end{aligned}$ | 4 | Ericsson | AIR32DB B66A/B2A | T-Mobile | (4) $6 \times 12$ <br> Hybrid ${ }^{1}$ <br> (6) $1-1 / 4$ " <br> Coax ${ }^{1}$ <br> (4) $7 / 8$ " <br> Coax ${ }^{2}$ | 1 |
|  |  | 2 | Andrew | TMBXX-6516-A2M |  |  |  |
|  |  | 2 | Commscope | SBNHH-1D65C |  |  | 2 |
|  |  | 4 | Ericsson | KRY 112 489/2 |  |  |  |
|  |  | 2 | - | Twin Style 1B |  |  | 1 |

Note:

1. Existing equipment to remain.
2. Existing equipment to be removed, was not considered in this analysis.

### 3.0 ASSUMPTIONS

This report is based on the theoretical capacity of the existing structural elements and is not an assessment of the overall suitability of the existing Structure or its components for any particular use other than specified here in this report:

- This report makes no warranties, expressed and/or implied, and disclaims any liability arising from material, fabrication and erection of the existing Structure and any other existing or proposed components or appurtenances.
- All proposed and existing antennas, mounts, coaxial cables and appurtenances are assumed to be properly installed and configured according to manufacturer requirements.
- All existing structural elements are assumed to be in place and in good condition, and were previously designed and constructed in accordance with applicable codes and standards.
- Existing anchorage to penthouse wall assumed to be $1 / 2$ " diameter threaded rods with Hilti HY70 adhesive and $31 / 8^{\prime \prime} \mathrm{min}$. embedment.
- Contractor to verify existing site condition including the existing structure prior to fabrication and construction. In the event the existing structure conditions are different than the assumptions made in this report, this has to be brought to the structural engineer's attention before proceeding any further with bidding, fabrication and/or erection.


### 4.0 APPLICABLE CODES AND STANDARDS

The existing structure was analyzed/designed per the provisions of following applicable codes and standards:

- 2015 Virginia Construction Code
- ANSI/TIA-222-G - Structural Standards for Antenna Supporting Structures and Antennas
- Minimum Design Loads for Buildings and Other Structures ASCE/SEI 7-10
- AISC Manual of Steel Construction, $14^{\text {th }}$ Edition - ANSI/AISC 360-10


### 5.0 ANALYSIS

## Design Loads:

- Ultimate wind speed: 115 mph
- Occupancy Category: II
- Exposure: B


## Load Combinations:

-D

- D + L
- $D+0.6 W$
- 0.6D + 0.6W


### 6.0 CONCLUSIONS \& RECOMMENDATIONS

The proposed appurtenances to are to be supported on the proposed $2.5 \mathrm{SCH} 40 \times 11^{\prime}-\mathbf{0}^{\prime \prime}$ LG mount pipes anchored to the penthouse walls. Refer to construction drawings prepared by NB+C ES for the proposed location of the appurtenances, and the supporting mounts.

Based on the performed analysis of this structure for applied gravity and lateral loads, the existing/proposed pipe mounts and anchorage are adequate to support the proposed T-Mobile appurtenances. The existing mount pipe was stressed to $6.40 \%$ of its capacity, the proposed mount pipe was stressed to $16.40 \%$ of its capacity, the existing wall mount angles were stressed to $23.60 \%$ of their capacity, and the existing anchorage was stressed to $41.0 \%$ of its capacity.

The proposed antenna installation represents an insignificant increase in gravity and lateral loads on the overall structure, therefore the installation is deemed acceptable by engineering judgement.

The conclusions reached by NB+C ES in this report are only applicable for the previously mentioned existing structural members supporting the T-Mobile equipment. Further, no structural qualification is made or implied by this report for existing structural members not supporting the T-Mobile equipment.

NB+C ENGINEERING SERVICES, LLC
Prepared by: Yaw O. Bonsu, E.I.T.
Respectfully Submitted by:
Krupakaran Kolandaivelu, P.E.
Chief Engineer - Structural
VA PE License \# 49792


APPENDIX A:
PLAN AND ELEVATION



## APPENDIX B: CALCULATIONS

| NB+C ES | Structural Analysis | 1 |
| :--- | :---: | ---: |
| 6095 Marshalee Drive | T-Mobile Site: | $5 / 27 / 2020$ |
| Suite 300 | 7WAC050A | NB+C ES No: 100291 |
| Elkridge, MD 21075 |  |  |

## PURPOSE

The purpose of these calculations is to structurally qualify the existing/proposed antenna mounts for support of the proposed T-Mobile apurtenances.

## Site Information:

Site Number: 7WAC050A
Address: 301 Maple Avenue West, Vienna, VA 22180

## 1) Antenna Mount Analysis:

## Wind Loads:

Occupancy Category: II

| Exposure: | Exp $:=" B "$ |
| :--- | :--- |
| Topographic Factor: | $\mathrm{K}_{\mathrm{zt}}:=1.0$ |
| Wind Directional Factor: | $\mathrm{K}_{\mathrm{d}}:=0.85$ |
| Gust Effect Factor: | $\mathrm{Gu}:=0.85$ |
| Basic Wind Speed (mph): | $\underset{\mathrm{Wi}}{\mathrm{V}}:=115$ |

## ASCE/SEI 7-10 Reference

Table 1.5-1, pg. 2

Section 26.7.3, pg. 251

Section 26.8.2, pg. 254

Table 26.6-1, pg. 250

Section 26.9.1, pg. 254
Figure 26.5-1 A-C, pgs. 247-249

Equipment Mid HeightAGL (ft): $\quad \mathrm{h}_{1}:=79$
Velocity Pressure Coefficient:
$\mathrm{z}_{\mathrm{g}}:=\left\lvert\, \begin{aligned} & 1200 \text { if } \operatorname{Exp}=" \mathrm{~B} "=1200 \\ & 900 \text { if } \operatorname{Exp}=" \mathrm{C} " \\ & 700 \text { if } \operatorname{Exp}=" \mathrm{D} "\end{aligned} \quad\right.$ Table 26.9-1, pg. 256

$$
\alpha:=\left\lvert\, \begin{aligned}
& 7 \text { if } \operatorname{Exp}=" \mathrm{~B} " \quad=7 \\
& 9.5 \text { if } \operatorname{Exp}=" \mathrm{C} " \\
& 11.5 \text { if } \operatorname{Exp}=" \mathrm{D} "
\end{aligned}\right.
$$

$\mathrm{K}_{\mathrm{z}}:=2.01 \cdot\left(\frac{\mathrm{~h}_{1}}{\mathrm{z}_{\mathrm{g}}}\right)^{\frac{2}{\alpha}}=0.924$

Velocity Pressure (psf):
$\mathrm{q}_{1 \mathrm{z}}:=0.00256 \cdot \mathrm{~K}_{\mathrm{z}} \cdot \mathrm{K}_{\mathrm{zt}} \cdot \mathrm{K}_{\mathrm{d}} \cdot \mathrm{V}^{2}{ }^{\mathrm{psf}}$
$\mathrm{q}_{1 \mathrm{z}}=26.59 \cdot \mathrm{psf}$

Table 29.3-1, pg. 310

Equation 29.3-1, pg. 307

## Antenna Dimensions:

|  | Antenna 1: <br> APXVAARR24_43 | TMBXX 6516 | $\frac{\text { RRU 1: }}{4449 \text { B71+B85 }}$ |
| :---: | :---: | :---: | :---: |
| Antenna Height | $\mathrm{h}_{\text {mu }}:=95.9 \mathrm{in}$ | $\mathrm{h}_{2 \times 2}:=59.8 \mathrm{in}$ | $\mathrm{h}_{5}:=14.9 \mathrm{in}$ |
| Antenna Width | $\mathrm{w}_{1}:=24 \mathrm{in}$ | $\mathrm{w}_{2}:=12.0 \mathrm{in}$ | $\mathrm{w}_{5}:=13.2 \mathrm{in}$ |
| Antenna Depth | $\mathrm{d}_{1}:=8.7 \mathrm{in}$ | $\mathrm{d}_{2}:=6.5 \mathrm{in}$ | $\mathrm{d}_{5}:=10.4 \mathrm{in}$ |
| Antenna Weight | $\mathrm{m}_{\text {ant1 }}:=128 \mathrm{lbf}$ | $\mathrm{mant} 2:=34.6 \mathrm{lbf}$ | $\mathrm{m}_{\text {rru1 }}:=741 \mathrm{bf}$ |
| Wind Area Front | $\mathrm{A}_{1 \mathrm{f}}:=\mathrm{h}_{1} \cdot \mathrm{w}_{1}$ | $\mathrm{A}_{2 \mathrm{f}} \mathrm{:}=\mathrm{h}_{2} \cdot \mathrm{w}_{2}$ | $\mathrm{A}_{5 \mathrm{f}}:=\mathrm{h}_{5} \cdot \mathrm{w}_{5}$ |
| Wind Area Side | $\mathrm{A}_{1 \mathrm{~s}}:=\mathrm{h}_{1} \cdot \mathrm{~d}_{1}$ | $\mathrm{A}_{2 \mathrm{~s}} \mathrm{l}=\mathrm{h}_{2} \cdot \mathrm{~d}_{2}$ | $\mathrm{A}_{5 \mathrm{~s}}:=\mathrm{h}_{5} \cdot \mathrm{~d}_{5}$ |
| Aspect Ratio | $\text { Aspect }_{1 \mathrm{f}}:=\frac{\mathrm{h}_{1}}{\mathrm{w}_{1}}=4$ | $\text { Aspect }_{2 \mathrm{f}}:=\frac{\mathrm{h}_{2}}{\mathrm{w}_{2}}=5$ | $\text { Aspect }_{5 \mathrm{f}}:=\frac{\mathrm{h}_{5}}{\mathrm{w}_{5}}=1.1$ |
|  | $\text { Aspect }_{1 \mathrm{~s}}:=\frac{\mathrm{h}_{1}}{\mathrm{~d}_{1}}=11$ | $\text { Aspect }_{2 \mathrm{~s}}:=\frac{\mathrm{h}_{2}}{\mathrm{~d}_{2}}=9.2$ | $\text { Aspect }_{5 \mathrm{~s}}:=\frac{\mathrm{h}_{5}}{\mathrm{~d}_{5}}=1.4$ |
| Antenna Height | $\frac{R R U \text { 2: }}{\text { KRY } 112}$ |  |  |
| Antenna Width | $\mathrm{h}_{6}:=11.0 \mathrm{in}$ |  |  |
| Antenna Depth | $\mathrm{w}_{6}$ : $=6.1 \mathrm{in}$ |  |  |
| Antenna Weight | $\mathrm{d}_{6}:=3.9 \mathrm{in}$ |  |  |
| Wind Area Front | $\mathrm{m}_{\text {rru2 }}:=15.4 \mathrm{lbf}$ |  |  |
| Wind Area Side | $\mathrm{A}_{6 \mathrm{f}}:=\mathrm{h}_{6} \cdot \mathrm{w}_{6}$ |  |  |
|  | $\mathrm{A}_{6 \mathrm{~s}}:=\mathrm{h}_{6} \cdot \mathrm{~d}_{6}$ |  |  |
| Aspect Ratio | $\text { Aspect }_{6 \mathrm{f}}:=\frac{\mathrm{h}_{6}}{\mathrm{w}_{6}}=1.8$ |  |  |
|  | $\text { Aspect }_{6 \mathrm{~s}}:=\frac{\mathrm{h}_{6}}{\mathrm{~d}_{6}}=2.8$ |  |  |

${ }^{\square}$ Force Coeff front
$\mathrm{C}_{\mathrm{flf}}=1.35 \quad \mathrm{C}_{\mathrm{f} 2 \mathrm{f}}=1.37 \quad \mathrm{C}_{\mathrm{f} 3 \mathrm{f}}=1.37 \quad \mathrm{C}_{\mathrm{f} 5 \mathrm{f}}=1.3$
$\mathrm{C}_{\mathrm{f} 1 \mathrm{~s}}=1.53 \quad \mathrm{C}_{\mathrm{f} 2 \mathrm{~s}}=1.47 \quad \mathrm{C}_{\mathrm{f} 3 \mathrm{~s}}=1.47 \quad \mathrm{C}_{\mathrm{f} 5 \mathrm{~s}}=1.31$

$$
\begin{aligned}
& \mathrm{C}_{\mathrm{f} 6 \mathrm{f}}=1.31 \\
& \mathrm{C}_{\mathrm{f} 6 \mathrm{~s}}=1.33
\end{aligned}
$$

## Wind Loads on Antennas:

Antenna 1:

| APXVAARR24_43 | $\frac{\text { Antenna 2: }}{\text { TMBXX 6516 A2M }}$ |
| :--- | :--- |
| $\mathrm{W}_{\mathrm{f} 1}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{f} 1 \mathrm{f}} \cdot \mathrm{A}_{1 \mathrm{f}}$ | $\mathrm{W}_{\mathrm{f} 2}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{f} 2 \mathrm{f}} \cdot \mathrm{A}_{2 \mathrm{f}}$ |
| $\mathrm{W}_{\mathrm{f} 1}=487.6 \cdot \mathrm{lbf}$ |  |
| $\mathrm{W}_{\mathrm{s} 1}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{f} 1 \mathrm{~s}} \cdot \mathrm{~A}_{1 \mathrm{~s}}$ | $\mathrm{~W}_{\mathrm{f} 2}=153.9 \cdot \mathrm{lbf}$ |
| $\mathrm{W}_{\mathrm{s} 1}=200.9 \cdot \mathrm{lbf}$ | $\mathrm{W}_{\mathrm{s} 2}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{f} 2 \mathrm{~s}} \cdot \mathrm{~A}_{2 \mathrm{~s}}$ |
|  |  |
|  | $\mathrm{~W}_{\mathrm{s} 2=89.9 \cdot \mathrm{lbf}}$ |

RRU 1:
4449 B71+B85
$\mathrm{W}_{\mathrm{f} 5}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{f} 5 \mathrm{f}} \cdot \mathrm{A}_{5 \mathrm{f}}$
$\mathrm{W}_{\mathrm{f} 5}=40.2 \cdot \mathrm{lbf}$
$\mathrm{W}_{\mathrm{s} 5}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{f} 5 \mathrm{~s}} \cdot \mathrm{~A}_{5 \mathrm{~s}}$
$\mathrm{W}_{\mathrm{s} 5}=31.8 \cdot \mathrm{lbf}$

Equation 29.5-1, pg. 308
RRU 2:
KRY 112 489/2
$\mathrm{W}_{\mathrm{f} 6}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{f} 6 \mathrm{f}} \cdot \mathrm{A}_{6 \mathrm{f}}$
$\mathrm{W}_{\mathrm{f} 6}=13.8 \cdot \mathrm{lbf}$
$\mathrm{W}_{\mathrm{s} 6}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{f} 6 \mathrm{~s}} \cdot \mathrm{~A}_{6 \mathrm{~s}}$
$\mathrm{W}_{\mathrm{s} 6}=9 \cdot \mathrm{lbf}$

Wind Loads Mount Members:
Equation 29.5-1, pg. 308

| Member: | 2.0" STD Pipe | 2.5 " STD Pipe |
| :--- | :--- | :--- |
| Width: | $\mathrm{w}_{\mathrm{p} 2}:=2.375$ in | $\mathrm{w}_{\mathrm{p} 25}:=2.875$ in |
| Force Coeff. | $\mathrm{C}_{\mathrm{fp} 2}:=1.2$ | $\mathrm{C}_{\mathrm{fp} 25}:=1.2$ |
| Wind Load: | $\mathrm{F}_{\mathrm{p} 2}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{fp} 2} \cdot \mathrm{w}_{\mathrm{p} 2}$ | $\mathrm{~F}_{\mathrm{p} 25}:=\mathrm{q}_{1 \mathrm{z}} \cdot \mathrm{G} \cdot \mathrm{C}_{\mathrm{fp} 25} \cdot \mathrm{~W}_{\mathrm{p} 25}$ |
|  | $\mathrm{~F}_{\mathrm{p} 2}=5.4 \cdot \mathrm{plf}$ | $\mathrm{F}_{\mathrm{p} 25}=6.5 \cdot \mathrm{plf}$ |

## Antenna Mount Frame Analyzes:

Refer to attached RISA 3D output.

## Check Connections

The existing connections are composed of 1/2" threaded rods in Hilti HY-70 adhesive (3 1/8" embed.), assumed per site photos.

Hilti HY-70 Techinical Guide:

| Spacing: | $\mathrm{s}_{\mathrm{b}}:=8 \mathrm{in}$ |
| :--- | :--- |
| Max Tension Strength: | $\mathrm{N}_{\mathrm{n}}:=905 \mathrm{lbf}$ |
| Max Shear Strength: | $\mathrm{V}_{\mathrm{n}}:=1685 \mathrm{lbf}$ |
| Total Tension Strength: | $\mathrm{T}:=\mathrm{N}_{\mathrm{n}}=0.91 \cdot \mathrm{kip}$ |
| Total Shear Strength: | $\mathrm{V}:=\mathrm{V}_{\mathrm{n}}=1.69 \cdot \mathrm{kip}$ |


| NB+C ES | Structural Analysis | 4 |
| :--- | :---: | ---: |
| 6095 Marshalee Drive | T-Mobile Site: | $5 / 27 / 2020$ |
| Suite 300 | 7WAC050A | NB+C ES No: 100291 |
| Elkridge, MD 21075 |  |  |

## Max Reactions From RISA 3D:

| (30) Envelope Joint Reactions |  |  |  |  |  |  | $\square \square$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \square$ | Joint |  | X [k] | L. | $\mathrm{Y}[\mathrm{k}]$ | LC | Z [k] | L... |
| 1 | N9 | max | . 035 | 4 | 48 | 3 | . 053 | * |
| 2 |  | min | -. 035 | 2 | -. 367 | 9 | -. 072 | ! |
| 3 | N7 | max | . 035 | 4 | 48 | 3 | . 053 |  |
| 4 |  | min | -. 035 | 2 | -. 367 | 9 | -. 072 | $!$ |
| 5 | N10 | max | . 057 | 8 | . 484 | 5 | . 113 |  |
| 6 |  | min | -. 057 | 6 | -. 364 | 7 | -. 095 | ! |
| 7 | N8 | max | . 057 | 8 | . 484 | 5 | . 113 | . |
| 8 |  | min | -. 057 | 6 | -. 364 | 7 | -. 095 | ! |
| 9 | N17 | max | . 027 | 4 | . 095 | 3 | . 028 |  |
| 10 |  | min | -. 027 | 2 | -. 049 | 9 | -. 035 | ! |
| 11 | N18 | max | . 021 | 8 | . 095 | 5 | . 033 |  |
| 12 |  | min | -. 021 | 6 | -. 049 | 7 | -. 026 | $!$ |
| 13 | N19 | max | . 027 | 4 | . 095 | 3 | . 028 |  |
| 14 |  | min | -. 027 | 2 | -. 049 | 9 | -. 035 | - |
| 15 | N20 | max | . 021 | 8 | . 095 | 5 | . 033 |  |
| 16 |  | min | -. 021 | 6 | -. 049 | 7 | -. 026 | !- |

$$
\begin{aligned}
& \mathrm{F}_{\mathrm{V} 1}:=57 \mathrm{lbf} \quad \mathrm{~F}_{\mathrm{V} 2}:=484 \mathrm{lbf} \quad \mathrm{~F}_{\mathrm{T}}:=113 \mathrm{lbf} \quad \mathrm{~F}_{\mathrm{V}}:=\sqrt{\mathrm{F}_{\mathrm{V} 1}^{2}+\mathrm{F}_{\mathrm{V} 2}^{2}}=487.3 \cdot \mathrm{lbf} \\
& \text { Interaction }:=\left(\frac{\mathrm{F}_{\mathrm{T}}}{\mathrm{~T}}\right)+\left(\frac{\mathrm{F}_{\mathrm{V}}}{\mathrm{~V}}\right)=0.41 \quad<1.0 ; \text { Thus OK }
\end{aligned}
$$

Hence the existing connections are adequate.

## Adhesive Anchoring Systems

3.2.6 HIT-HY 70 Hybrid for Masonry Construction

Table 10-HIT-HY 70 allowable adhesive bond loads for threaded rods in the face of hollow brick 1, , , , 4, 5, 10

| Nominal | Effective embedment in. $(\mathrm{mm})^{6}$ | $\begin{aligned} & \text { Tension } \\ & \text { lb } \quad(\mathrm{kN})^{7,8} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Minimum edge } \\ & \text { distance } \mathrm{c}_{\mathrm{mn}} \\ & \text { in. } \quad(\mathrm{mm})^{9} \end{aligned}$ | Load reduction factor @ $\mathrm{C}_{\text {min }}$ | Shear | Edge distance ${ }^{6}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| anchor <br> diameter |  |  |  |  |  | Critical $\mathrm{c}_{\mathrm{a}}$ in. (mm) | Minimum $\mathrm{C}_{\text {min }}$ in. (mm) | Load reduction factor @ $\mathrm{C}_{\text {min }}$ |
| 1/4 | 3-1/8 (79) | 530 (2.4) | 8 (203) | 1.00 | 370 (1.6) | 12 (304.8) | 8 (203) | 1.00 |
| 5/16 |  | 735 (3.3) |  |  | 595 (2.6) |  |  | 1.00 |
| 3/8 |  | 905 (4.0) |  |  | 1,045 (4.7) |  |  | 0.76 |
| 1/2 |  | 905 (4.0) |  |  | 1,685 (7.5) |  |  | 0.52 |



| $N B+C$ ES |  | SK -1 |
| :--- | :---: | :--- |
| YOB | 7WAC050A | May 27, 2020 at 12:07 PM |
| 100291 | RENDERING | 7WAC050A.r3d |



Envelope Only Solution

| $N B+C$ ES |  | SK -2 |
| :--- | :---: | :--- |
| YOB |  | MWAC050A |
|  | SHAPES | May 27, 2020 at $12: 08$ PM |



Loads: BLC 1, DEAD Envelope Only Solution

| $N B+C$ ES |  | SK -3 |
| :--- | :---: | :--- |
| YOB |  | MWAC050A |
|  | DEAD | May 27, 2020 at $12: 08$ PM |
| 100291 | 7WAC050A.r3d |  |



| $N B+C$ ES |  | SK -5 |
| :--- | :---: | :--- |
| YOB |  | 7WAC050A |
|  | WIND $Z$ | June 15,2020 at 2:33 PM |
| 100291 | 7WAC050A.r3d |  |



Loads: BLC 2, WIND X
Envelope Only Solution

| NB+C ES | 7WAC050A WIND X | SK-4 |
| :---: | :---: | :---: |
| YOB |  | May 27, 2020 at 12:09 PM |
| 100291 |  | 7WAC050A.r3d |



$\qquad$

Hot Rolled Steel Properties

|  | Label | E [ksi] | G [ksi] | Nu | Therm (/1E. | Density[k/ft... | Yield[ksi] | Ry | Fu[ksi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A992 | 29000 | 11154 | . 3 | . 65 | . 49 | 50 | 1.1 | 65 | 1.1 |
| 2 | A36 Gr. 36 | 29000 | 11154 | . 3 | . 65 | . 49 | 36 | 1.5 | 58 | 1.2 |
| 3 | A572 Gr. 50 | 29000 | 11154 | . 3 | . 65 | . 49 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr.B RND | 29000 | 11154 | . 3 | . 65 | . 527 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | . 3 | . 65 | . 527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | . 3 | . 65 | . 49 | 35 | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | . 3 | . 65 | . 49 | 50 | 1.4 | 65 | 1.3 |

Hot Rolled Steel Section Sets

|  | Label | Shape | Type | Design List | Material | Design Rules | A [in2] | lyy [in4] | Izz [in4] | J [in4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | MP | PIPE_2.5 | Beam | Pipe | A53 Gr.B | Typical | 1.61 | 1.45 | 1.45 | 2.89 |
| 2 | WM | L3X3X4 | Beam | Single Angle | A36 Gr. 36 | Typical | 1.44 | 1.23 | 1.23 | . 031 |
| 3 | MP 2 | PIPE 2.0 | Beam | Pipe | A53 Gr.B | Typical | 1.02 | . 627 | . 627 | 1.25 |

Joint Coordinates and Temperatures

|  | Label | X [ft] | Y [ft] | Z [ft] | Temp [F] | Detach From Diap... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N1 | 0 | 0 | 0 | 0 |  |
| 2 | N2 | 0 | 11 | 0 | 0 |  |
| 3 | N3 | 0 | 9 | 0 | 0 |  |
| 4 | N4 | 0 | 5 | 0 | 0 |  |
| 5 | N5 | 0 | 9 | -. 333 | 0 |  |
| 6 | N6 | 0 | 5 | -. 333 | 0 |  |
| 7 | N7 | . 5 | 9 | -. 333 | 0 |  |
| 8 | N8 | . 5 | 5 | -. 333 | 0 |  |
| 9 | N9 | -. 5 | 9 | -. 333 | 0 |  |
| 10 | N10 | -. 5 | 5 | -. 333 | 0 |  |
| 11 | N11 | 4 | 3 | 0 | 0 |  |
| 12 | N12 | 4 | 11 | 0 | 0 |  |
| 13 | N13 | 4 | 9 | 0 | 0 |  |
| 14 | N14 | 4 | 5 | 0 | 0 |  |
| 15 | N15 | 4 | 9 | -. 333 | 0 |  |
| 16 | N16 | 4 | 5 | -. 333 | 0 |  |
| 17 | N17 | 4.5 | 9 | -. 333 | 0 |  |
| 18 | N18 | 4.5 | 5 | -. 333 | 0 |  |
| 19 | N19 | 3.5 | 9 | -. 333 | 0 |  |
| 20 | N20 | 3.5 | 5 | -. 333 | 0 |  |

Basic Load Cases

|  | BLC Description | Category | X Gravity | Y Gravity | Z Gravity | Joint | Point |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | DEAD | DL |  | -1 |  | 6 |  |
| 2 | WIND X | WLX |  |  |  |  | 6 |
| 3 | WIND Z | WLZ |  |  |  |  | 6 |

$\qquad$

Member Point Loads (BLC 1 : DEAD)

|  | Member Label | Direction | Magnitude $[\mathrm{k}, \mathrm{k}-\mathrm{ft}]$ | Location[ft,\%] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M 1 | Y | -.074 | 11 |
| 2 | M 1 | Y | -.074 | 3 |
| 3 | M 1 | Y | -.074 | 1.5 |
| 4 | M | Y | -.017 | .5 |
| 5 | M 6 | Y | -.017 | 5.5 |
| 6 | M 6 | Y | -.045 | 8 |

Member Point Loads (BLC 2 : WIND X)

|  | Member Label | Direction |  | Magnitude $[\mathrm{k}, \mathrm{k}-\mathrm{ft}]$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | X | .101 | Location[tt,\%] |
| 2 | M1 | X | .101 | 11 |
| 3 | M1 | X | .032 | 3 |
| 4 | M6 | X | .045 | 1.5 |
| 5 | M6 | X | .045 | .5 |
| 6 | M6 | X | .027 | 5.5 |

Member Point Loads (BLC 3 : WIND Z)

|  | Member Label | Direction | Magnitude $[k, k-f t]$ | Location $[\mathrm{tt}, \%]$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Z | -.244 | 11 |
| 2 | M1 | Z | -.244 | 3 |
| 3 | M1 | Z | -.04 | 1.5 |
| 4 | M6 | Z | -.077 | .5 |
| 5 | M6 | Z | -.077 | 5.5 |
| 6 | M6 | Z | -.042 | 8 |

Member Distributed Loads (BLC 2 : WIND X)

|  | Member Label | Direction | Start Magnitude $[\mathrm{k} / \mathrm{ft}, \ldots$ | End Magnitude[k/ft,F... | Start Location $[\mathrm{ft}, \%]$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | X | .006 | .006 | 0 |
| 2 | M6 | X | .005 | .005 | 0 |

Member Distributed Loads (BLC 3 : WIND Z)

| Member Label | Direction | Start Magnitude[k/ft,... | End Magnitude[k/ft,F... | Start Location[tt,\%] |
| :---: | :---: | :---: | :---: | :---: | End Location[ft,\%]

## Load Combinations

|  | Description | So..P. | S... BLCFac. | . BLC | Fac.. | BLC | Fac.. | BLCF | Fac.. | BLCF | Fac.. | BLCF | Fac.. | BLCF | Fac.. | BLCF | Fac.. | BLCF | Fac.. ${ }^{\text {B }}$ | BLCFac... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | ASCE ASD 1 | Yes Y | DL 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | ASCE ASD 5 (a) (a) | Yes Y | DL 1 | W... | . 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | ASCE ASD 5 (a) (b) | Yes Y | DL 1 | W... | . 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | ASCE ASD 5 (a) (c) | Yes Y | DL 1 | W... | -. 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | ASCE ASD 5 (a) (d) | Yes Y | DL 1 | W... | -. 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | ASCE ASD 7 (a) | Yes $Y$ | DL . 6 | W... | . 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | ASCE ASD 7 (b) | Yes Y | DL . 6 | W... | . 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | ASCE ASD 7 (c) | Yes Y | DL . 6 | W... | -. 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | ASCE ASD 7 (d) | Yes Y | DL . 6 | W... | -. 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

May 27, 2020
12:14 PM
Job Number $\qquad$

Envelope Joint Reactions

| Joint |  |  | X [k] | LC | Y [k] | LC | Z [k] | LC | MX [k-ft] | LC | MY [k-ft] | LC | MZ [k-ft] | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N8 | max | . 057 | 8 | . 484 | 5 | . 113 | 3 | 0 | 9 | 0 | 9 | 0 | 9 |
| 2 |  | min | -. 057 | 6 | -. 364 | 7 | -. 095 | 9 | 0 | 1 | 0 | 1 | 0 | 1 |
| 3 | N10 | max | . 057 | 8 | . 484 | 5 | . 113 | 3 | 0 | 9 | 0 | 9 | 0 | 9 |
| 4 |  | min | -. 057 | 6 | -. 364 | 7 | -. 095 | 9 | 0 | 1 | 0 | 1 | 0 | 1 |
| 5 | N7 | max | . 035 | 4 | . 48 | 3 | . 053 | 7 | 0 | 9 | 0 | 9 | 0 | 9 |
| 6 |  | min | -. 035 | 2 | -. 367 | 9 | -. 072 | 5 | 0 | 1 | 0 | 1 | 0 | 1 |
| 7 | N9 | max | . 035 | 4 | . 48 | 3 | . 053 | 7 | 0 | 9 | 0 | 9 | 0 | 9 |
| 8 |  | min | -. 035 | 2 | -. 367 | 9 | -. 072 | 5 | 0 | 1 | 0 | 1 | 0 | 1 |
| 9 | N17 | max | . 027 | 4 | . 095 | 3 | . 028 | 7 | 0 | 9 | 0 | 9 | 0 | 9 |
| 10 |  | min | -. 027 | 2 | -. 049 | 9 | -. 035 | 5 | 0 | 1 | 0 | 1 | 0 | 1 |
| 11 | N19 | max | . 027 | 4 | . 095 | 3 | . 028 | 7 | 0 | 9 | 0 | 9 | 0 | 9 |
| 12 |  | min | -. 027 | 2 | -. 049 | 9 | -. 035 | 5 | 0 | 1 | 0 | 1 | 0 | 1 |
| 13 | N18 | max | . 021 | 8 | . 095 | 5 | . 033 | 3 | 0 | 9 | 0 | 9 | 0 | 9 |
| 14 |  | min | -. 021 | 6 | -. 049 | 7 | -. 026 | 9 | 0 | 1 | 0 | 1 | 0 | 1 |
| 15 | N20 | max | . 021 | 8 | . 095 | 5 | . 033 | 3 | 0 | 9 | 0 | 9 | 0 | 9 |
| 16 |  | min | -. 021 | 6 | -. 049 | 7 | -. 026 | 9 | 0 | 1 | 0 | 1 | 0 | 1 |
| 17 | Totals: | max | . 279 | 8 | . 409 | 5 | . 44 | 7 |  |  |  |  |  |  |
| 18 |  | min | -. 279 | 2 | . 245 | 6 | -. 44 | 5 |  |  |  |  |  |  |

Envelope AISC 14th(360-10): ASD Steel Code Checks

|  | Member | Shape | Code Check | Loc[ft]LC Shear |  |  | Loc[ft]Dir LC Pnc/om |  |  |  | Pnt/om [...Mnyy/ |  | Mnzz/o | Cb Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M3 | L3X3X4 | . 236 | . 5 | 5 | . 050 | 0 | z | 5 | 30.362 | 31.042 | 1.123 | 2.499 | 1... H2-1 |
| 2 | M2 | L3X3X4 | . 210 | . 5 | 3 | . 049 | 0 | z | 3 | 30.362 | 31.042 | 1.123 | 2.499 | 1... $\mathrm{H} 2-1$ |
| 3 | M1 | PIPE_2.5 | . 164 | 4.927 | 5 | . 017 | 3.094 |  | 9 | 12.508 | 33.743 | 2.393 | 2.393 | 1 H1-1b |
| 4 | M6 | PIPE_2.0 | . 064 | 2 | 5 | . 007 | . 5 |  | 9 | 9.924 | 21.377 | 1.245 | 1.245 | 1 H1-1b |
| 5 | M8 | L3X3X4 | . 047 | . 5 | 5 | . 010 | 0 | z | 5 | 30.362 | 31.042 | 1.123 | 2.499 | 1... $\mathrm{H} 2-1$ |
| 6 | M7 | L3X3X4 | . 039 | . 5 | 3 | . 010 | 0 | z | 3 | 30.362 | 31.042 | 1.123 | 2.499 | 1... $\mathrm{H} 2-1$ |

## Address:

301 Maple Ave W Vienna, Virginia 22180

## ASCE 7 Hazards Report



## Wind

## Results:

Wind Speed:
10-year MRI
25-year MRI
50-year MRI
100-year MRI

## Data Source:

## Date Accessed:

115 Vmph
76 Vmph
84 Vmph
90 Vmph
96 Vmph
ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of March 12, 2014

Wed May 272020

Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability $=$ $0.00143, \mathrm{MRI}=700$ years).

Site is not in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2.
Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

AMERICAN SOCIETY OF CIVIL ENGINEERS
Ice

Results:

Ice Thickness:
Concurrent Temperature:
Gust Speed:
Data Source:
Date Accessed:
0.75 in.

15 F
30 mph
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Wed May 272020

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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